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INITIAL OPERATIONAL TEST AND EVALUATION
OF FORMS 20, 21, AND 22
OF THE ARMED SERVICES VOCATIONAL
APTITUDE BATTERY
(ASVAB)

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Defense Manpower Data Center



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Personnel Testing Division
DEFENSE MANPOWER DATA CENTER



#### NOTE

This report, INITIAL OPERATIONAL TEST AND EVALUATION OF FORMS 20, 21, AND 22 OF THE ARMED SERVICES VOCATIONAL APTITUDE BATTERY(ASVAB), has been produced in two sections to facilitate review.

The front section contains the preface, the executive summary, the text that discusses the procedures and analysis, the appendixes, and a list of references.

The back section, titled ASVAB 20, 21, AND 22 IOT&E SUPPLEMENT, contains all tables and figures that provide information to support the discussion of procedures and analyses.

Reviewed by:

Bert F. Green, Jr.

Johns Hopkins University

This report was prepared for the Directorate for Accession Policy, Office of the Assistant Secretary of Defense (Personnel and Readiness). The technical project officer for this report was Dr. Bruce Bloxom, Quality Control and Analysis Branch, Personnel Testing Division, Defense Manpower Data Center. The views, opinions, and findings contained in this report are those of the authors and should not be construed as an official Department of Defense position, policy, or decision, unless so designated by other official documentation.

# INITIAL OPERATIONAL TEST AND EVALUATION

OF FORMS 20, 21, AND 22

# OF THE ARMED SERVICES VOCATIONAL

## **APTITUDE BATTERY**

(ASVAB)

Gary L. Thomasson, Bruce Bloxom, and Lauress Wise Defense Manpower Data Center

# **JANUARY 1994**

Personnel Testing Division

DEFENSE MANPOWER DATA CENTER

# **TABLE OF CONTENTS**

Preface		• •		•		•	•	•	•	•	•	•	•	•	•	•	•	•	•	•	•	•	•	•	٠	•	•	•	•	•	•	. i
Executiv	ve Summai	ry.									•	•		•			•					•										iii
Introdu	ction						•			•		•		•																		. 1
Method																																. 2
	n																															
	cts																															
	dure																															
Data Qı	ality Cont	rol																														. 3
Editin	g																															. 3
	alence of G																															
	Order Effec																															
Equatin	g of Subte	sts .																														. 6
	ing Method																															
	st Distributi																															
	opment of																															
Comp	arisons of l	Equat	ed-	Sub	test	Int	er	cor	Tel	lati	ion	S	•																			. 9
Analyse	s of Comp	osites	of	Co	nve	rte	d S	Sul	bte	:st	Sc	or	es																			10
Comp	arison with	Refe	ren	ce a	and	Cu	rre	nt	O	pei	rati	on	ıal	F	011	ns																12
	arison with																															
	arison of R																															
Recomn	nended Co	nvers	ion	Ta	ıble	<b>s</b> .						•																•	•	•		16
Summa	ry and Cor	nclusi	ions	3.		•								•			•				•							•				16
Referen	ces						٠,																									17
Append	ixes																															20
A: A	lternative P																															
B: A	lternative M	<b>letho</b>	ds f	or	Eau	atiı	10					_										-				Ī	•		•		•	23
C: L	og-linear Si	nooth	ning	of	AS	VA	В	Su	bte	est	Di	stı	rib	uti	ion	IS I	fro	m	th	е												
	perational ( stimation of																						•	•	•	•	•	•	•	•	•	25
	r Equiperce																							_				_		_		26
	hoosing Alt																															
	onversion o																															
G: D	istributions	of C	om	pos	ites	bу	A	SV	ΑI	3 F	<sup>7</sup> 01	m	A	fte	r (	Co	nν	ers	sio	n 1	Üs	ing	Į F	<b>le</b> c	or	nn	er	nde	d			
E	quatings								•																							38

## PREFACE

The completion of this work would not have been possible without the efforts of many persons at the Defense Manpower Data Center (DMDC) and elsewhere. Dr. Linda Curran, formerly at Air Force Human Resources Laboratory, and Dr. Pamela Palmer at Operational Technologies developed the items used in the new test forms. Mr. John Harris at DMDC and Dr. Wayne Shore at Operational Technologies developed the final forms of the new test booklets. Mr. Richard Branch and others at the Military Entrance Processing Command provided both leadership and day-to-day assistance in the distribution and special administration of the test forms as required for the study. Mr. Robert Hamilton at DMDC meticulously developed and documented the data base for the analyses. Dr. Bert F. Green, Jr., at Johns Hopkins University, provided thoughtful and detailed comments on an earlier version of this report. And Ms. Norma Vishneski at DMDC provided careful attention to all of the necessary details in the final editing and production of the report.

Special recognition must be made of the contributions of Dr. D.R. Divgi at the Center for Naval Analyses. This project was one of the first equating studies conducted entirely at DMDC. Through his generous and extensive counsel on the data analysis plans and procedures for the project, Dr. Divgi provided DMDC with invaluable support, sharing with the authors the benefits of his keen analytic insights and his extensive experience with equating and related statistical issues.

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## **EXECUTIVE SUMMARY**

The Armed Services Vocational Aptitude Battery (ASVAB) is a multiple-choice test battery administered to all applicants for active-duty and reserve enlistment in the United States Armed Services. In addition, it is administered to approximately one million students each year as part of the Department of Defense (DoD) Student Testing Program. The battery consists of the ten subtests listed in Table 1. In addition, Verbal (VE) -- which is the sum of two subtests, Word Knowledge (WK) and Paragraph Comprehension (PC) -- is treated like a separate subtest in many analyses and applications. Various combinations of the subtest standard scores form composites that are used by DoD and the Services for determining eligibility for enlistment and for classification into military occupations.

ASVAB Forms 15, 16, and 17 were implemented for use in the Enlistment Testing Program in January 1989. New items for ASVAB Forms 20, 21, and 22 were developed by the Armstrong Laboratory in the Air Force Human Resources Directorate to replace ASVAB 15, 16, and 17 (Palmer, Curran, and Haywood, 1990). Items were then selected for the new forms by a contractor for Defense Manpower Data Center (Shore, Welsh, and Palmer, 1990). For each of the ten subtests, the items in the new forms were selected to make forms that were parallel to the corresponding subtest of the ASVAB reference form, 8a.

Although ASVAB Forms 20, 21, and 22 were designed to be parallel to the reference form, their item contents and statistical properties could not be assumed to have distributions that are identical to the reference form or to each other. Therefore, it was necessary to equate them to the reference form, so that their scores would have the same interpretation as scores on the latter form. Being able to use this same score scale for all ASVAB forms serves three purposes. First, examinees can receive some assurance that they will have comparable scores for military enlistment, regardless of which ASVAB form is administered to them. Second, DoD and the Military Services can receive some assurance that similar numbers of military applicants will be eligible for enlistment regardless of which ASVAB form is administered. Third, policy makers can use ASVAB scores of cohorts of military recruits to study trends in the aptitude of persons entering the military, even when the cohorts differ in the ASVAB forms that are administered to them.

The present study had three purposes. The first was to develop conversion tables for ASVAB Forms 20, 21 and 22. These tables convert subtest raw scores for each form to equated standard scores. The subtest scores would then be on the 1980 standard score scale, the same as the reference form and other forms used operationally in the Enlistment Testing Program. The second purpose was to provide at least a partial check of the use of these conversion tables for constructing composites of subtests in the Enlistment Testing Program. If the test forms are sufficiently parallel in content, and if the conversion tables are correct, then the composites for the new forms should have the same distributions as the composites for the reference form and current operational forms.

<sup>&</sup>lt;sup>1</sup> For each subtest, the reference-form score scale is defined by a standard-score transformation (mean = 50 and standard deviation = 10) of the number-right score. Standard scores are based on the mean and standard deviation of the subtest in a sample from the 1980 18-23-year-old American youth population (Department of Defense, 1982). See Table 1 for the normative mean and standard deviation of the number-right scores of each subtest.

The third purpose of the study was to adjust the conversion tables for effects of using the new answer sheet implemented in February 1992. Scores on the two speed subtests, NO and CS, can vary across answer-sheet formats (Ree and Wegner, 1990). Specifically, scores have been found to be lower with the new answer sheet than with the one for which norms are available (Bloxom, McCully, Branch, Waters, Barnes, and Gribben, 1991; Bloxom, Thomasson, Wise, and Branch, 1992). Therefore, obtaining accurate conversion tables for these two subtests in this study required score- scale adjustments based on combining the new ASVAB form equating with a prior answer-sheet calibration. The latter calibration was provided in Bloxom et al. (1992).

The design of this study was to administer eight ASVAB forms to randomly equivalent groups of at least 12,000 military applicants each. The eight forms were versions <u>a</u> and <u>b</u> of ASVAB forms 20, 21, and 22 -- plus ASVAB 15g (a current operational form) and ASVAB 15h. Except for its cover, the latter was identical to ASVAB Form 8a, the reference form that was used to collect the normative data (Department of Defense, 1982). The forms were administered as part of the normal processing of military applicants, with scores based on a preliminary equating (Thomasson and Bloxom, 1992) being used to determine eligibility for enlistment and for assignment to military specialties.

The data analyses consisted of data quality-control procedures, checks on the equivalence of the groups taking the eight test forms, a check for item-order effects before pooling the results for different forms having the same items administered in different orders, an equating of subtests on the new forms to subtests on the reference form, the development of subtest conversion tables, and an assessment of the effect of subtest equatings on the equatings of operational composites of subtests.

Analyses of the gender, race, and education of the groups taking the eight test forms showed only slight differences (in gender) between the groups. Also, the sample size varied across test forms in a way that indicated the administration of the forms was not spiralled; but the effects of this on the operational composites were shown to be slight and nonsystematic. However, significant item-order effects were found on forms 21a and 21b of the Coding Speed (CS) subtes: Consequently, even though these two forms of CS contained the same items (in different orders), the were not pooled before being equated to the reference form.

Subtests of the new forms were equated to the reference form using equipercentile equating. The procedure employed subtest distributions that were smoothed by fitting a model with as few parameters as necessary to provide no statistically significant departure from the unsmoothed distributions. The equatings did not produce a perfect match of the new-form AFQT composite distribution to the reference-form AFQT composite distribution or to the AFQT composite distribution of a current operational form. However, the precision of its match to the distributions of those forms was comparable to the match obtained in the IOT&E of ASVAB forms 15, 16, and 17 and in the IOT&E of ASVAB 18/19. Similar patterns of results were found for the Services' specialty composites.

Conversion tables based on the equatings developed here were provided for operational use.

## **INITIAL OPERATIONAL TEST**

AND EVALUATION OF FORMS 20, 21, AND 22

OF THE ARMED SERVICES

**VOCATIONAL APTITUDE BATTERY** 

#### Introduction

The Armed Services Vocational Aptitude Battery (ASVAB) is a multiple-choice test battery administered to all applicants for active-duty and reserve enlistment in the United States Armed Services. In addition, it is administered to approximately one million students each year as part of the Department of Defense (DoD) Student Testing Program. The battery consists of the ten subtests listed in Table 1. In addition, Verbal (VE) -- which is the sum of two subtests, Word Knowledge (WK) and Paragraph Comprehension (PC) -- is treated like a separate subtest in many analyses and applications. Various combinations of the subtest standard scores form composites that are used by DoD and the Services for determining eligibility for enlistment and for classification into military occupations.

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Although ASVAB Forms 20, 21, and 22 were designed to be parallel to the reference form, their item contents and statistical properties could not be assumed to have distributions that were identical to the reference form or to each other. Therefore, it was necessary to equate them to the reference form, so that their scores would have the same interpretation as scores on the latter form.<sup>2</sup> Being able to use this same score scale for all ASVAB forms serves three purposes. First, examinees can receive some assurance that they will have comparable scores for military enlistment, regardless of which ASVAB form is administered to them. Second, DoD and the Military Services can receive some assurance that similar numbers of military applicants will be eligible for enlistment regardless of which ASVAB form is administered. Third, policy makers can use ASVAB scores of cohorts of military recruits to study trends in the aptitude of persons entering the military, even when the cohorts differ in the ASVAB forms that are administered to them.

<sup>&</sup>lt;sup>2</sup> For each subtest, the reference-form score scale is defined by a standard-score transformation (mean = 50 and standard deviation = 10) of the number-right score. Standard scores are based on the mean and standard deviation of the subtest in a sample from the 1980 18-23-year-old American youth population (Department of Defense, 1982). See Table 1 for the normative mean and standard deviation of the number-right scores of each subtest.

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The third purpose of the study was to adjust the conversion tables for effects of using a new answer sheet that was implemented in February 1992. Scores on the two speed subtests, NO and CS, can vary across answer-sheet formats (Ree and Wegner, 1990). Specifically, scores were found to be lower with the new answer sheet than with the one for which norms are available (Bloxom, McCully, Branch, Waters, Barnes, and Gribben, 1991; Bloxom, Thomasson, Wise, and Branch, 1992). Therefore, obtaining accurate conversion tables for these two subtests in this study required score-scale adjustments based on combining the new ASVAB form equating with a prior answer-sheet calibration. The latter calibration was provided in Bloxom et al. (1992).

#### Method

#### Design

The design of this study was to administer eight ASVAB forms to randomly equivalent groups of at least 12,000 military applicants each. The eight forms were versions a and b of ASVAB forms 20, 21, and 22 -- plus ASVAB 15g (a current operational form) and ASVAB 15h. Except for its cover, the latter was identical to ASVAB Form 8a, the reference form that was used to collect the normative data (Department of Defense, 1982). The forms were administered as part of the normal processing of military applicants, with scores based on a preliminary equating being used to determine eligibility for enlistment and for assignment to military specialties.

#### **Subjects**

The subjects in this study were applicants for military enlistment who were scheduled for aptitude testing between 1 October 1992 and 15 January 1993. The total number of persons tested at the sites used for this study was 140,062. The only sites excluded were those associated with the Military Entrance Processing Stations (MEPS) at San Diego, California; Los Angeles, California; and Jackson, Mississippi. There, special studies were being conducted that could not be interrupted.

#### **Procedure**

The subjects were tested in groups that varied in size according to the number of applicants needing to be tested. The test administrators were employees of a MEPS or were persons hired by the Office of Personnel Management (OPM) to administer the test at Mobile Examining Team (MET) sites.

Each subject was provided with the currently operational answer sheet (circular response spaces), an ASVAB test booklet, two pencils, and two pieces of scratch paper. To provide equivalent conditions and frequency of administration for the eight test forms, the forms were to be distributed in a "spiralled" order, that is, a given form was administered to every eighth subject in a test session. Furthermore, the cycle of distribution of forms in each session was to begin where it stopped in the test administrator's previous session. The resulting number of cases administered each of the eight ASVAB forms is shown in the first column of Table 2.

Before the administration of the ASVAB subtests, subjects were given standard ASVAB instructions (Department of Defense, 1990) for providing identifying information and for signing a Privacy Act statement on the answer sheet. The subtests were then administered as specified in the standard ASVAB instructions. Following the test administration, the answer sheets were scanned and scored at MEPS. Number-right (raw) scores and identifying information were electronically transmitted to Headquarters, U.S. Military Entrance Processing Command (MEPCOM). At the end of the study, the data were sent by tape to Defense Manpower Data Center. In addition, item response data were obtained from the scanning of the answer sheets at the METS; these data were mailed to MEPCOM for concatenation into a single file.

# **Data Quality Control**

## **Editing**

In addition to range checks, three procedures were used for editing. The first was to eliminate cases with all subtest scores equal to zero. Such cases were assumed to represent erroneous entries in the data set. Only one such case was found in the data for this study.

The second procedure for editing was to eliminate cases known to have previously taken an ASVAB<sup>3</sup>. Such cases were assumed to be performing in ways not representative of cases in the normative sample (Department of Defense, 1982). This editing resulted in the elimination of 21,796, or 15.6%, of the cases tested. The remaining cases were distributed across test forms as shown in the second column of Table 2.

The third procedure for editing was to delete sessions and sites where the sample sizes for the eight test forms were severely out of balance. As can be seen in the second column of Table 2, the number of cases of initial tests varied from 15,959 for ASVAB 15g to 13,007 for ASVAB 22b. An inspection of the distribution of the eight test forms by test site (defined by a two-digit MEPS code and an additional two-digit site-within-MEPS code) and test date revealed that (a) for some dates at some sites, only a subset of the test forms was administered and (b) for some test sites, one or more of the test forms was never administered during the study.

In the first stage of the third edit, test sessions were defined as severely out of balance when the number of cases that were administered the most frequently used form differed by more than two from the number of cases that were administered the least frequently used form<sup>4</sup>. Deleting these sessions resulted in the deletion of 21,306 cases. Because applying this criterion did not exclude sessions at the large number of low-volume sites, the second stage of the third edit was to apply a similar criterion to the totals across all sessions at test sites where the number of cases was 16 or less during the entire data

<sup>&</sup>lt;sup>3</sup> Information about previous ASVAB testing was provided by recruiters who brought or sent the subjects to be tested.

<sup>&</sup>lt;sup>4</sup> As can be seen from the first two columns of Table 2, the least frequently administered forms were those with the highest form-identification numbers and, therefore, were located lowest in a spiralled set of forms to be administered.

collection.<sup>5</sup> Deleting these out-of-balance test sites resulted in the elimination of 1,302 cases. Following the third edit, the number of cases for each test form was as shown in the third column of Table 2.

As can be noted from the final percentages in Table 2, the edited samples are out of balance to nearly the same extent as the unedited samples. An inspection of data from a number of test sites and sessions suggested that the imbalance was occurring as a result of lack of careful spiralling of test forms across large numbers of small test sessions as well as within those sessions; test administrators at the large number of low-volume test sites tended to consistently use lower-numbered ASVAB forms more often than higher-numbered forms. To evaluate the effect of this imbalance on the utility of the equatings developed in this study, supplemental analyses were conducted using data selected with additional edits to further balance the number of cases administered each form. (See Appendix A.) The results of these analyses are provided in a later section of this report. (See "Comparisons of Results for Three Subsets of Data.")

## **Equivalence of Groups**

During the data collection, the eight test forms were to have been distributed in a spiralled manner to subjects in each testing session. This procedure was intended to provide eight randomly equivalent groups of subjects. However, as noted in the preceding section, the sample sizes differed substantially across the eight test forms. (See Table 2.) If the eight groups also differed on demographic characteristics that are typically correlated with test performance, then the assumption that the groups have the same aptitude distribution would be questionable. If this were the case, then using the data for equipercentile equating would require adjustments of the distributions. Therefore, as a check on group equivalence, the eight groups were compared with respect to three background characteristics (gender, race, and education) that were indicated by the examinees on their answer sheets. Also, the groups were compared with respect to their distribution across the 65 MEPS, because the aptitude distributions of military applicants processed at the MEPS are known to vary.

Table 3 provides frequencies and percentages at each level of gender, race, and education. The group-by-test-form Pearson chi-squares were statistically significant (p < .05) for only one of the three background characteristics: gender. As is indicated by cell percentages and contributions to the chi-square, ASVAB 20b had a slightly higher representation of females than did the other forms.

A 65-MEPS-by-8-test-form Pearson chi-square of the number of persons tested was not statistically significant (chi-square = 271.932, d.f. = 448). This provided some assurance that whatever

MAXZERO = 
$$(7.5 - 0.5*NTOT)$$
, if NTOT < 16  
MAXZERO = 0, if NTOT >= 16

Sites with the number of forms having zero administrations greater than MAXZERO were deleted.

<sup>&</sup>lt;sup>5</sup> If forms were perfectly spiralled at a site, then the maximum number of test forms having zero number of administrations would equal the total number of forms (eight) minus the total number of tests administered at the site (for sites administering fewer than eight tests). For sites administering eight or more tests, the maximum number of forms with zero administrations would be zero. To permit the inclusion of data from some small sites where spiralling was not perfect, the requirement of perfect spiralling was replaced by computing the maximum permissible number of zero administrations (MAXZERO) from the total number of test administered at a site (NTOT) as follows:

differences there were in the aptitude distributions of the 68 MEPS was not directly associated with differences in the sample sizes of the eight test forms.

The results of the group comparisons provided sufficient indication of group equivalence to support proceeding with equating without making adjustments to the distributions. Table 4 provides the resulting subtest means, standard deviations, skewness and kurtosis of the reference form (15h), the current operational form (15g), and the six new ASVAB forms (20a/b, 21a/b and 22a/b) being equated to the reference form.

#### **Item-Order Effects**

For the subtests that are not in the AFQT composite (GS, NO, CS, AS, MC, EI), each pair of same-numbered forms contains the same items (i.e., forms 20a and 20b contain the same items; forms 21a and 21b contain the same items; and forms 22a and 22b contain the same items). However, the subtests that are in the AFQT (AR, WK, PC, MK, and thus VE) contain unique sets of items in each ASVAB form; this provides somewhat greater protection against the compromise of tests in the composite that is used to determine eligibility for enlistment.

In each pair of the same-item, non-AFQT subtests (excluding NO), the items differ slightly in the order of their administration in the two forms. (For the NO subtest, item order was constant across the a and b versions of each form.) The purpose of this slight scrambling of the item order is to make it unlikely that an examinee could obtain correct answers by copying responses from the answer sheet of another person who is administered another ASVAB form.

Two forms of a subtest with the same items but slightly different item orders may not have the same distribution of scores, and may, therefore, require separate equatings to the reference form. For example, the distributions for MC might have been affected by the order of item administration if examinees were using strategies developed on one question to formulate answers for subsequent questions.

A statistical test was used to assess item-order effects for each subtest on each pair of forms containing scrambled orderings of the same items. If the test statistics were found to be significant for a pair of same-item forms, then separate equatings were to be done for each separate form. Otherwise, the distributions of the two same-item forms were to be combined and a single equating developed for use with either form.

A procedure developed by Hanson (1991) that uses log-linear modeling and provides a likelihood ratio chi-square statistic was used to test the differences in test-score distributions of the pairs of same-item different-order subtests. The first step in this procedure, which is also a part of the equipercentile equating of smoothed distributions (see below), is to fit each of the separate distributions using the log-linear model (see Holland and Thayer, 1987) with polynomials of varying degrees. In this study, the upper limit for the degree of polynomial was the smaller of 10 and M/2, where M is the number of items in the subtest. This limit was to restrict overfitting the distribution by further limiting the number of parameters in the polynomial. The next step in the procedure was to determine the degree of polynomial to use for the log-linear fit for each of the separate forms. (See the discussion below on the modified "Haberman's Rule" used to determine the degree of the fitted polynomial.) The higher degree of the two fitted polynomials was chosen to be the "comparison test degree" (CTD). The comparison was then made of the log-linear fit to the combined distribution at degree CTD versus the log-linear fit to the separate distributions at degree CTD. A likelihood ratio chi-square test was made to determine if the fit

of the separate distributions was significantly better than the fit to the combined distribution. In this analysis, an alpha level of 0.05/15 = 0.0033 was used for each statistical test, so that the expected number of Type I errors for the 15 statistical tests would be 0.05.

Table 5 contains the results of the likelihood ratio chi-square tests for item-order effects for each pair of tested forms. For subtests GS, NO, CS, AS, MC, and EI, 20a/b denotes the combination of forms 20a and 20b; 21a/b denotes the combination of forms 21a and 21b; and 22a/b denotes the combination of forms 22a and 22b. Except for CS on forms 21a/b, the chi-square statistic was nonsignificant (alpha = 0.0033). Thus, except for CS on ASVAB 21a/b, the forms could be combined when computing their equating functions for same-item forms for subtests GS, CS, AS, MC, and EI. Same-item forms for the NO subtest were combined because the item order did not vary for that subtest. For the AFQT subtests, all equatings were separate because each form of each AFQT subtest contained unique items.

# **Equating of Subtests**

## **Equating Methods**

The use of ASVAB forms 20, 21, and 22 to obtain scores for use in military enlistment or for comparison with national norms requires that score scales for these forms be given an equating transformation, to enable their scores to be placed on the same standard score scale as the reference form, ASVAB 8a (or 15h).

Several methods of equating were selected from alternatives reported in the research literature. Appendix B provides a discussion of the approaches that were considered and the reasons for selecting the methods -- including smoothing distributions -- used in these analyses. The methods were ones used in previous ASVAB equating studies (e.g., Bloxom and McCully, 1992): linear-identity, linear-rescaling, raw equipercentile, and polynomial-log-linear equipercentile. Linear-rescaling equating was the conventional linear procedure for converting number-right scores on the new test forms to have the same mean and standard deviation as scores on the reference form (e.g., see Angoff, 1971). Linear-identity equating used the scores from the new form without changing them. It was a special case of linear equating, where equal means and standard deviations are assumed. Both the linear-identity and linear-rescaling equating were included for comparative purposes, but neither one was considered for subsequent operational use. Divgi (1988) showed that, for the sample size and population used in this study, linear equatings have a higher cross-validation root- mean-squared error than do equipercentile equatings.

Equipercentile equatings were obtained from each of two estimates of the subtest cumulative frequency distributions. Raw equipercentile equating was an equipercentile equating obtained from the unsmoothed frequency distribution for each test form; this was obtained for reference only and was not considered for operational use because of its lack of smoothness, its large number of parameters, and its consequency greater sampling variability. Polynomial log-linear equating was an equipercentile equating obtained from a log-linear smoothing that included all polynomial terms up through the highest-order statistically significant term (less than the 11th term); the number of terms was based on a decision rule suggested by Haberman (see Holland and Thayer, 1987), with an upper bound placed on the number of terms in the polynomial; the upper bound was the smaller of M/2 and 10, where M was the number of items in the subtest; Table 6 shows the resulting number of terms selected for each of the distributions.

Prior to each equipercentile equating, two modifications were made in the estimates of the cumulative distribution functions. First, the extreme lower tail of each distribution was smoothed in a way that would make the equating smooth and would result in an identity equating at the bottom of the number-right score scale. The major concern was that equipercentile equating is unstable where the score frequencies are small. The reason for making the lower end of the equating converge on an identity equating instead of some other function was that equipercentile equating provides no alternative to assuming parallel measurement where the test contents are parallel, score levels are below the level expected under random responding, and the score frequencies are small. The mechanism for making the lower end of the equating converge on an identity equating here was to substitute a power function (Appendix D) for the estimated cumulative distribution below the 0.5th percentile. The parameters of the function were chosen to preserve both the estimated frequency and cumulative distribution functions where the power function was attached. Such a procedure results in a relatively smooth equating function and does not affect the equating at scores above the .5th percentile. This mechanism is a modification of one used by Kolen and Brennan (1990); those authors used a linear function with a zero intercept instead of the more general power function, resulting in an equating that may not be very smooth at the .5th percentile if the test is short.

The second modification of the cumulative distributions prior to equipercentile equating was to add .5 to the number-right score associated with each cumulative frequency and to create a new origin (X = -.5, F(X) = .0) at the lower end of the function. This was done so that the cumulative distribution could have the conventional interpretation as a continuous-score distribution that is linear from .5 below each number-right score to .5 above each number-right score (Kolen and Brennan, 1990).

After the distributions were smoothed and the equipercentile equatings were computed, the final step was to check the differences between the raw and polynomial log-linear equatings. Specifically, this step required comparing the equatings in the score metric (i.e., in terms of differences between their score scales) and in the frequency metric (i.e., in terms of differences between distributions of the equated scores). These comparisons were measured both in terms of the algebraic distance between functions (root mean square difference) and in terms of the practical impact of those differences (i.e., percent of cases affected). Appendix E provides further details on these criteria and indices.

#### Subtest Distributions and Equatings

Figures 1 through 11 show raw and polynomial log-linear smoothed distributions for each of the 11 subtests. Figure 12 shows the standard-score contrast of the raw, linear-rescaling and polynomial log-linear equatings with a linear identity equating for GS. Figures 14, 16, ..., 32 show these results for the other subtests, AR, WK, PC, NO, CS, AS, MK, MC, EI, and VE, respectively. In each case, the contrast is plotted as a function of the number-right score on the new test form; also shown is the raw frequency distribution of the new test. The means and standard deviations in Table 6 were used to compute the linear-rescaling equatings. The polynomial log-linear smoothings of the distributions were used to compute the corresponding equipercentile equatings. The means and standard deviations from the Youth Population (Table 1) were used to convert the equated scores to the standard scores being contrasted in Figures 12, ..., 32. Tables 7 and 8 summarize the differences between the equating functions in terms of their root mean squared differences and in terms of the practical impact of using one equating versus another. (See Appendix E.) For comparative purposes, these tables also include results from a re-equating of the current operational form, 15g.

Figure 13 shows the contrast (i.e., arithmetic difference) of the cumulative distributions of the new forms' raw and polynomial log-linear equated scores with the cumulative distribution of the

reference-form scores for GS. Figures 15, 17, ..., 33 show these results for the other subtests, AR, WK, PC, NO, CS, AS, MK, MC, EI, and VE, respectively. In each case, the contrast is plotted as a function of the number-right score on the reference form; also shown is the frequency distribution of the reference form. Linear interpolation was used to obtain the cumulative distributions of equated scores at these points. None of the cumulative distributions used in these contrasts was smoothed. Tables 9 and 10 summarize the differences between the distribution functions in terms of their root mean squared discrepancy from the reference form distribution and in terms of the practical impact of using one equating versus another. (See Appendix E.) For comparative purposes, these tables also include results from a re-equating of the current operational form, 15g.

## **Development of Standard Score Conversion Tables**

Conversion to Rounded Equated Standard Scores. For the conversion table for each test form, a rounded equated standard score (RESS) (usually called simply "Standard Score") was computed from the fractional equated standard score (FESS) of the polynomial log-linear equating. For all subtests, except CS and NO (see conversions using new "circle" answer sheets below for subtests CS and NO), the conversion was simply a rounding of the fractional equated standard scores to the nearest integer, then truncating below 20 or above 80.

RESS = 
$$\begin{cases} 20, & \text{if FESS} < = 20\\ 80, & \text{if FESS} > = 80\\ & \text{truncate(FESS+0.5)}, & \text{otherwise} \end{cases}$$

The rounding followed the convention of rounding up if the decimal remainder is greater than or equal to .5, and rounding down otherwise. The truncation followed the ASVAB convention of limiting the standard score scale to values between and including 20 and 80. (See Maier and Sims, 1986.)

Standard Score Conversion Tables with New "Circle" Answer Sheets. Since the speeded subtests, NO and CS, were found by Bloxom et al. (1991, 1992) to have an answer-sheet effect, an additional transformation was needed to put scores of these speeded subtests using the new "circle" answer sheet on the same score scale as the previous "vertical bar" answer sheet scale.

Four steps were used in the development of NO and CS conversion tables for the use with the new "circle" answer sheet. As with all subtests, the first step was to equate the raw number-right score on the new form to the reference form (15h, aka 8a) number-right score (where the "circle" answer sheets were used for both new and reference forms, and denoted by a subscript c):

Equated Number-Right Score = f(Raw Number-Right Score),

and where transformation f is the number-right equating for the new form. Second, the equated number-right scores on the "circle" answer sheet (denoted by a subscript c) were converted to equated number-right-equivalent scores on the older "vertical bar" answer sheet (denoted by a subscript b). This was done by using linear interpolation with the appropriate answer-sheet equatings<sup>6</sup> (denoted by function g) selected in the Optical Mark Reader (OMR) study by Bloxom et al. (1992):

Equated Number-Right Score, = g(Equated Number-Right Score,).

<sup>&</sup>lt;sup>6</sup> These answer-sheet equivalents for the reference form (ASVAB 8a) are shown in the second column of Tables 16 (for NO) and Tables 17 (for CS) in Bloxom et al. (1992).

Third, the 1980 Youth Population means and standard deviations (Table 1) were used to convert the reference-form, "vertical-bar"-answer-sheet-equivalent-fractional-number-right score to the standard-score metric producing the fractional equated standard scores (FESS):

FESS = 50 + 10(Equated Number-Right Score, - M)/S.

The fourth step in developing conversion tables for NO and CS was to round the fractional standard score equivalents and truncate them at 20 and 80, paralleling the last step for the nonspeeded subtests, and producing rounded equated standard scores (RESS) or simply "standard scores." The resulting integers provided the standard score values for NO and CS, for the conversion tables designated for use with ASVAB 20a, 20b, 21a, 21b, 22a, and 22b and the new "circle" answer sheets during the implementation in the Enlistment Testing Program. (Appendix F contains the new-form fractional equated standard scores based on polynomial log-linear equatings for all subtests, including standard scores for NO and CS after linking to the OMR answer-sheet transformation.<sup>7</sup>)

## **Comparisons of Equated-Subtest Intercorrelations**

In previous equating studies of ASVAB 18/19 (Bloxom and McCully, 1992) and 20/21/22 (Thomasson and Bloxom, 1992), differences were found in the correlations between the power subtests that were indicative of variation in the construct validity of the ASVAB subtests across ASVAB forms. In the effort to explore this in the present study, an investigation of the means, variances, and intercorrelations between the subtests' converted standard scores was made. Table 11 contains the subtest standard score means, standard deviations, and intercorrelations for each form; all statistics are based on analyses of rounded standard scores, i.e., scores obtained from application of the conversion tables. Also in Table 11 are the differences between the new forms' subtest standard score means, standard deviations, and intercorrelations and those of the reference form (15h; middle of the page) and the current operational form (15g; bottom of the page). In addition, Figures 34 and 35 1 de plots of the first three unrotated principal components of the power subtests of each of the eight ASVAB forms; the first component is in Figure 34; the second and third components are in Figure 35.

An inspection of Table 11 and Figures 34 and 35 revealed three patterns in the differences between ASVAB forms. The first pattern was that GS was less correlated with the technical subtests on the new forms (ASVAB 20, 21, and 22) than on the reference form and on the current operational form. This pattern was more pronounced in comparisons with the reference form (15h) than with the current operational form (15g); the differences were approximately .05 greater in the comparisons with the reference form. The largest differences were for ASVAB 21a and 21b, where the GS correlation with AS was .23 lower than for ASVAB 15h and where the GS correlation with EI was .18 lower than for ASVAB 15h<sup>8</sup>. Fully understanding this pattern of results requires a study of the correlations between items in GS and the technical subtests. However, in the absence of such a study, it is useful to note that the pattern was consistent with that found in the IOT&E of ASVAB 18/19 (Bloxom and McCully, 1992) and in the previous operational calibration of ASVAB 20/21/22 (Thomasson and Bloxom, 1992). As in

<sup>&</sup>lt;sup>7</sup> Appendix F also contains equated standard scores that were re-developed here for the current operational form, ASVAB 15g. However, these equatings were not used for any of the subsequent analyses reported here.

<sup>&</sup>lt;sup>8</sup> Note that the consistent pattern of results for ASVAB 21a and 21b was due to the fact that both GS and EI had the same items in those two forms.

those studies, the implication here is that the distributions of composites -- such as the Air Force M composite -- containing both GS and technical subtests were more likely to vary across ASVAB forms even if the subtests themselves were accurately equated.

The second pattern in the correlations between subtests was that the new forms were, in general, more like the current operational form than like the reference form. However, a notable exception was in the correlation between VE and EI, which was approximately .10 higher for the new forms than for the current operational form; in contrast, the correlation was slightly smaller (by .02) for the new forms than for the reference form. Although this pattern was reliable and may indicate more of a verbal component to the EI subtest than has been the case in recent operational use, it was not likely to have an impact on the distribution of composites because none of them contains both VE and EI.

The third pattern in the correlations between subtests was that the AFQT subtest scores (VE, AR and MK) had somewhat lower intercorrelations (by approximately .04) for ASVAB 21b than for the reference form, 15h. The pattern was also present in the comparison of 21b with the current operational form, 15g, but the difference was less pronounced (approximately .02-.03). The implication here is the distributions of the AFQT and other composites containing these three subtests were more likely vary across ASVAB forms even if the subtests themselves were accurately equated.

Further analyses -- including item analyses -- are needed to more fully explain the correlational differences between the newer ASVAB forms, the reference form and the current operational form. Wise, Nicewander, and Bloxom (1991) provided analyses of such differences for ASVAB 18/19 and the reference form.

# **Analyses of Composites of Converted Subtest Scores**

The Armed Forces Qualification Test (AFQT) that is used in determining enlistment qualification is based on a weighted sum of three ASVAB standard scores -- VE, AR and MK. For all ASVAB forms, this weighted sum is converted to a percentile score -- the AFQT score -- using norms for ASVAB 8a in the 1980 Youth Population (Department of Defense, 1982). The AFQT score scale is then divided into eight categories having the upper bounds for this composite shown in Table 12. These categories are, from the highest to lowest percentiles, labelled: I, II, IIIa, IIIb, IVa, IVb, IVc, V. AFQT-based enlistment standards and reports of aptitudes of military accessions are typically stated in terms of the AFQT categories (e.g., Department of Defense, 1992).

Other composites of ASVAB standard scores are used by the Services in determining eligibility for training in occupational specialties. Table 12 shows which subtests are used, and how they are combined, in each of these composites for each of the Services. Although the Services each use this general approach for obtaining composites, they differ in the final metric employed in determining training qualification. The Air Force converts the sum of subtest standard scores (SSS) to percentile scores as is done for the AFQT; the Army and the Marine Corps convert SSS to standard scores that have a mean of 100 and a standard deviation of 20 for ASVAB 8a in the 1980 Youth Population; and the Navy uses no further conversion of SSS. Further variability across Services is introduced in the choice of cutting scores that are used to determine training qualifications. (See category boundaries in the right column of Table 20.) For example, the Army has more qualification categories on the EL composite than does the Marine Corps.

Because of the variety and large number of operational composites of the ASVAB subtests, the composites are not separately equated for new ASVAB forms once the subtests of those forms have been equated to the reference form. However, after the subtest equatings have been used to convert their raw scores to standard score equivalents on the reference form, it is important to assess the impact of using the composites of the converted subtest scores -- in terms of the comparability of their composites with those of a current operational form as well as the comparability with those of the reference form. Comparability with a current operational form is important for maintaining continuity of qualification standards for, and rates of flow into, occupational-specialty training schools. Comparability with the reference form is important for maintaining continuity of the AFQT score scale when monitoring long-term trends in qualifications of military applicants and accessions.

To assess the comparability of new-form composites with reference-form composites and current-form composites in this study, converted subtest scores were used to generate composites for all of the forms, with the conversions for the new forms (ASVAB 20/21/22) being based on the equatings described in the preceding section of this report. Then, the distributions of these composite scores for the new forms were compared with the distributions of the corresponding composite scores for the reference form (ASVAB 15h) and with distributions of composites for a current operational form (ASVAB 15g). In the preceding section, comparisons of the subtest intercorrelations across test forms suggested that, even after the subtests were equated, the composites would not necessarily have the same distributions across forms. Therefore, it was thought to be important to assess whether new-form composite distributions differed from the reference form and/or from a current operational form.

Generating the distributions of composite scores for the comparisons required several steps. First, rounded-standard-score conversion tables were generated as described in the preceding section and were applied to all subtest scores from the new test forms. The current standard score conversion table for the reference form, ASVAB 15h, (Department of Defense, 1992; as modified in Bloxom et al., 1992) was applied to all subtest scores from the reference form. The current operational standard score conversion table for ASVAB Form 15g (Department of Defense, 1992; as modified in Bloxom et al., 1992) was applied to all subtest scores from that ASVAB form.

The second step in generating distributions of composites was to sum the standard scores of subtests as indicated in Table 12. These scores were then converted to a percentile or standard score metric, depending on which of those metrics would be used operationally. In the third step, the frequencies at each score level for each composite, plus the category score ranges indicated in Table 12, were used to compute the number of subjects in each category for each test form.

Three types of indices were used to assess differences between the new-form, reference-form, and operational-form distributions of a composite. The first of these was a Pearson chi-square, based on a cross-tabulation of the eight ASVAB forms and the categories defined by operational cut-scores on the composite's score scale. A probability for each chi-square was computed and evaluated without adjusting the alpha level to take into account the number of significance tests; because the chi-squares were computed in the sample used for equating, the true probability of a Type I error was almost certainly below any nominal alpha level applied to the computed probabilities, although the extent of this reduction was unknown. Because the true probability was unknown, the evaluation of these chi-squares included the application of a heuristic; the heuristic was to compare the chi-quare with two times its degrees of freedom.

The second index used to assess differences (across forms) in the distribution of a composite was the standard deviation of the composite. Once the subtests were equated, the means of composites of the

subtests were equated. However, because subtest intercorrelations varied across forms, the standard deviations of the composites could vary across forms. For example, because GS and AS had a lower correlation on ASVAB 21b than on the reference form, the standard deviation of a composite containing the sum of these subtests (e.g., the Air Force M composite) could show a lower standard deviation on ASVAB 21b than on the reference form.

The third index used to assess differences (across forms) in the distribution of a composite was the percentage of all cases at or above a cut score; this was computed for each of the operational cut scores on the composite and was done separately for each of the forms used in this study. The expectation was that those forms with lower standard deviations would have smaller percentages of cases scoring above high cut scores and larger percentages of cases scoring above low cut scores. Unlike the chi-square and standard deviation indices, this index also was useful for assessing the potential operational impact of using the form. By comparing the percentages for a composite on a new form with the corresponding percentages on the reference form (15h), the accuracy of the equating to the reference form could be evaluated in an operationally relevant metric. By comparing the percentages for a composite on a new form with the corresponding percentages on the current operational form (15g), it was possible to estimate the operational impact of a transition from the current operational form to an implementation of the new form.

# Comparison with Reference and Current Operational Forms

The first step in comparing the distributions of each composite for the equated new forms with its distributions for the reference form and the current operational form was to compute a Pearson chi square measuring the independence of composite score categories and test forms. This was based on an m x 8 frequency table with cells containing the number of cases in each of the m cut-score categories for each of eight test forms (20a, 20b, 21a, 21b, 22a, 22b, the reference form [15h] and the current operational form [15g)]. The resulting chi-squares, degrees of freedom<sup>9</sup> and probability values are shown in the first part of Table 13; the table also indicates which of the chi-squares was more than two times its degrees of freedom — a conservative criterion, in that it is less likely to be exceeded by chance as the degrees of freedom become large. Fifteen of the 30 composites — including the AFQT — had chi-squares that were statistically significant at alpha = .05; 8 of the 15 had chi-squares that were more than two times their degrees of freedom. The second part of Table 13 supplements the first part of the table by showing chi-squares and degrees of freedom for the comparison of each new form and the current operational form with the reference form. The results in the two parts of this table clearly suggested that many composites did not have the same distributions across the new forms, reference form and current operational form. The results did not, however, indicate the nature or practical importance of the differences.

The second step in comparing the eight forms' distributions of each composite was to examine the standard deviations of the composite across the ASVAB forms. Table 14 shows these for all composites and for all ASVAB forms used in this study. As expected from the pattern of correlations between the subtests, the two composites containing both GS and AS -- Air Force G and Army GM -- had lower standard deviations on each of the new forms than on the reference form, 15h; for the Air Force G composite -- which double-weights AS -- it was as much as 1.47 lower. Because the equated subtests had essentially the same standard deviations on all forms, the lower standard deviations for composites on the new forms were due to the lower correlations between GS and AS on the new forms than on the

<sup>&</sup>lt;sup>9</sup> Note that the degrees of freedom vary considerably across composites because of the wide variation in the number of categories defined by their cutting scores.

reference form. (See Table 11.) However, this pattern was only somewhat sustained in comparisons of the new form with the current operational form, 15g; each of these two composites had notably lower standard deviations on only two of the new forms (21a and 21b) than on 15g. This, too, can be attributed to the correlations between GS and AS, which were notably lower than 15g only for forms 21a and 21b.

Another pattern in the standard deviations in Table 14 was in the composites of subtests used in the AFQT -- VE, AR, and MK. These five composites are AFQT, Army GT and CL, Air Force G, and Navy GT. As expected from the pattern of lower correlations between these subtests for ASVAB 21b, these five composites had lower standard deviations on ASVAB 21b than on either the reference form or the current operational form.

The third step in comparing the eight forms' distributions of each composite was to examine the percentages of cases exceeding each operational cut point. Appendix G shows a table of these percentages for each of the 30 operational composites listed in Table 12. The top of each table in Appendix G shows the percentage of cases at or above each of the cut points for each of the eight ASVAB forms used in this study; the bottom of each table shows the percentage for each form minus the percentage for the reference form, 15h. For each cut point on the AFQT composite, the percentage above the cut point for each of the new forms was within 1.00 of the percentage for the reference form and within 2.00 of the percentage for the current operational form. The largest of these differences were between the Category-I percentages for new forms 20b, 22a, and the current operational form. In contrast to what was expected from the pattern of subtest intercorrelations and composite standard deviations, ASVAB 21b did not show the lowest percentages of all forms in the highest categories of this composite, or the highest percentages in the lowest category.

Although the pattern in the percentages of cases in the AFQT categories did not show the expected differences across forms, the percentages for the Air Force M composite did show the expected pattern. As was the case for that composite in the IOT&E of ASVAB 18/19 (Bloxom and McCully, 1992, Appendix G), all of the new forms had smaller percentages than the reference form in the highest score category and larger percentages than the reference form in the lowest score category; this would be expected from the lower standard deviation of the composite for the new forms than for the reference form.

In comparing the percentages across forms in Appendix G, it is important to consider how much the percentages can vary due to sampling variability. Although confidence intervals were not provided here, an indication of this variability was provided by the results for the Air Force M composite. In that composite, like-numbered new ASVAB forms (20, 21, and 22) used the same items for all three subtests in this composite; thus, differences in percentages between the results for the a and b versions of each form were attributable to variation in the samples of cases for those versions. Across the six score categories and three ASVAB forms, more than two-thirds of the percentages differed by at least .7 and more than one-third of the percentages differed by at least 1.0. In view of this variability, the magnitude of differences obtained between new forms and the comparison forms (15g and 15h) of the AFQT was not greater than would be expected from sampling variation; however, nonrandom patterns of small differences may have been present.

#### Comparison with IOT&E Results of Other ASVAB Forms

Comparison with IOT&E of ASVAB 15, 16 and 17. To provide a another benchmark for evaluating the comparisons with the reference form in the present study, Table 15 provides the composite-category-by-test-form chi-squares for the ASVAB 15/16/17 IOT&E data, based on the use of

that of the AFQT -- were statistically significant with alpha = .05. Also, 22 of the 33 chi-squares were more than two times as large as their degrees of freedom, with the AFQT chi-square being nearly four times its degrees of freedom. The composite having a chi-square that was the largest multiple of its degrees of freedom was Army MM. For that composite, the percent of cases in the lowest category was from 0.0 to 1.6 less for forms 15/16/17 than for the reference form, and the percent of cases in the highest category was from .9 more to 2.0 less for the new forms than for the reference form. In general, this pattern of results indicated that equal or larger differences existed between forms in the IOT&E of ASVAB 15/16/17 than in the present study.

In the IOT&E of ASVAB 15/16/17, the new-form distributions of composites containing AS -not GS -- differed systematically from the corresponding distributions in the reference form. All ten
composites containing AS had chi-squares that were statistically significant; nine of these had chi-squares
that were more than two times their degrees of freedom. Also, the standard deviations of composites
containing AS (see Table 16) were consistently smaller for ASVAB 15/16/17 than for the reference form.
For the Air Force M composite, which contains GS and gives AS twice the weight of other subtests, the
largest departure of the standard deviations in ASVAB 15/16/17 from the standard deviation in the
reference form was .76 (ASVAB 15a in Table 16); for forms 20/21/22 in the present study, the largest
difference for this composite was 1.47 (ASVAB 21b in Table 14). These results were consistent with
expectation from results reported by Wise, Nicewander, and Bloxom (1991), who found the correlations
of AS with other subtests were an average of .06 lower for forms 15/16/17 than for the reference form.
Thus, differences in subtest intercorrelations were affecting standard deviations and other distributional
indices of composites in the IOT&E of ASVAB 15/16/17 as well as in the present study.

In addition to these systematic differences between standard deviations for forms in the IOT&E of ASVAB 15/16/17, there were nonsystematic differences (in the AFQT distributions) that were of a similar order of magnitude as those obtained in this study. The AFQT standard deviations of new forms ranged from .26 below the reference form to .26 above the reference form in that study (Table 16). In the present study, the standard deviations of the new forms ranged from .16 below the reference form to .40 above the reference form (Table 14).

Comparison with IOT&E of ASVAB 18/19. To provide yet another benchmark for evaluating the comparisons with the reference form in the present study, results reported by Bloxom and McCully (1992) included the composite-category-by-test-form chi-squares for the ASVAB 18/19 IOT&E data, based on the use of the conversion tables obtained from that same data set. Fourteen of the 33 chi-squares -- not including that of the AFQT -- were statistically significant with alpha = .05. Also, seven of the 33 chi-squares were more than two times as large as their degrees of freedom. The composite having a chi-square that was the largest multiple of its degrees of freedom was Air Force M, with a chi-square over seven times its degrees of freedom. For that composite, the percentage of cases in the lowest category was from 1.4 to 2.0 less for the new forms than for the reference form, and the percentage of cases in the highest category was from 2.3 to 3.3 less for the new forms than for the reference form. In general, this pattern of results indicated that at least some differences between forms in the IOT&E of ASVAB 18/19 were of the same order of magnitude as differences between forms in the present study.

In addition to these differences between the frequency tables for forms in the IOT&E of ASVAB 18/19, there were differences in the standard deviations of AFQT distributions that were of the same order of magnitude as those obtained in this study even though the chi-square comparison of AFQT distributions was not statistically significant in the IOT&E of ASVAB 18/19. The AFQT standard deviations of new forms in that study ranged from .01 above the reference form to .41 above the

reference form in that study (Table 17). In the present study, the standard deviations of the new forms ranged from .16 below the reference form to .40 above the reference form (Table 14). Also, the newform standard deviations of the Air Force M composite were as much as 1.36 below the reference-form standard deviation in the IOT&E of ASVAB 18/19; in the present study, the Air Force M new-form standard deviations were as much as 1.47 below the corresponding reference-form standard deviation.

# Comparison of Results for Three Subsets of the Data

The preceding sections reported comparisons of distributions of equated new forms with the distribution of the reference form. These analyses provided an assessment of the precision of the computations of equatings and conversion tables and an assessment of the effects of variation in the covariance structure across ASVAB forms. However, the analyses did not indicate the extent to which the equatings -- and the consequent conversion tables and distributions of composites -- were specific to the samples used for the equating. Of particular concern in this study was the possibility of effects of nonequivalent groups, due to the incompletely spiralled administration of test forms. An earlier section of this paper showed that the administration of test forms was not confounded with gender, race, or education. However, to the extent that some nonequivalence of groups was introduced by incomplete spiralling of administration, group differences in aptitude could have been confounded with test-form differences. If this happened, percentile-equivalent scores on different forms could represent different levels of aptitude.

To estimate the effect of incomplete balancing of test-form administration, three subsets of data were selected to simulate various amounts of balancing across data sets. In each set, the composite distributions for the equated new forms were then compared with the corresponding composite distribution for the reference form. To the extent that the match to the reference form distribution was equivalent across the three data sets, it could be inferred that the equating of composites was robust to -- i.e., invariant across -- at least the simulated amount of variation in balancing.

The three data sets used in this analysis were sequentially nested subsets of each other. The first data set consisted of all initial-test cases, with no removal of cases from severely imbalanced sessions or sites; as indicated in the second column of Table 2, this provided from 13,007 to 15,959 cases per test form. The second data set consisted of all cases used in the development of the equating and conversion tables contained in this report, i.e., excluding the cases from severely imbalanced sessions and sites; as indicated in the third column of Table 2, this provided from 10,986 to 13,312 cases per test form. The thard data set consisted of cases further selected by the procedures for creating "strongly balanced samples," as described in Appendix A; this provided 7497 cases per test form.

Table 18 shows the results of applying the conversion tables developed in this report to obtain the AFQT-category distribution for each of the new test forms; the top, middle, and bottom sections of the table show the results for the first, second, and third data sets, respectively. As in Appendix G, the percentage of cases at or above the cut score for each category is listed separately for the reference form (15h). For each of the other forms, the percentage above each cut score is contrasted with the corresponding percentage for the reference form (15h) in the same data set; also included for comparative purposes is a contrast of the current operational form (15g) with the reference form.

An inspection of the three AFQT category distributions in Table 18 indicated that the first two samples differed very little in AFQT, with percentages differing by no more than .25. It also indicated that the third sample did have a somewhat higher AFQT distribution, with percentages differing from the first two samples by as much as 2.00 for some categories. However, the contrasts of the other forms'

distributions with the reference form distribution did not vary by more than .63 percentage points across the three samples; variation that large was the exception rather than the rule. Furthermore, an inspection of the pattern of differences between samples revealed nothing indicative of an effect of editing (i.e., systematic variation of contrasts across samples).

Tables 19 and 20 show the results of the same kinds of analyses as in Table 18. Table 19 shows comparisons with the reference form for the Air Force M composite. Table 20 shows comparisons with the reference form for the Army GM composite. These two composites were analyzed here because each uses both the AS and GS subtests; this makes them relatively sensitive to changes in distributions across test forms where those changes are due to changes in the AS-GS correlation. In general, contrasts of the other forms' distributions with the reference form distribution did not vary by more than .61 and .86 percentage points across the three samples for the M and GM composites, respectively; and variation that large was the exception rather than the rule. Furthermore, an inspection of the pattern of differences between samples revealed nothing indicative of an effect of editing.

#### **Recommended Conversion Tables**

On the basis of the results of this study -- including comparisons of these results with previous IOT&E studies and comparisons across data sets simulating various amounts of balancing of test administration -- it was recommended that conversion tables obtained from the equipercentile equatings in the present study be implemented operationally. These tables are presented in Tables 21-26 and contain rounded and truncated values from Appendix F.

# **Summary and Conclusions**

In October 1993, the Department of Defense planned to begin using ASVAB 20, 21, and 22 in the Enlistment Testing Program. This necessitated equating these forms to the reference form, ASVAB 8a (aka. ASVAB 15h). The results of this study indicated that equipercentile equating of subtests on the new forms to subtests on the reference form resulted in equatings of composites on the new forms that were comparable in accuracy to equatings obtained on previous operational ASVAB forms -- ASVAB 15/16/17 and ASVAB 18/19. The results also indicated that the accuracy of the equatings did not vary as a function of unbalanced form administration, to the extent that such administration could be simulated by editing the data. However, it should be noted that, on some composites other than the AFQT, there were systematic departures from the distributions provided by the reference form. Composites containing the GS subtest in combination with technical subtests -- most notably AS -- tended to have smaller standard deviations on the new forms. Additional analyses showed this also to be true for the subtest equatings currently used operationally with ASVAB 15/16/17 and with ASVAB 18/19. The problem is that the reference form contains some subtests -- most notably, GS -- that are more highly correlated with other subtests than is the case for the ASVAB forms developed in recent years.

Because the results of equating ASVAB 20, 21, and 22 to the reference form showed patterns similar to results previously obtained for equatings of operational ASVAB forms, this study provided a set of conversion tables (Tables 21-26) that were recommended for operational use.

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# **Appendixes**

# Appendix A:

# Procedure for Balancing Sample Sizes Across ASVAB Forms

Current procedures for operational administration of the ASVAB in an Initial Operational Test and Evaluation (IOT&E) do not result in equal numbers of examinees being administered each of the ASVAB forms, i.e., the test forms are not spiralled within and across test sessions. Although the resulting variation in sample size does not appear to be directly related to the MEPS region, the week or month of testing, or the examinee's Gary L. Thomasson or education, it may still result in a calibration that is specific to the mixture of populations in the IOT&E data collection and not to the population of military applicants under normal operational conditions, when more nearly equal numbers of examinees are administered each of the ASVAB forms. Furthermore, if the aptitude distribution varies across forms as a result of the lack of spiralling, the calibration cannot be viewed as an equating of the forms.

In an effort to obtain balanced samples from an unbalanced IOT&E data set, cases were deleted from various combinations of test forms, testing groups (defined by site and four-week period of testing) and demographic groups (defined by gender, race, and education). Testing groups and demographic groups were used as control variables during the deletion of cases because of their potential relationships to the aptitude distribution. Not controlling these variables during the deletion of cases could introduce -- or exacerbate -- either random or systematic differences in aptitude distributions across test forms.

A major constraint in the balancing of samples was the requirement that the sample size for each form not be reduced below the sample size for the form used least frequently. The purpose of this constraint was to obtain balancing while deleting as few cases as possible. The first application of the constraint was at the level of the overall sample, i.e., such that the sample size for each form not be reduced below the sample size of the form used least frequently in the overall sample. In this study, the form used least frequently overall was ASVAB 22b. This form was, therefore, designated as the "target" form for balancing at the level of the overall sample. Cases for the other seven forms were deleted to provide sample sizes the same as for the target form. Because this resulted in the least loss of data, the resulting samples were called weakly balanced samples.

The second application of the balancing constraint was at the level of the testing-group sample, i.e., such that the sample size for each form in a testing group (defined by test site and four-week period) not be reduced below that of the form used least frequently in that testing group. Thus, the "target" form could vary from site to site and from period to period within a site. Because this target form was, for some testing groups, a form used less frequently than ASVAB 22b, the result was a greater loss of data than when ASVAB 22b was the target form for all groups. Thus, the resulting samples were called strongly balanced samples.

Weakly Balanced Samples. To specify the deletion procedure for the weakly balanced samples, let t = 1,...,D denote the index of testing groups and d = 1,...,D denote the index of demographic groups. Then let  $m_{td}$  be the target form's sample size for testing group t combined with demographic group d, and let  $m_{td}$  be the target form's marginal sample size over all testing groups and demographic groups. Similarly, let  $n_{tdj}$  and  $n_{...j}$  be the td-conditional and marginal sample sizes of ASVAB form j, where j is a form other than the target form.

The object of the deletion procedure was to delete  $n_{i,j}$  -  $m_{i,j}$  cases for form j. If the TD differences  $n_{idj}$  -  $m_{id}$  were all non-negative, then deleting  $z_{idj} = n_{idj}$  -  $m_{id}$  cases from group td for each of the TD groups would result in  $n^*_{idj} = n_{idj}$  -  $z_{idj} = m_{id}$  cases for form j for each of the TD groups and would meet the objective of obtaining  $n^*_{i,j}$  -  $m_{i,j} = 0$ .

However, it became known that some  $n_{tdj} - m_{td} < 0$ , i.e., that the target form was used more than form j in some groups. It was therefore necessary to define  $z_{tdj} = 0$  for those groups. (Cases could not be added for form j.) This, in turn, would result in the sum of the  $z_{tdj} > n_{tdj} - m_{td}$ . To obtain balancing in this situation, the number to be deleted from each group was not  $z_{tdj} = n_{tdj} - m_{td}$ ; instead it was a smaller number,  $d_{tdj} = a_j z_{tdj}$ , where the scale factor  $a_j = (n_{tdj} - m_{td}) / z_{tdj} < 1.$  Summing the  $d_{tdj}$  across the TD groups then yielded the total number of deletions for form j,  $d_{tdj} = a_j z_{tdj} = [(n_{tdj} - m_{td}) / z_{tdj}] = [(n_{tdj} - m_{td}) / z_{tdj}] = [(n_{tdj} - m_{td}) / z_{tdj}]$ , which was the number of deletions required to obtain balanced samples.

For each form j, cases could be deleted from the TD groups by either of two approaches. The first was random sampling from a uniform distribution, with a deletion threshold determined by the probability of deletion,  $p_{tdj} = d_{tdj}/n_{tdj}$ . The second was systematic deletion of one out of every  $n_{tdj}/d_{tdj}$  cases<sup>11</sup>, using a selected ordering of the cases in the data file. The latter approach was used in this study to better stratify cases by test session and by SSN within test session, the two variables that determined the ordering of cases within groups in the file. Because aptitude distributions tend to vary by date of testing, it was assumed that this would introduce less random variation in the aptitude distribution than would random sampling of cases to be deleted.

The result of applying this procedure in this study -- along with edits of retesters, extreme departures from balancing, and cases with all scores equal to zero -- was to obtain 10,986 cases for each ASVAB form, the number of cases that were obtained for ASVAB 22b before the procedure was used.

Strongly Balanced Samples. To specify the deletion procedure for the strongly balanced samples, again let t=1,...,T denote the index of testing groups and d=1,...,D denote the index of demographic groups. Then let  $m_{td}$  be the target form's sample size for testing group t combined with demographic group d and  $m_{t}$  be the target form's marginal sample size over all demographic groups for testing group t. Similarly, let  $n_{tdj}$  and  $n_{t,j}$  be the td-conditional and t-conditional sample sizes of ASVAB form j, where j is a form other than the target form.

<sup>&</sup>lt;sup>10</sup> Note that, like  $z_{tdj}$ ,  $d_{tdj}$  is zero when  $z_{tdj}$  is zero, whether the latter is due to negative or null differences between  $n_{tdi}$  and  $m_{td}$ .

Because the ratio,  $n_{tdj}/d_{tdj}$ , is not an integer, the probability  $p_{tdj}$  was used to define a sequence of non-integers,  $s_{tdj} + p_{tdj}$ ,  $s_{tdj} + 2p_{tdj}$ ,...,  $s_{tdj} + kp_{tdj}$ , ..., which were used to select cases to be deleted. Specifically, the k-th case was deleted where the following condition held for truncated values of elements of the sequence:

trunc. [ $s_{tdj} + kp_{tdj}$ ] > trunc. [ $s_{tdj} + (k-1)p_{tdj}$ ]. The start value,  $s_{tdj} < 1$ , was .5 for the first group (td = 1) and was the decimal remainder from the truncation of the last number of the sequence for each successive group; i.e., for all td > 1,  $s_{tdj} = dec.rem$ . [max. ( $s_{(td-1)j} + kp_{(td-1)j}$ )].

<sup>&</sup>lt;sup>12</sup> Note that the target form is the form used least frequently in testing group t and so can differ across testing groups.

The object of the deletion procedure for each testing group t was to delete  $n_{i,j}$  -  $m_{i,j}$  cases for form j. If the D differences  $n_{idj}$  -  $m_{id}$  were all non-negative, then deleting  $z_{idj} = n_{idj}$  -  $m_{id}$  cases from group td for each of the D groups would result in  $n^*_{idj} = n_{idj}$  -  $z_{idj} = m_{id}$  cases for form j for each of the D groups and would meet the objective of obtaining  $n^*_{i,j}$  -  $m_{i,j}$  = 0.

It was expected, however, that some  $n_{tdj}$  -  $m_{td}$  < 0, i.e., that the target form was used more than form j in some demographic groups. It was then necessary to define  $z_{tdj} = 0$  for those groups. (Cases could not be added for form j.) This, in turn, would result in the sum of the  $z_{t,j} > n_{t,j}$  -  $m_{t,j}$ . To obtain balancing in this situation, the number to be deleted from each group was not  $z_{tdj} = n_{tdj} - m_{td}$ ; instead it was a smaller number,  $d_{tdj} = a_{tj} z_{tdj}$ , where the scale factor  $a_{tj} = (n_{t,j} - m_{t,j}) / z_{t,j} < 1$ . Summing the  $d_{tdj}$  across the D groups then yielded the total number of deletions for form j,  $d_{t,j} = a_{tj} z_{t,j} = [(n_{t,j} - m_{t,j}) / z_{t,j}]$  [ $z_{t,j} = (n_{t,j} - m_{t,j})$ , which was the number of deletions required to obtain balanced samples.

The procedure for using  $d_{tdj}$  to delete cases from each of the TD groups for strongly balanced samples was the same that used to delete cases for the weakly balanced samples. The result of applying this procedure in the present study -- along with edits of retesters, extreme departures from balancing, and cases with all scores equal to zero -- was to obtain 7497 cases per form.

# **Appendix B:**

# **Alternative Methods of Equating**

When equating new-form subtests, so their right-number scores will be on the same score scale as on the reference form, several approaches can be considered. The primary approaches discussed here comprise the following methods of equating: random-groups linear equating, random-groups equipercentile equating, matched-groups linear equating, and matched-groups equipercentile equating. True-score equating is not included here, because of the lack of research and experience related to equating from an item response theory for speed tests, which are two of the ten subtests of the ASVAB. Summary descriptions of these five approaches are provided in Angoff (1971); Braun and Holland (1982); Peterson, Kolen, and Hoover (1989); Kolen and Brennan (1990); and Dorans (1990).

Even though a randomly-equivalent-groups design is typically used for ASVAB equating-data collection, matched-groups equating methods can be considered when the subjects are military recruits. These methods potentially can control for whatever random differences occur between groups. The matching variable in this case would be the pre-enlistment ASVAB score on the subtest being equated. Any association of this score with the score on the test being equated could potentially be exploited to improve the precision of the equating.

In spite of this theoretical advantage of matched-groups equating, the approach is not considered for equating forms of the ASVAB. When forms are being administered operationally (in an IOT&E) to collect equating data, a separate matching variable is not available, unlike when forms are being administered to military recruits. Even when equating data are being collected from recruits -- in which case pre-enlistment scores are available -- using these scores to obtain a more precise equating has not yet been demonstrated. The problem is that the matching variable (pre-enlistment ASVAB) is a measure taken, in some cases, two years prior to the test being calibrated, and under different motivational conditions. This is in contrast to conventional matched-groups equating in which the matching variable is a measure taken in close temporal proximity to, and under similar motivational conditions as, the test being calibrated. Systematic influences between the measurement of the matching variable and the test being calibrated include substantial selection (50% for military enlistment), learning (during the final year of secondary education), and motivational changes (from operational to non-operational conditions of administration). This, plus the highly skewed -- in the case of NO, monotonic -- distributions of ASVAB subtests, make it difficult to assume that the results of previous studies of matched-groups equating (e.g., see Dorans [Ed.], 1990) generalize to the present context. However, there is a need for ASVAB studies of matched-groups equating -- e.g., using the evaluation design employed by Divgi (1988) -- so that any improvements obtainable by this approach could be exploited in future calibrations.

Random-groups linear equating and random-groups equipercentile equating are methods that have been used for equating new forms of the ASVAB. Also, both approaches were used in an answer-sheet calibration study by Ree and Wegner (1990). Divgi (1988a) compared linear and equipercentile equatings from recruit samples and, for each approach, found some subtests in which the approach provided the best prediction of equating in large samples of military applicants. However, Divgi (1988b) found that for sample sizes closer to those used in an IOT&E data collection, linear equatings do not replicate as well as equipercentile equatings.

Equipercentile equating usually employs some form of smoothing, either the test distributions or the equating function, in an effort to reduce the sampling variance of the equating function. Three criteria

guide the choice between alternative smoothing methods for use in equipercentile equating. The first criterion is that the method be symmetric, so that the equating can serve as a basis for converting scores on either test form to the score scale provided by the other test form; this is a criterion that has been advocated by Lord (1980); Peterson, Kolen, and Hoover (1989); and Dorans (1990) in support of the idea of interchangeability of equated test forms. The second criterion is that the method of estimating score distributions use a statistical measure of fit to the distributions of scores on the two test forms. The third criterion is that there be a sequence of distributional models, differing primarily in their number of parameters; the objective here is to choose the model with the smallest number of parameters to reduce sampling variability in the estimator of the equating function.

Equipercentile equating based on smoothed distributions, instead of using smoothed equating functions, can be developed in a way that satisfies these three criteria. This approach -- termed presmoothing (Fairbank, 1987) -- provides a symmetric equating by independently smoothing the distribution of scores obtained from each test form instead of risking the regression effects associated with smoothing the equating function directly.

By basing the equating on log-linear-smoothed distributions, the method also provides a statistical measure of fit to the distributions. The smoothing employs the method of maximum likelihood to fit polynomials to the logarithm of the frequency distributions, in a manner suggested by Holland and Thayer (1987). This method is implemented by a computer program (Hanson, 1990), which provides a chi-square fit statistic for polynomials with as many as ten terms.

By basing alternative equatings on a sequence of log-linear-smoothed distributions, it is possible to select an equating obtained from the smallest number of parameters without jeopardizing the fit of the model to the data. The procedure is to obtain as many terms in the polynomial as are necessary to provide a good statistical fit to the non-null bins of a distribution. Sampling variability is then reduced by excluding all terms with a power higher than ten and all other high-order terms that do not improve the fit. (See example of results in Appendix C.) The method has an added advantage of exactly preserving as many moments of a distribution as there are powers of x in the polynomial. Although equipercentile equating is not defined in terms of preserving the moments of a distribution, knowing that the first several moments are preserved provides another check on the extent to which the distribution is preserved. Of course, exactly fitting the first few moments of a distribution is a desideratum only in samples of the size used in equating studies; in smaller samples, this would result in an overfitting --particularly of the higher moments of the distribution.

# **Appendix C:**

# Log-Linear Smoothing of ASVAB Subtest Distributions From the Operational Calibration of ASVAB 15, 16, and 17

# Lower/Upper Bounds (Up to 10) of Polynomial Degree Producing Statistically Significant\* Improvement in Likelihood-Ratio Chi-Square

		ASVAI					
Subtest	15a	15b	15c	<u>16a</u>	16b	17a	17b
GS	6/6	6/6	2/6	2/4	2/8	4/4	6/9
<b>A</b> R	4/4	4/10	4/4	3/8	4/6	4/4	4/4
WK	5/8	6/6	3/10	4/4	3/6	2/10	3/8
PC	5/5	6/9	4/4	4/10	4/7	4/4	5/5
NO	4/9	4/6	5/8	4/8	4/9	4/8	4/8
CS	5/5	5/5	5/7	5/7	5/5	5/10	5/7
AS	5/5	4/4	6/6	4/4	6/6	4/4	4/6
мк	4/4	4/7	4/10	4/8	4/8	5/5	4/4
MC	2/4	2/9	4/7	2/4	2/4	2/5	2/4
EI	5/5	5/5	2/4	4/4	4/4	4/10	4/4
VE	8/8	6/6	4/6	4/6	6/10	2/6	4/4

<sup>\*</sup> Alpha = .05 with d.f. = 1. Lower bound is the number of terms including and below which each produces a statistically significant improvement in the fit to the data. Upper bound is the highest-numbered term that produces a statistically significant improvement in the fit to the data; some lower-numbered terms may not produce a significant improvement in the fit.

# **Appendix D:**

# Estimation of the Lower Tail of the Subtest Cumulative Distribution for Equipercentile Equating

Let  $F_i$  be the proportion of the population at or below test score i, i=0,...,m, where m is the number of items in the test.

Let  $f_i$  be the proportion of a population of subjects at test score i, or  $f_i = F_i - F_{i-1}$ 

Let u in 0 < u < m be the lowest (integer) score above j, such that  $F_i$  .005.

Let the estimated

$$F_i = [(i+1)/(u+1)]^c F_u,$$
 (1)

where c is chosen to preserve the slope of F<sub>i</sub> over the interval (u-1,u). Then

$$c = \ln [1 - f_u/F_u] / \ln [u/(u+1)].$$
 (2)

Proof:

If 
$$i = u$$
, then  $[(i+1)/(u+1)] = 1$  and  $F_i = F_u$  in (1).

If 
$$i = u$$
, then, from (1),  $F_{u-1} = [u/(u+1)]^c F_u$  and  $f_u = F_u - F_{u-1} = F_u - [u/(u+1)]^c F_u = F_u \{1 - [u/(u+1)]^c\}$ .

Dividing by F<sub>u</sub>, transposing terms, and taking logarithms yields

c 
$$\ln [u/(u+1)] = \ln [1 - f_u/F_u].$$

Dividing by  $\ln [u/(u+1)]$  yields (2).

# **Appendix E:**

#### **Choosing Between Alternative Equatings**

In their discussion of evaluating an observed-score equating, Braun and Holland (1982) stated that, if there exists a population for which the reference-form distribution differs from the equated new-form distribution, then the forms have not been equated. This implies two metrics in which equatings can be compared. The first is the score metric, in which the (cumulative) frequency is held constant and equated scores are compared. This is a type of comparison often used in a close study of alternative equatings, e.g., to see how different a linear equating is from an equipercentile equating. If various equatings provide similar equated scores, they are considered equally acceptable from the perspective of the examinee.

The second metric implied by Braun and Holland is the frequency metric, in which the score is held constant -- e.g., at integer values on the reference form -- and the cumulative distributions of the equated scores and reference form scores are compared. This is a type of comparison used to assess whether implementing an equated new form will change the score distributions, e.g., to see if there will be a change in the percent of persons qualifying for employment. If various equatings have no effect on the score distributions, they are considered equally acceptable from the perspective of the employing institution (Sympson, 1985).

Two criteria can be used to assess differences between the alternative equatings in the score metric. The first criterion is the root mean squared difference between a pair of equatings, with the difference at each score level weighted by the proportion of cases at that level on the new test form. The second criterion is the proportion of cases (from the new-test-form distribution) for which the two equatings differ by more than .5 standard score points (Department of Defense, 1988). The first criterion is an index of the algebraic difference between two sets of equated scores. The second criterion is an indicator of the practical impact of using one equating instead of the other.

Two criteria can be used to assess differences between alternative equatings in the <u>frequency</u> metric. The first criterion is the root mean squared difference between the cumulative distribution of equated scores (after linear interpolation at integer scores on the reference form) and the cumulative distribution of scores on the reference form, with the difference at each score level weighted by the proportion of cases at that level on the reference form. The second criterion is the proportion of cases (from the reference form distribution) for which the cumulative proportions differ by more than .01. The first criterion is an index of the algebraic difference between the equated-score and reference distributions. The second criterion is an indicator of the practical impact (on the score distribution) of using the equated new test form instead of the reference form.

When two or more methods of equating are being considered for operational use, a procedure for choosing between them is to use the two root-mean-squared-difference indices (in the score metric and in the frequency metric) to select the equating with the best fit to the raw equipercentile equating. Then, the two indices of impact (in the score metric and in the frequency metric) can be used to assess whether an equating with fewer parameters could be employed without having a practical consequence for the equated scores or their cumulative distribution.

The following heuristics implement this procedure for selecting an equating for ASVAB subtests. They specify cutting points on the indices employed to compare equatings. The cutting points

have been chosen from a visual inspection of the results of applying them to the data from the OPCAL of ASVAB 15, 16 and 17. (See Appendix C for results of fitting the log-linear model to the distributions from this data set.) In choosing the points, an effort was made to provide some choice between alternative equatings where it seemed reasonable to have a choice, e.g., where two equatings with differing numbers of parameters provided visually similar equatings and visually similar equated-score distributions. An advantage of using cut points as specific as these is that the selection procedure can be replicated and evaluated. A disadvantage of this approach is that the cutting points based on a study of military recruits may not result in the selection of the best equating for population of military applicants, in which equatings are be used. More research is required to assess the inferential validity of the cutting points for selecting the most appropriate equating to use in an applicant population. Until such research provides further reassurances about these cutting points or provides more defensible alternatives, the last step, (e), in the hearistics provides a necessary confirmation that the selected equating is accurate at least for the subtest and sample in which the equating was developed.

#### The heuristics are:

- (a) Select the smooth equating that minimizes the root-mean-squared-discrepancy between the smooth equating (linear or smoothed-equipercentile) and the raw equipercentile equating; then,
- (b) Compare the smooth equating from (a) with other smooth equatings that use fewer parameters; select the equating with the fewest parameters if it reduces the root-meansquared-discrepancy in the frequency metric by at least 10% without increasing the root-mean-squared-discrepancy in the score metric by more than 10%; if no such alternative smooth equating exists, use the selection from (a) as the best-fitting alternative; then,
- (c) Compare the equating selected in (b) with other smooth equatings that use fewer parameters; find those equatings with fewer parameters that also differ from (b) by more than .5 standard score points for fewer than 10% of the cases; then,
- (d) Select that equating from (c) that uses the fewest parameters and that results in fewer than 10% of the cases at scores where the equated cumulative distribution differs from the reference cumulative distribution by more than.01; then,
- (e) Graphically inspect the differences between an identity equating, a linear equating and any equipercentile equatings under consideration; also, graphically inspect the differences between the reference-form cumulative distribution and the distributions of equated scores based on the equipercentile equatings under consideration.

# Appendix F:

## Conversion of GS Raw Test Scores to 1980 Unrounded Standard Score Equivalents

Raw	15G	203	20B	21A	21B	22A	22B
0	17.91397	17.83452	17.83452	18.39998	18.39998	18.59734	18.59734
1	19.88265	19.79450	19.79450	20.42165	20.42185	20.64081	20.64081
2	21.79847	21.68481	21.68481	22.49374	22.49374	22.77608	22.77608
3	23.69515	23.54969	23.54909	24.58375	24.58375	24.94459	24.94459
4	25.58435	25.40510	25.40510	26.68083	26.68083	27.12610	27.12610
5	27. <b>4699</b> 5	27.25558	27.25558	26.76132	28.76132	29.22347	29.22347
6	29.52851	29.27368	29.27368	30.43061	30.43061	30.96139	30.96139
7	31.51705	31.19056	31.19056	31.97861	31.97861	32.57831	32.57931
8	33.47853	33.0 <b>669</b> 5	33.06695	33.53501	33.53501	34.22869	34.22869
9	35.44093	34 . 93524	34.93524	35.09428	35.09428	35.91191	35.911 <b>9</b> 1
10	37.42388	36.84445	36.84445	36.54449	36.54449	37.62493	37.62493
11	39.43567	38.79329	38.79329	38.10338	38.10338	39.36369	39.36369
12	41.47170	40.77064	40.77064	39.76661	39.76661	41.12347	41.12347
13	43.51519	42.75737	42.75737	41.53483	41.53483	42.85988	42.85988
14	45.54170	44.73010	44.73010	43.40689	43.40689	44.62671	44.62671
15	47.52653	46.66711	46.66711	45.37355	45.37355	46.41880	46.41880
16	49.45260	48.55415	48.55415	47.41423	47.41423	48.23683	48.23683
17	51.31593	50.38886	50.38886	49.49942	49.49942	50.08934	50.08934
18	53.12736	52.18194	52.18194	51.59920	51.59920	51.99303	51.99303
19	54.92116 56.74766	53.9 <b>566</b> 5 55.7 <b>48</b> 06	53 . <b>9566</b> 5 55 . <b>748</b> 06	53.69433 55.7 <b>05</b> 29	53.69433 55.78 <b>5</b> 29	53.97224	53.97224
20 21	58.65691	57.60411	57.60411	57. <b>8966</b> 5	57. <b>8966</b> 5	56.05617 58.27118	56.05617 58.27118
22	60.69924	59.58778	59. <b>58778</b>	60.07465	60.07465	60.62299	60.62299
23	62.90255	61.77491	61.77491	62.37291	62.37291	63.06665	63.06665
24	65.30792	64.23561	64.23561	64.81174	64.81174	65.69345	65.69345
25	67.81637	66.99136	66.99136	67.47499	67.47499	68.06579	68.06579
43	00103.	44 . 22774	90 · 32130	01.4/477	07.4 <b>/43</b> 3	99.V93/7	90.093/7

## Conversion of AR Raw Test Scores to 1980 Unrounded Standard Score Equivalents

```
25.43686
26.78031
                25.36979
26.70698
                            26.27766
27.72933
                                       25.49755
26.84667
                                                  25.28033
                                                              25.31474
                                                                         25.61453
                                                   26.60916
                                                              26.64678
                                                                         26.97458
                                       28.18040
     28.09621
                                                              27.92679
                28.00317
                            29.28587
                                                   27.87906
                                                                         28.34267
     29.40136
                29.28338
                            30.93671
                                       29.50812
                                                   29,12600
                                                              29.18653
                                                                         29.71389
                            32.47386
33.79089
     30.70223
                                       30.83345
                30.55723
                                                   30.36380
                                                              30.43819
                                                                         31.08637
     31.98745
                31.85902
                                       32.19897
                                                   31,62381
                                                              31.88222
                                                                         32.27819
                            35.03080
     33.26050
                33.06552
                                       33.53691
                                                   32.74028
                                                              33.29365
                                                                         33.43412
     34.56800
                34.10053
                            36.26829
                                       34.85600
                                                   33.91511
                                                              34.63283
                                                                         34.61815
     35.89854
37.24618
                            37.50858
                                       36.16024
                35.13634
                                                   35.12282
                                                              35.89346
                                                                         35.82789
                                                              37.09452
38.23470
                36.20257
                            38.75630
                                                   36.35047
                                                                         37.05790
                                       37.44555
     38.60608
10
                37.29906
                            40.01554
                                       38.71169
                                                   37.59514
                                                                         38.32769
11
     39.97323
                38.42801
                            41.28890
                                       39.96696
                                                   38.86149
                                                              39.41299
                                                                         39.66551
                            42.57647
                                       41.22652
     41.34256
                39.59185
                                                   40.15968
                                                              40.65185
                                                                         41.06309
     42.70978
                            43.87529
                                       42.50435
                                                              41.96448
                                                                         42.50789
13
                40.84767
                                                   41.50277
                                       43.81010
                                                              43.34962
     44.07206
                42.19338
                            45.18010
                                                   42.90344
                                                                         43.97500
                            46.49036
15
     45.42821
                 43.62146
                                       45.14369
                                                   44.37062
                                                              44.79093
                                                                         45.44786
                            47.80404
16
     46.77852
                 45.11404
                                       46.48874
                                                   45.90698
                                                              46.26124
                                                                         46.90663
                            49.12208
17
     48.12424
                 46.64264
                                       47.82542
                                                   47.50812
                                                              47.73602
                                                                         48.33643
                            50.44800
51.78697
                                                              49.20187
18
     49.46716
                 48.17759
                                       49.13990
                                                   49.16295
                                                                         49.73099
                49.70475
19
     50.80952
                                       50.43115
                                                   50.85393
                                                              50.65908
                                                                         51.09189
20
21
     52.15410
53.50476
                51.21412
52.70677
                                                                         52.42607
53.74335
                            53.14416
                                       51.71141
                                                   52.56783
                                                              52.11801
                            54.52255
                                                   54.28099
                                       53.00125
                                                              53.59063
                            55.92007
57.32649
22
23
     54.86678
                 54.19272
                                       54.32115
55.68107
                                                   55.95852
                                                              55.07734
                                                                         55.05410
     56.24691
                                                                         56.36708
                 55.68706
                                                   57.56377
                                                              56.56141
                                       57.07179
     57.65227
                            58.72204
                 57.20468
                                                   59.05227
                                                              58.01044
24
                                                                         57.68737
                            60.08033
                 58.75322
25
     59.08792
                                       58.46702
                                                   60.39359
                                                              59.39129
                                                                         59.01492
                 60.32924
                                       59.84426
26
27
                            61.37740
     60.55314
                                                   61.59141
                                                              60.69360
                                                                         60.34549
                 61.90186
                            62.60467
                                       61.21830
     62.03783
                                                   62.68290
                                                              61.94729
                                                                         61.67567
                            63.77926
                63.43474
64.89890
28
     63.52013
                                       62.66274
                                                   63.730B1
                                                              63.22243
                                                                          63.01344
                            64.95067 64.27496
66.23377 66.02238
29
      64.96509
                                                   64.82433
                                                              64.60675
                                                                         64.40053
     66.31626 66.27991
                                                  66.14606
                                                              66.12327
```

#### Conversion of WK Raw Test Scores to 1980 Unrounded Standard Score Equivalents

Baw	15G	20A	20B	21A	218	224	22B
0	16.03719	16.42861	16.45135	16.13752	16.03736	16.01020	15.85413
1	17.34762	17.78688	17.81240	17.46021	17.34782	17.32632	17.14220
2	18.68217	19.20040	19.21230	18.82903	18.68242	18.65437	10.41410
3	20.02500	20.60255	20.62226	20.21372	20.02532	19.98928	19.68065
4	21.37103	22.04227	22.07070	21.60452	21.37142	21.32684	20.94496
5	22.71858	23.50683	23.54458	22.99825	22.71906	22.66566	22.20829
6	24.06698	24.98832	25.03578	24.38081	24.06754	24.00518	23.47104
7	25.41590	26.48174	26.53918	25.74642	25.41654	25.34512	24.73344
8	26.76514	27.95156	28.01707	27.11297	26.76587	26.68534	25. <b>9956</b> 3
9	28.02004	29.28012	29.51118	28.50765	28.03126	28.14085	27.42234
10	29.24157	30.52154	30.98398	29.94035	29.22530	29.65044	28.99431
11	30. <b>51196</b>	31.75197	32.45045	31.39759	30.43399	31.16307	30.61743
12	31.82764	32.97045	33.92026	32.86818	31.70 <b>984</b>	32. <b>6957</b> 3	32.24477
13	33.1 <b>659</b> 7	34 . 17757	35.3 <b>8748</b>	34.33589	33.0 <b>005</b> 2	34.22436	33.83480
14	34.58174	35 <sub>.</sub> 37573	36.83779	35.78205	34 . 5 <b>8584</b>	35.72126	35.40214
15	36.00494	36 . 5 <b>688</b> 2	38.25087	37. <b>1893</b> 1	36.16047	37.16217	36. <b>91289</b>
16	37. <b>4199</b> 5	37. <b>7613</b> 6	39.60646	38.54547	37.75603	38.53224	38.34489
17	38. <b>82</b> 431	38.95742	40.89121	39. <b>8456</b> 0	39.34003	39. <b>8289</b> 7	39.69132
18	40.20817	40.15970	42.10265	41.09202	40.85558	41.06087	40. <b>9595</b> 5
19	41.56188	41.36914	43.24883	42.29241	42.26738	42.24342	42.16610
20	42.87672	<b>42.585</b> 03	44.34451	43.45687	43.56914	43.39435	43.33079
21	44.15449	43.80376	<b>45.406</b> 10	44.59549	44.77829	44.52965	44.47200
22	45.3 <b>96</b> 45	45.01115	46.44798	45.71663	45.92435	45.66170	45.60406
23	46.60699	46.22160	47.44454	46.82656	47.03824	46.79081	46.73681
24	47.79195	47.43414	48.44385	47.92995	48.14606	47.94588	47.87632
25	48.95242	48.64892	49.45703	49.03088	<b>49.26690</b>	49.10541	49.02612
26	50.09425	49.86752	50.48311	50.11635	50.41246	50.27621	50.17638
27	51.24339	51.0 <b>931</b> 5	51. <b>51244</b>	51.21768	51. <b>58649</b>	51. <b>45368</b>	51.34529
28	52.41285	52.33067	52.54110	52.34750	52.78228	52. <b>6493</b> 3	52.53601
29	53 . <b>61668</b>	53. <b>5861</b> 3	53. <b>5889</b> 2	53. <b>5166</b> 2	54.00263	53 . <b>8597</b> 0	53 . <b>7400</b> 3
30	54.86814	<b>54 . 8654</b> 5	54.66371	54.73662	55.23 <b>6</b> 69	55.08101	54.90052
31	56.17527	56.17188	55.7 <b>8584</b>	56.01626	56.48817	56.30 <b>9</b> 73	56.23187
32	57.53310	57.50 <b>234</b>	56. <b>988</b> 62	57.35504	57.75720	57.54357	57.4 <b>992</b> 2
33	58.91394	58 . <b>8427</b> 6	58.31100	58.73434	59.05101	58.78309	58.77798
34	60.25754	60.1 <b>6239</b>	59.7 <b>642</b> 3	60.10782	60.34121	60.03435	60.06141
35	<b>61.4592</b> 3	61.40240	61.24335	61.36661	61 . <b>4985</b> 5	61.3 <b>158</b> 6	61.33930

#### Conversion of PC Raw Test Scores to 1980 Unrounded Standard Score Equivalents

Raw	15G	20A	20B	21A	21B	22A	22B
0	16.87800	17.74411	16.70272	16.57687	17.48701	16.84402	17.91502
1	19.78418	20.86358	19.56573	19.40888	20.54316	19.74182	21.07657
2	22.61058	24.13180	22.30271	22.08167	23.68023	22.55089	24.43198
3	25.41758	27.43620	25.00905	24.71573	26.83699	25.33838	27.72301
4	28.21129	30.14343	27.68983	27.13869	29.69224	28.16565	30.88016
5	30.80825	32.83856	30.11776	29.44794	32.52641	30.93565	34.17280
6	33.27385	35.67195	33.01228	32.04753	35.44123	33.82882	37.37751
7	35.81754	38.63253	36.47500	34.95562	38.45389	36.86399	40.36813
8	38.57550	41.61454	40.14427	38.17095	41.47969	39.94501	43.15466
ğ	41.45566	44.47886	43.81707	41.59641	44.42804	42.96623	45.81685
10	44.33192	47.16593	47.24736	45.10604	47.27934	45.89793	48.38909
11	47.19690	49.72706	50.33738	48.58468	50.06668	48.76685	50.80936
12	50.17183	52.28909	53.14200	51.94322	52.82528	51.60197	53.25720
13	53.37785	55.01109	55.80656	55.21571	55.57198	54.39467	55.76763
14	56.75338	58.00048	58.49925	58.30370	58.32051	57.16113	58.39201
15	60.18763	61.16030	61.36069	61.32077	61.19720	60.24030	61.22918

## Conversion of NO Raw Test Scores to 1980 Unrounded Standard Score Equivalents Without Linkage to Answer Sheet Calibration

```
    0
    15.54694
    15.40206
    15.40206
    15.49707
    15.49707
    15.44852
    15.44852

    1
    16.48229
    16.28219
    16.41341
    16.41341
    16.34635
    16.34635

    2
    17.42453
    17.12877
    17.12877
    17.32274
    17.32274
    17.22362
    17.22362

    3
    18.36811
    17.96887
    17.96887
    18.23070
    18.23070
    18.09690
    18.09690

    4
    19.31215
    18.80673
    18.80673
    19.13819
    19.13819
    18.96881
    18.96881

    5
    20.25641
    19.62589
    19.62589
    20.04547
    20.04547
    19.84009
    19.84009
```

Raw	15G	204	20B	218	21B	224	22B
6	21.20078	20.43725	20.43725	20.95263	20.95263	20.71102	20.71102
7	22.14521	21.25618	21.25618	21.85972	21.85972	21.58175	21.58175
8 9	23.08969 24.03421	22.07956 22.90576	22.07956 22.90576	22.76677 23.67378	22.76677 23.67378	22.44908 23.30887	22.44908 23.30887
10	24.97874	23.73386	23.73388	24.58077	24.58077	24.17091	24.17091
ii	25.92330	24.56334	24.56334	25.48775	25.48775	25.03455	25.03455
12	26.80661	25.48029	25.48029	26.41378	26.41378	25.92156	25.92156
13	27.64144	26.50457	26.50457	27.36400	27.36400	26 . <b>88244</b>	26.88244
14	28.50168	27.56742	27.56742	28.31824	28.31824	27.90650	27.90650
15	29.38835	28.63614 29.70753	28.63614 29.70753	29.2 <b>89</b> 18 30.2 <b>83</b> 27	29.2 <b>8918</b> 30.2 <b>8</b> 327	28.96864	28.96864
16 17	30.30007 31.23343	30.77723	30.77723	31.30104	31.30104	30.03020 31.09487	30.03020 31.0 <b>948</b> 7
ié	32.18368	31.81827	31.81827	32.33832	32.33832	32.14843	32.14843
19	33.14576	32.84706	32.84706	33.38799	33.38799	33.18127	33.18127
20	34.11505	33.86773	33.86773	34.44186	34.44186	34.18900	34.18900
21	35.08781	34.88090	34.88090	35.48055	35.48055	35.1 <b>718</b> 3	<b>35.1718</b> 3
22	36.06135	35. <b>887</b> 59	35.88759	36.50160	36.50160	36.13314	36.13314
23	37.03387	36.88886	36. <b>68886</b>	37.51404	37.51404	37.07796	37.07796
24 25	38.00427 38.97188	37. <b>88</b> 550 38. <b>87794</b>	37.88550 38.87794	38.51607 39.50700	38.51607 39.50700	38.01181 38.93987	38.01181 38.93987
26	39.93624	39.86612	39.86612	40.48695	40.48695	39. <b>86644</b>	39. <b>8664</b> 4
27	40.89693	40.84967	40.84967	41.45667	41.45667	40.79475	40.79475
28	41.85347	41.82792	41.82792	42.41720	42.41720	41.72674	41.72674
29	42.80532	42.80018	42.80018	43.36972	43.36972	42.66306	42.66306
30	43.75192	43.76573	43.76573	44.31524	44.31524	43.60302	43.60302
31 32	44.69246 45.62669	44.72257 45.67444	44.72257 45.67444	45.2 <b>546</b> 2 46.1 <b>884</b> 5	45.25462 46.18845	44.54485 45.48602	44.54485
33	46.55531	46.62248	46.62248	47.11723	47.11723	46.42368	45.48602 46.42368
34	47.47842	47.56860	47.56860	48.04148	48.04148	47.35527	47.35527
35	48.39645	48.51543	48.51543	48.96198	48.96198	48.27898	48.27898
36	49.31007	49.46616	49.46616	49.88002	49.88002	49.19412	49.19412
37	50.22069	50.42432	50.42432	50.79756	50.79756	50.10118	50.10118
38	51.12982	51.39350	51.39350	51.71734	51.71734	51.00182	51.00182
39 40	52.03896	52.37662 53.37495	52.37662 53.37495	52.64278 53.57744	52.64278 53.57744	51.89863 52.79494	51.89863 52.79494
41	52.94956 53.86292	54.38630	54.38630	54.52385	54.52385	53.69442	53.69442
42	54.77998	55.40258	55.40258	55.48106	55.48106	54.60071	54.60071
43	55.70090	56.40752	56.40752	56.44115	56.44115	55.51651	55.51651
44	56.62433	57.37631	57.37631	57.38589	57.38589	56.44210	56.44210
45	57.54654	58.28064	58.28064	58.28726	58.28726	57.37360	57.37360
46	58.46063	59.10092	59.10092	59.11690	59.11690	58.30181	58.30181
47 48	59.35716 60.22661	59. <b>84249</b> 60. <b>54351</b>	59. <b>8424</b> 9 60.5 <b>43</b> 51	59. <b>8655</b> 0 60. <b>5607</b> 2	59. <b>865</b> 50 60.56072	59.21414 60.10144	59.21414 60.10144
49	61.06361	61.22172	61.22172	61.22505	61.22505	60.96783	60.96783
50	61.86973	61.90331	61.90331	61.90083	61.90083	61.83761	61.83761

# Conversion of CS Raw Test Scores to 1980 Unrounded Standard Score Equivalents Without Linkage to Answer Sheet Calibration

Raw	15G	204	20B	214	21B	22A	22B
0	21.52204	21.55967	21.55967	21.49453	21.52401	21.53872	21.53872
1	22.08792	22.14026	22.14026	22.04967	22.09067	22.11112	22.11112
2	22.63186	22.70942	22.70942	22.57518	22.63594	22.66623	22.66623
3	23.17162	23.27640	23.27640	23.09504	23.17712	23.21805	23.21805
4	23. <b>70992</b>	23.84262	23. <b>8426</b> 2	23.57531	23.7 <b>169</b> 0	23.76873	23.76873
5	24.23328	24.40851	24.40851	24.07079	24.24497	24.31890	24.31890
6	24.75498	24.97420	24.97420	24.57385	<b>24.7680</b> 0	24.86481	24.86481
7	<b>25.2814</b> 0	25.5 <b>3978</b>	25.53978	25.08087	<b>25.2958</b> 2	25.40300	25.40300
8	25.81059	<b>26.10529</b>	26.10529	25.59021	25.82644	25. <b>944</b> 23	<b>25.94423</b>
9	26.34155	<b>26.67066</b>	26.67066	26.10103	<b>26.3588</b> 5	26.48741	<b>26.4874</b> 1
10	26.87371	27.23064	27.23064	26.60138	26.89247	27.03189	27.03189
11	27.40671	27.79165	27.79165	27.10043	27.42694	27.57731	<b>27.5773</b> 1
12	27.94033	28.35342	28.35342	27.60271	27.96204	28.12341	28.12341
13	28.47441	28.91577	28.91577	28.10735	28.49761	28.67002	28.67002
14	28.97788	29.47289	29.47289	28.66773	29.06059	29.2 <b>58</b> 57	29.25857
15	29.47238	30.03 <del>95</del> 6	30.03 <b>9</b> 56	<b>29.29511</b>	29.65936	29. <b>8927</b> 5	29. <b>892</b> 75
16	29. <b>987</b> 50	30. <b>62924</b>	30.62924	29.95355	30.27277	30. <b>53564</b>	30.53 <b>564</b>
17	30.51731	31. <b>2396</b> 0	31.2 <b>396</b> 0	30.63024	30. <b>892</b> 57	31.18206	31.18206
18	31.06025	31.87216	31. <b>872</b> 16	31.32071	31.52258	31.83493	31.83493
19	31.61865	32.52826	32.5 <b>282</b> 6	32.02750	32.16612	32. <b>49</b> 671	32.49671

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Raw	15G	208	20B	218	21B	22A	22B
20	32.19487	33.20875	33.20875	32.74185	32.82590	33.16926	33.16926
21	32.79111	33.90653	33.90653	33.47310	33.50378	33.85159	33.85159
22	33.40920	34 . 62358	34.62358	34.22125	34.20061	34.53940	34.53940
23	34.05026	35.35918	35.35918	34 . 98373	34.91608	35.23678	35.23678
24	34.71445	36.10919	36.10919	35.74456	35.64599	35.94131	35.94131
25	35.40073	36.86313	36.86313	36.50573	36.37877	36.64969	36. <b>6496</b> 9
26	36.10675	37.60894	37.60894	37.26490	37.11942	37.35804	37.35804
27	36.82736	38.35084	38.35084	38.01542	37.86329	38.05637	38.05637
28	37.54722	39.08386	39.00306	38.7 <b>389</b> 5	38.60524	38.74142	38.74142
29	38.27120	39. <b>80294</b>	39.80294	39.44663	39.32568	39.41543	39.41543
30	38.99420	40.49432	40.49432	40.13635	40.03633	40.07630	40.07630
31	39.71147	41.16992	41.16992	40.80728	40.73492	40.72284	40.72284
32	40.41579	41.82967	41.82967	41.45963	41.42010	41.35470	41.35470
33	41.09860	42.47428	42.47428	42.09448	42.09138	41.97228	41.97228
34	41.76825	43.10508	43.10508	42.71357	42.74904	42.57662	42.57662
35	42.42417	43.72377	43.72377	43.31902	43.39170	43.16915	43.16915
36	43.06651	44.33227	44.33227	43.91314	44.02105	43.75161	43.75161
37	<b>43.69600</b>	44 . 93254	44.93254	44.4 <b>982</b> 3	44.64196	44.32582	44.32582
38	44.31377	45.52646	<b>45.5264</b> 6	45.07648	45.2 <b>558</b> 9	44.89361	44.89361
39	44.92117	46.11581	46.11581	45.64 <del>99</del> 0	45.86428	45.45673	45.45673
40	45.51967	46.70222	46.70222	46.22028	46.46853	46.01676	46.01676
41	46.11079	47.28714	47.28714	46.78916	47.06992	46.57517	46.57517
42	46.69593	47.87183	47.87183	47.35787	47.66968	47.13323	47.13323
43	47.27645	48.45743	48.45743	47.92756	48.26889	47.69208	47.69208
44	47.85359	49.04492	49.04492	48.49922	48.86856	48.25271	48.25271
45	48.42844	49.63515	49.63515	49.07369	49.46958	48.81601	48.81601
46	49.00198	50.22887	50.22887	49.65170	50.07274	49.38275	49.38275
47	49.57511	50.82665	50.82665	50.23388	50.67870	49.95358	49.95358
48	50.14862	51.42898	51.42898	50.82079	51.28802	50.52898	50.52898
49	50.72319	52.03616	52.03616	51.41285	51.90110	51.10942	51.10942
50	51.29944	52.64834	52.64834	52.01037	52.51815	51.69546	51.69546
51	51.87790	53.26544	53.26544	52.61354	53.13921	52.28698	52.28698
52	52.45894	53.88717	53.88717	53.22234	53.76411	52.88364	52.88364
53	53.04289	54.51301	54.51301	53.83659	54.39242	53.48489	53.48489
54	53.62986	55.14221	55.14221	54.45584	55.02350	54.08997	54.08997
55	54.21982	55.77379	55.77379	55.07946	55.65648	54.69791	54.69791
56	54.81256	56.40660	56.40660	55.70656	56.29029	55.30770	55.30770
57	55.40764	57.03938	57.03938	56.33604	56.92377	55.91867	55.91867
58	56.00440	57.67081	57.67081	56.96665	57.55565	56.52905	56.52905
59	56.60201	58.30049	58.30049	57.59705	58.18469	57.13752	57.13752
60	57.19945	58.92803	58.92803	58.22586	58.80977	57.74298	57.74298
61	57.79557	59.55095	59.55095	58.85180	59.42993	58.34450	58.34450
62	58.38913	60.16860	60.16860	59.47376	60.04448	58.94155	58.94155
63	58.97888	60.78070	60.78070	60.09203	60.65304	59.53395	59.53395
64	59.56361	61.38739	61.38739	60.70527	61.25556	60.12197	60.12197
65	60.14218	61.98927	61.98927	61.31243	61.85236	60.70631	60.70631
66	60.71361	62.58740	62.58740	61.91351	62.44407	61.28813	61.28813
67	61.27705	63.18326	63.18326	62.50888	63.03164	61.86901	61.86901
68	61.83573	63.77884	63.77884	63.09929	63.61631	62.45251	62.45251
69	62.38763	64.37653	64.37653	63.68584	64.19955	63.03939	63.03939
70	62.93230	64.97907	64.97907	64.27000	64.78299	63.63178	63.63178
71	63.47018	65.58931	65.58931	64.85356	65.36836	64.23200	64.23200
72	64.00209	66.20965	66.20965	65.43989	65.95719	64.84227	64.84227
73	64.52949	66.84112	66.84112	66.02972	66.55049	65.46751	65.46751
74	65.05475	67.48183	67.48183	66.62398	67.14804	66.10960	66.10960
75	65.58170	68.12486	68.12486	67.22312	67.74737	66.76606	66.76606
76	66.11630	68.75639	68.75639	67.82585	68.34249	67.43217	67.43217
77	66.66736	69.35560	69.35560	68.42784	68.92282	68.09829	68.09829
78	67.24699	69.89914	69.89914	69.02053	69.47356	68.74931	68.74931
79	67.87014	70.37237	70.37237	69.59074	69.97932	69.36625	69.36625
80	68.55193	70.78016	70.78016	70.12281	70.43232	69.93170	69.93170
81	69.30156	71.10572	71.10572	70.60496	70.84370	70.43910	70.43910
82	70.11245	71.41065	71.41065	71.03950	71.19578	70.90280	70.90280
83	70.93228	71.63953	71.63953	71.45138	71.52689	71.34303	71.34303
84	71.67150	71.88218	71.88218	71.81321	71.84001	71.77268	71.77268

## Conversion of AS Raw Test Scores to 1980 Unrounded Standard Score Equivalents

Raw	15G 24 . 24820	20A 23.98878	209 23.98878	21 <u>A</u> 23 . 73053	21 <u>8</u> 23 . 73053	22A 24 . 01244	22B 24 .01244
0 1	26.05558	25.76372	25.76372	25.47317	25.47317	25.7 <del>9</del> 033	25.79033
2	20.03330 27. <b>8728</b> 2	27.49115	27.49115	27.11120	27.11120	27.52595	27.52595
3	29.69342	29.20242	29.20242	28.71364	28.71364	29.24720	29.24720
4	31.51531	30.90747	30.90747	30.06295	30.06295	30.96291	30.96291
5	33.48424	32.73432	32.73432	31.70401	31.70401	32.78815	32.78815
6	35.53017	34.57209	34.57209	33.44998	33.44998	34.66564	34.66564
7	37.55505	36.39416	36.39416	35.28970	35.28970	36.59378	36.59378
é	39.52092	38.18534	38.18534	37.21560	37.21560	38.54380	38.54380
9	41.39533	39.94095	39.94095	39.19109	39.19109	40.47151	40.47151
10	43.21146	41.67194	41.67194	41.16872	41.16872	42.33922	42.33922
ii	44.97440	43.40200	43.40200	43.11539	43.11539	44.12939	44.12939
12	46.69551	45.16303	45.16303	45.01814	45.01814	45.84344	45.84344
13	48.39344	46.99079	46.99079	46.90243	46.90243	47.49506	47.49506
14	50.08492	48.91577	48.91577	48.77569	48.77569	49.10632	49.10632
15	51.78196	50.94551	50.94551	50.63625	50.63625	50.70625	50.70625
16	53.49429	53.04764	53.04764	52.47018	52.47018	52.32586	52.32586
17	55.22564	55.15193	55.15193	54.25840	54.25840	53.98732	53.98732
18	56.97043	57.18092	57.18092	55.99108	55.99108	55.69488	55.69488
19	58.71587	59.08809	59.08809	57.67861	57.67861	57.43292	57.43292
20	60.45018	60.87386	60.87386	59.35305	59.35305	59.18229	59.18229
21	62.17278	62.57443	62.57443	61.07195	61.07195	60.94110	60.94110
22	63.90245	64.24240	64.24240	62.88112	62.88112	62.73611	62.73611
23	65.67589	65.93059	65.93059	64.80823	64.80823	64.61600	64.61600
24	67.51643	67.66660	67.66660	66.85254	66.85254	66.62622	66.62622
25	69.34479	69.39836	69.39836	68. <b>94</b> 223	68.94223	68.81634	68.81634

#### Conversion of MK Raw Test Scores to 1980 Unrounded Standard Score Equivalents

Raw	15G	20A	20B	218	21B	223	22B
0	28.79944	28.7 <b>584</b> 0	28.91140	28.62819	28.63338	29.46237	29.21225
1	30.37034	30.32213	30.50185	30.16918	30.17528	31.11880	30.85525
2	31.95057	31. <b>8852</b> 0	32.1 <b>2894</b>	31.67775	31.68602	32.81149	32.60824
3	33.53351	33.44807	33.76663	33.17694	33.1 <b>877</b> 5	34.54794	34.30823
4	35.01 <b>8</b> 03	35.1 <b>562</b> 2	35.3 <b>9</b> 126	34.88609	34 . 90366	36.20146	35.96702
5	36.45125	36. <b>8253</b> 2	36. <b>96261</b>	36.59361	36.61542	37.72928	37.57352
6	37. <b>8796</b> 0	38.40034	38.52940	38.21970	38.19901	39.17858	39.15959
7	39.30550	39.93504	40.11149	39. <b>8313</b> 0	39.69943	40.58687	40.74316
8	40.73446	41.47448	41.71707	41.46455	41.16188	41.97064	42.33150
9	42.17915	43.05038	43.34782	43.13362	42.62684	43.36542	43.92191
10	43.65680	44.67419	44.99906	44.83053	44.12817	44.78772	45.50391
11	45.18228	46.32966	46.66010	46.52658	45.68605	46.22809	47.06449
12	46.76105	47.97754	48.31710	48.18311	47.30022	47.67310	48.59434
13	48.38547	49.57666	49.95817	49.76867	48.95307	49.10776	50.09126
14	50.03884	51.10655	51.57779	51.27156	50.62253	50.52049	51.55952
15	51.70216	52.57521	53.17516	52.70081	52.29485	51.90663	53.00684
16	53.36028	54.01043	54.75060	54.07873	53.96789	53.26939	54.44502
17	55.00447	55.44481	56.30070	55.43277	55.64355	54.61921	55.87885
18	56.63152	56.90089	57.81550	56.79068	57.31524	55.97921	57.30801
19	58.24145	58.37807	59.28006	58.17744	58.95811	57.36703	58.72637
20	59.83532	59.84855	60.68334	59.60937	60.53380	58.79834	60.12526
21	61.41433	61.27463	62.01875	61.08580	62.01564	60.28503	61.50044
22	62.98073	62.64578	63.30741	62 58781	63.42137	61.82948	62.86041
23	64.54070	64.00576	64.59681	64.09482	64.82077	63.43091	64.23124
24	66.11014	65.47025	65.95673	65.62559	66.29819	65.12037	65.66922
25	67.74255	67.28684	67.57153	67.40261	67.85483	67.07131	67.40674

#### Conversion of MC Raw Test Scores to 1980 Unrounded Standard Score Equivalents

Dane	15G	20 <b>A</b>	20B	21A	218	225	22B
Raw	123				21B	221	448
0	23. <b>2713</b> 6	23. <b>588</b> 11	23.58811			23.1 <b>659</b> 7	23.16597
1	25.1 <b>052</b> 0	25.46768	25.46768	24.89014	24.89014	24.98458	24.98458
2	26.88192	27.36337	27.36337	26.5 <b>96</b> 30	26.59630	26.72173	26.72173
3	28.64052	29.26416	29.26416	28.27053	26.27053	28.43301	28.43301
4	30.3 <b>9226</b>	31.16690	31.16690	29.79674	29.79674	30.13451	30.13451
•	22 14022	22 88061	22 00061	21 <b>68</b> 016	21 <i>C</i> 001E	32 ACE3A	22 06520

Raw	15G	20A	20B	21A	21B	22A	22B
6	33.81222	34.55 <b>98</b> 7	34.55987	33.39263	33.39263	33.9 <del>299</del> 9	33.9 <del>299</del> 9
7	35.37803	36.26301	36.26301	35.02143	35.02143	35.73977	35.73977
8	37.01454	37.98569	37. <b>9856</b> 9	36.65323	36.65323	37.51073	37.51073
9	38.69640	39.72777	39.72777	38.32408	38.32408	39.26745	39.26745
10	40.40599	41.49148	41.49148	40.05649	40.05649	41.06378	41.0637B
11	42.13857	43.27988	43.27988	41.86170	41.86170	42.90404	42.90404
12	43.89918	45.09701	45.09701	43.73464	43.73464	44.78403	44.78403
13	45.70080	46.94859	46.94859	45.65702	45.65702	46.69527	46.69527
14	47.56269	48.84152	48.84152	47.60955	47.60955	48.63178	48.63178
15	49.50738	50.78102	50.78102	49.58389	49.58389	50.59452	50.59452
16	51.55470	52.76504	52.76504	51.58458	51.58458	52.59058	52.59058
17	53.71075	54.77886	54.77886	53.61993	53.61993	54.62228	54 . 62228
18	55.95399	56.79435	56.79435	55.68590	55.68590	56.67336	56.67336
19	58.22959	58.77900	58.77900	57.75410	57.75410	58.70864	58.70864
20	60.46504	60.71213	60.71213	59.77805	59.77805	60.68869	60.68869
21	62.60458	62.59750	62.59750	61.72315	61.72315	62.59533	62.59533
22	64.64233	64.46341	64.46341	63.60062	63.60062	64.44857	64.44857
23	66.60920	66.35193	66.35193	65.47568	65.47568	66.30553	66.30553
24	68.53920	68.29815	68.29815	67.43545	67.43545	68.23986	68.23986
25	70.39131	70.25777	70.25777	69.70615	69.70615	70.22830	70.22830

## Conversion of Raw EI Test Scores to 1980 Unrounded Standard Score Equivalents

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Raw	15G	20A	20B	21A	21B	22A	22B
0	<b>22.08362</b>	22.36199	22.36199	22.32777	22.32777	22.48844	22.48844
1	24.33328	24.66273	24.66273	24.62223	24.62223	24.81238	24 81238
2	26.43345	26.88274	26.88274	26.82751	26.82751	27.08682	27.08682
3	28.35786	29.0 <b>799</b> 6	29.07996	29.00761	29.00761	29.34729	29.34729
4	30.62847	31.38164	31.38164	31.41497	31.41497	31.81506	31.81506
<b>4</b> 5	33.13286	33.70604	33.70604	33.86816	33.86816	34.22581	34.22581
ĕ	35.69909	36.04048	36.04048	36.29964	36.29964	36.50515	36.50515
ž	38.31327	38.41933	38.41933	38.74936	38.74936	38.75724	38.75724
é	41.07538	40.86223	40.86223	41.24003	41.24003	41.07552	41.07552
9	43.90635	43.34468	43.34468	43.74798	43.74798		
		••••			· · - · - ·	43.49391	43.49391
10	46.66490	45.80785	45.80785	46.21451	46.21451	45.97281	45.97281
11	49.24618	48.19922	48.19922	48.58860	48.58860	48.43487	48.43487
12	51.63949	50. <b>5037</b> 3	50.50373	50. <b>85944</b>	50. <b>85944</b>	50. <b>8236</b> 1	50. <b>8236</b> 1
13	53.90111	52.74096	52.74096	53.05319	53. <b>05319</b>	53.13005	53.13005
14	56.09285	54.94101	54.94101	55.20753	55.20753	55.37446	55.37446
15	58.23888	57.12111	57.12111	57.34618	57.34618	57.57238	57.57238
16	1723 ق	59.27564	59.27564	59.46294	59.46294	59.71419	59.71419
17	62.29207	61.45345	61.45345	61.55569	61.55569	61.77566	61.77566
18	64 . 17696	63.65869	63.65869	63.68364	63.68364	63.85321	63.85321
19	66.24488	65.98744	65.98744	65.89629	65.89629	66.08959	66.08959
20	68.64922	68.54096	68.54096	68.40442	68.40442	68.57597	68.57597
Z-U	00.0 <b>174</b> 4	ロロ・コマリフロ	90.3 <b>4</b> 030	00.3U394	DD. TUTTA	00.3/33/	00.3/37/

## Conversion of Raw VE Test Scores to 1980 Unrounded Standard Score Equivalents

Raw	15G	20A	20B	21A	21B	224	22B
0	1 <b>4 . 862</b> 87	<b>15.2338</b> 3	14.91123	14.81379	14.84415	14.76109	14 . <b>8269</b> 6
1	15.81132	16.21635	15.86412	15.75774	15.7 <b>908</b> 9	15. <b>7002</b> 0	15.77212
2	16.7 <b>6978</b>	17.20711	16. <b>8366</b> 5	16.70191	16.74389	16.62904	16.72012
3	17.73216	18.22746	17.81688	17.64618	17.69937	17.55385	17.66925
4	18.69611	19.27609	18.80019	18.59048	18.65582	18.47705	18.61882
5	19.66082	20.34410	19.78500	19.53480	19.61275	19.39947	19.56861
6	20.62595	21.42560	20.77063	20.47912	20.56995	20.32145	20.51852
7	21.59134	22.51678	21.75677	21.42346	21.52731	21.24318	21.46850
	22.55690	23.61507	22.74323	22.36779	22.48477	22.16473	22.41853
8 9	23.52257	24.71873	23.72993	23.31213	23.44231	23.08616	23.36860
10	24.48832	25.78608	24.71679	24.25647	24.39990	24.00750	24.31869
iĭ	25.45415	26.86019	25.69440	25.20081	25.35753	24.92878	25.26879
12	26.42601	27.95670	26.67185	26.14516	26.31519	25.85001	26.21891
13	27.31598	28.98894	27.66691	27.12827	27.21383	26.82666	27.29398
14	28.19110	29.93425	28.70006	28.15017	28.11959	27.85889	28.52244
15	29.10260	30.85231	29.75185	29.18407	29.11149	28.93043	29.78101
16	30.04099	31.74414	30.81554	30.22351	30.1 <b>8394</b>	30.03276	31.0 <b>8</b> 002
17	30. <b>996</b> 33	32.61455	31.88332	31.26061	31.31471	31.15178	32.35716
18	31.95886	33.47015	32.94826	32.28585	32.43 <del>9</del> 37	32.27124	33.55504
19	32.92041	34.31755	34.00529	33.28769	33.55580	33.35079	34.69325
20	33.87549	35.16233	35.05156	34.27567	34.64733	34.40964	35.76514
21	34.82148	36.00139	36.04038	35.25016	35.70546	35.44423	36.77465

Raw	150	204	20B	214	218	228	229
22	35. <b>7582</b> 6	36.83628	37.09162	36.21277	36.73068	36.45394	37.73165
23	36.68736	37.67944	38.09366	37.16550	37.72890	37.44021	38.64816
24	37.61106	38.53135	39.0 <b>859</b> 6	38.11019	38.70789	38.40539	39.53579
25	38.53175	39.39154	40.06724	39.04817	39.67457	39.35202	40.40456
26	39.45134	40.25902	41.03561	39. <b>98</b> 019	40.63336	40.28243	41.26231
27	40.37096	41.13246	41.90009	40.90632	41.58553	41.19862	42.11472
28.	41.29082	42.01038	42.92513	41.82624	42.52940	42.10231	42.96535
29	42.21012	42.89131	43.84304	42.73935	43.46133	<b>42.995</b> 16	43.81578
30	43.12727	43.77380	44.74241	43.64506	44.37724	43.87882	44.66601
31	44.04015	44 . 65656	45.62404	44 . 54298	45.27425	44 . 75500	45.51485
32	44 . <b>946</b> 66	45.53845	46.48954	45.42571	46.15189	45.62540	46.35050
33	45. <b>845</b> 13	46.41666	47.33614	46.30033	47.01252	46.49158	47.17710
34	46.73466	47.28494	48.16162	47.16825	<b>47.86091</b>	47.35200	47.99809
35	47.61542	48.15036	48.97679	48.03131	48.70311	48.20256	48.81345
36	48.48857	49.01310	49.78340	48.89162	49.54530	49.05310	49.62435
37	49.35612	49.87356	50. <b>582</b> 17	49.75136	<b>50.3927</b> 3	49.90453	50.43260
38	50. <b>2209</b> 3	50.73243	51.37302	<b>50.61276</b>	51.24892	50.75728	51.24070
39	51.08118	51.59088	52.15561	51.47818	52.11501	51.61145	52.04900
40	51. <b>9485</b> 6	52.45085	52.92475	52.35038	52. <b>98</b> 687	52.46705	52.86163
41	52. <b>8298</b> 8	53.31552	53. <b>68874</b>	53.23276	53.86332	53.32438	53.69006
42	53.73047	54.18960	54 . 45553	54 . 12932	54.73827	54.18429	54.53726
43	54.65487	55.07 <b>92</b> 7	55.23194	55.04417	55.60464	55.04847	55.40445
44	55. <b>6054</b> 7	55. <b>991</b> 31	56.02819	55. <b>980</b> 38	56 . 45915	55. <b>9193</b> 0	56.2 <b>89</b> 67
45	56.58057	56.93104	56 . <b>85</b> 651	56 . <b>938</b> 26	57.30558	56.79948	57.18699
46	57.57288	57. <b>8999</b> 5	57.72910	57. <b>9142</b> 3	58.15613	<b>57.69296</b>	58.08717
47	58.570 <b>8</b> 0	58. <b>89</b> 377	58.65402	58.90109	59.02 <b>948</b>	58.60348	58.98105
48	59.56409	59. <b>9031</b> 1	59.62540	59 . <b>8909</b> 5	59. <b>945</b> 62	59.53615	59.86480
49	60.5 <b>558</b> 6	60.91737	60. <b>64257</b>	60.88147	60.916 <b>9</b> 6	60.50427	60.75197
50	61. <b>6469</b> 0	61.93385	61.74924	61.89548	61.93109	61.57779	61.74949

# Conversion of NO Raw Test Scores to 1980 Unrounded Standard Score Equivalents After Linkage to Answer Sheet Calibration

Raw	15G	208	20B	21A	21B	223	22B
0	15. <b>60598</b>	15.44527	15.44527	15.55226	15.55226	15.49758	15.49758
1	16. <b>5679</b> 5	16.36168	16.36168	16.49656	16.49656	16.42764	16.42764
2	17.55321	17.24384	17.24384	17.44663	17.44663	17.34300	17.34300
3	18.54276	18.12403	18.12403	18.39859	18.39859	18.25829	18.25829
4	19.53378	19.00318	19.00318	19.35113	19.35113	19.17332	19.17332
5	20.52548	19.86327	19 86327	20.30392	20.30392	20.08822	20.08822
6	21.51753	20.71545	20.71545	21.25685	21.25685	21.00304	21.00304
7	22.50981	21.57575	21.57575	22.20985	22.20985	21.91780	21.91780
8	23.50224	22.44083	22.44083	23.16291	23.16291	22.82910	22.82910
9	24.49390	23.30896	23.30896	24.11601	24.11601	23.73255	23.73255
10	25.47935	24.17915	24.17915	25.06564	25.06564	24.63690	24 . 63690
11	26.43564	25.04740	25.04740	26.00511	26.00511	25.53699	25.53699
12	27.28283	25.99740	25.99740	26 . <b>89828</b>	26.89828	26.43399	26.43399
13	28.14349	26.98392	26.98392	27.85367	27.85367	27.36049	27.36049
14	29.08506	28.06257	28.06257	28.88347	28.88347	28.43330	28.43330
15	30.10912	29.24035	29.24035	29.99459	29.99459	29.62437	29.62437
16	31.20460	30.49192	30.49192	31.18439	31.18439	30.88002	30.88002
17	32.35480	31.79206	31.79206	32.43876	32.43876	32.16389	32.18389
18	33.54048	33.08437	33.08437	33.72829	33.72629	33.49649	33.49649
19	34.70768	34.34556	34.34556	34.99918	34.99918	34.75041	34.75041
20	35.87381	35.5 <b>765</b> 0	35. <b>5765</b> 0	36.26576 37.51065	36.26576	35. <b>9625</b> 0	35. <b>9625</b> 0
21	37.04026	36.79230	36.79230	38.73461	37.51065	37.14089	37.14089
22	38.20658	37. <b>99818</b> 39.1 <b>976</b> 1	37. <b>99818</b> 39.1 <b>976</b> 1	39.93438	38.73461 39.93438	38.29268	38.29268
23	39. <b>3685</b> 0	40.37291	40.37291	41.11949	41.11949	39.42047 40.52246	39.42047
24 25	40.51353 41.66140	41.54947	41.54947	42.29896	42.29896	41.62326	40.52246
25 26	42.81191	42.72805	42.72805	43.47053	43.47053	42.72844	41.62326 42.72844
26 27	43.96080	43.90429	43.90429	44.63003	44.63003	43.83861	43.83861
28	45.09799	45.06785	45.06785	45.76218	45.76218	44.94853	44.94853
29	46.21429	46.20830	46.20830	46.87107	46.87107	46.04857	46.04857
30	47.31266	47.32862	47.32862	47.96266	47.96266	47.14062	47.14062
31	48.39484	48.42933	48.42933	49.03811	49.03811	40.22572	48.22572
32	49.46154	49.51588	49.51588	50.10040	50.10040	49.30145	49.30145
33	50.51643	50.59262	50.59262	51.15371	51.15371	50.36716	50.36716
33 34	51.56337	51. <b>6656</b> 6	51.66566	52.20220	52.20220	51.42369	51.42369
35	52.60543	52.74057	52.74057	53.24806	53.24806	52.47198	52.47198
36	53.64418	53.82181	53.82181	54.29168	54.29168	53.51223	53.51223
20	27.64470	23.02101	33.02707	34.53700	34 - 53100	JJ.J1243	33.31443

Raw	15G	203	20B	21A	21B	228	22B
37	54.67553	54 . 90498	54 . 904 98	55.32210	55.32210	54.54087	54.54087
38	55.68380	55.97085	55.97085	56.31701	56.31701	55.54445	55.54445
39	56.64270	56.98463	56. <b>9846</b> 3	57.24481	57.24481	56.50059	56.50059
40	57. <b>52113</b>	57.90429	57. <b>90429</b>	58.07528	58.07528	57.38186	57.38186
41	58.29717	58.703 <b>9</b> 8	58.703 <b>98</b>	58.7 <b>96</b> 16	58.7 <b>96</b> 16	58.16620	58.16620
42	58. <b>961</b> 77	59.3 <b>564</b> 5	59.35645	59.39775	59.39775	58.84586	58.84586
43	59.51347	59.87726	59.87726	59.89306	59.89306	59.41642	59.41642
44	59.97913	60.31897	60.31897	60.32278	60.32278	59.89351	59.89351
45	60.3 <b>866</b> 9	60.67300	60. <b>6730</b> 0	60.67540	60.67540	60.31789	60.31789
46	60.73837	60.97374	60.97374	60.96029	60.98029	60.68068	60.68068
47	61.07878	61.27773	61.27773	61.28717	61.28717	61.02016	61.02016
48	61.41786	61.52662	61.52662	61.53253	61.53253	61.37489	61.37489
49	61.72097	61.78988	61.78988	61.79133	61.79133	61.67923	61.67923
50	62.07560	62.09239	62.09239	62.09115	62.09115	62.05954	62.05954

# Conversion of CS Raw Test Scores to 1980 Unrounded Standard Score Equivalents After Linkage to Answer Sheet Calibration

Raw	15G	20A	20B	21A	21B	22A	22B
0	21.50235	21.53661	21.53661	21.47731	21.50415	21.51754	21.51754
ĭ	22.02907	22.07796	22.07796	21.99335	22.03164	22.05074	22.05074
2	22.53475	22.60676	22.60676	22.48212	22.53853	22.56666	22.56666
2		23.13297	23.13297				
3	23.03573			22.96467	23.04084	23.07883	23.07883
4	23.53524	23.65837	23.65037	23.41034	23.54171	23.58981	23.58981
4 5 6	24.02082	24.18339	24.18339	23.87007	24.03166	24.10025	24.10025
7	24.50483	24.70821	24.70821	24.33679	24.51692	24.60673	24.60673
	24.99306	25.23238	25.23238	24.80717	25.00641	25.10569	25 . 10569
8	25.48319	25.75599	25.75599	25.27908	25.49786	25.60690	25.60690
9	25.97470	26.27948	26.27948	25.75204	25.99071	26.10977	26.10977
10	26.46754	26.79818	26.79818	26.21532	26.48491	26.61406	26.61406
11	26.96130	27.31798	27.31798	26.67755	26.98005	27.11936	27.11936
12	27.45575	27.85094	27.85094	27.14289	27.47587	27.62541	27.62541
13	27.97092	28.41891	28.41891	27.61053	27.99392	28.16487	28.16487
14	28.48461	29.00992	29.00992	28.16260	28.57210	28.78151	28.78151
15	29.00 <b>938</b>	29.61845	29.61 <b>84</b> 5	28.82017	29.20 <b>989</b>	29.46019	29.46019
16	29. <b>562</b> 13	30.25691	30.25691	29.52540	29.87074	30.15512	30.15512
17	30.13529	30.92117	30.92117	30. <b>258</b> 00	30.54355	30. <b>858</b> 61	30. <b>8586</b> 1
18	30. <b>7260</b> 5	31. <b>60838</b>	31.60838	31.00936	31.22886	31. <b>568</b> 06	31. <b>5680</b> 6
19	31.33331	32.31 <b>87</b> 6	32.31 <b>87</b> 6	31.77659	31. <b>9267</b> 0	32. <b>284</b> 61	32. <b>2846</b> 1
20	31.95783	33.05489	33.05489	32.54995	32.64091	<b>33.01221</b>	33. <b>01221</b>
21	32.60326	33. <b>8082</b> 1	33. <b>8082</b> 1	33.34061	33.37377	33.7 <b>489</b> 6	33. <b>7489</b> 6
22	33.27155	34.58012	34.58012	34.14738	34.12518	34.48958	34.48958
23	33. <b>96323</b>	35.3 <b>69</b> 17	35. <b>3691</b> 7	34.96667	34.89413	35.23804	35.23804
24	34.67787	36.17024	36.17024	35.78113	35.67576	35. <b>99136</b>	35.99136
25	35.41358	36.97235	36.97235	36.59274	36.45748	36.74566	36.74566
26	36.16764	37.76278	37.76278	37.39854	37.24452	37.49715	37.49715
27	36.93436	38.54606	38.54606	38.19215	38.03157	38.23537	38.23537
28	37.69743	39.31706	39.31706	38.95455	38.81381	38.95715	38.95715
29	38.46213	40.07109	40.07109	39.69787	39.57091	39.66512	39.66512
30	39.22294	40.79322	40.79322	40.42001	40.31547	40.35732	40.35732
31	39.97532	41.49514	41.49514	41.11891	41.04384	41.03131	41.03131
32	40.71135	42.17880	42.17880	41.79545	41.75449	41.68674	41.68674
33	41.42115	42.84580	42.84580	42.45285	42.44964	42.32642	42.32642
34	42.11517	43.49766	43.49766	43.09310	43.12976	42.95157	42.95157
35	42.79395	44.13632	44.13632	43.71853	43.79356	43.56381	43.56381
36	43.45784	44.76385	44.76385	44.33163	44.44292	44.16503	44.16503
37	44.10768	45.38236	45.38236	44.93487	45.08298	44.75720	44.75720
38	44.74478	45.99387	45.99387	45.53058	45.71532	45.34228	45.34228
39	45.37066	46.60025	46.60025	46.12088	46.34147	45.92211	45.92211
40	45.98689	47.20321	47.20321	46.70766	46.96293	46.49837	46.49837
41	46.59508	47.80427	47.80427	47.29254	47.58107	47.07259	47.07259
42	47.19674	48.40477	48.40477	47.87691	48.19716	47.64613	47.64613
43	47.79330	49.00587	49.00587	48.46197	48.81234	48.22017	48.22017
44	48.38604	49.60859	49.60859	49.04874	49.42766	48.79573	48.79573
45	48.97611	50.21381	50.21381	49.63808	50.04403	49.37375	49.37375
46	49.56454	50.82228	50.82228	50.23076	50.66227	49.95499	49.95499
47	50.15224	51.43460	51.43460	50.82742	51.28306	50.54015	50.54015
48	50.74003	52.05124	52.05124	51.42860	51.90693	51.12969	51.12969
49	51. 1863	52.67249	52.67249	52.03473	52.53430	51.72409	51.72409
50	51. 863	53.29846	53.29846	52.64611	53.16535	52.32390	52.32390
J-0	J	22.27040		~2.04011	JJ . 10JJJ	JE.JEJ90	JE. JEJ 30

Dave	15G	204	20B	21A	21B	22A	22B
Raw 51	52.51056	53.92905	53.92905	53.26289	53.80009	52.92897	52.92897
52	53.10481	54.56391	54.56391	53.88504	54.43829	53.53892	53.53892
53	53.70166	55.20246	55.20246	54.51230	55.07949	54.15316	54.15316
53 54	54.30120	55.84387	55.84387	55.14417	55.72294	54.77085	54.77085
55 55	54.90337	56.48705	56.48705	55.77994	56.36767	55.39099	55.39099
56	55.50788	57.13074	57.13074	56.41863	57.01253	56.01244	56.01244
57	56.11424	57.77358	57.77358	57.05902	57.65623	56.63447	56.63447
58	56.72171	58.41409	58.41409	57.69976	58.29738	57.25520	57.25520
59	57.32936	59.05175	59.05175	58.33933	58.93459	57.87320	57.87320
60	57.93606	59.68601	59.68601	58.97624	59.56659	58.48723	58.48723
61	58.54054	60.31417	60.31417	59.60903	60.19225	59.09628	59.09628
62	59.14144	60.93542	60.93542	60.23640	60.81070	59.69965	59.69965
63	59.73735	61.54926	61.54926	60.85848	61.42137	60.29704	60.29704
64	60.32693	62.15561	62.15561	61.47370	62.02401	60.88856	60.88856
65	60.90887	62.75481	62.75481	62.08078	62.61868	61.47474	61.47474
66	61.48205	63.34761	63.34761	62.67948	63.20575	62.05652	62.05652
67	62.04546	63.93516	63.93516	63.26990	63.78589	62.63523	62.63523
68	62.60214	64.51900	64.51900	63.85249	64.35996	63.21411	63.21411
69	63.14989	65.10100	65.10100	64.42799	64.92902	63.79352	63.79352
70	63.68809	65.68325	65.68325	64.99748	65.49421	64.37509	64.37509
71	64.21696	66.26780	66.26780	65.56225	66.05667	64.96055	64.96055
72	64.73714	66.85612	66.85612	66.12502	66.61730	65.55135	65.55135
73	65.24964	67.44826	67.44826	66.68591	67.17638	66.15141	66.15141
74	65.75621	68.04146	68.04146	67.24512	67.73300	66.76148	66.76148
75	66.26053	68.62848	68.62848	67.80239	68.28426	67.37804	67.37804
76	66.76782	69.19592	69.19592	68.35582	68.82421	67.99557	67.99557
יין	67.28570	69.72618	69.72618	68.90093	69.34331	68.60425	68.60425
78	67.82444	70.20026	70.20026	69.42984	69.82907	69.18964	69.18964
79	68.39620	70.61313	70.61313	69.93127	70.27021	69.73547	69.73547
вó	69.01249	70.96570	70.96570	70.39539	70.66543	70.22866	70.22866
81	69.67873	71.24576	71.24576	70.81499	71.02035	70.67135	70.67135
82	70.38636	71.50475	71.50475	71.18879	71.32232	71.07120	71.07120
83	71.09656	71.69907	71.69907	71.53933	71.60343	71.44733	71.44733
84	71.72621	71.90294	71.90294	71.84525	71.86766	71.81134	71.81134

## Appendix G:

#### Distributions of Composites by ASVAB Form After Conversion Using Recommended Equatings

#### AFOT PERCENTILE COMPOSITE

Percentages	At	or	Above	Cut	Scores	(Ordered	High	to	Low)
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Test	Cut Score									
	93.00	65.00	50.00	31.00	21.00	16.00_	10.00			
REF	5.07	35.95	57.62	80.91	91.39	94.53	97.76			
15G	4.12	37.04	57.26	80.81	91.31	94.69	97.91			
20A	4.91	36.54	57.43	81.86	91.94	94.67	97.59			
20B	5.99	36.79	56.76	81.01	91.97	95.02	97.89			
21A	5.20	35.73	56.72	81.52	91.87	95.01	97.76			
21B	5.48	35.87	57.56	81.86	92.21	95.24	97.94			
22A	6.07	36.87	57.15	81.20	91.54	94.58	97.59			
22B	5.24	36.06	57.27	81.12	91.85	95.08	97.89			

#### AFOT PERCENTILE COMPOSITE

#### Differences in Percentages At or Above Cut Scores (Test-REF)

Test				Cut Score					
	93.00	65.00	50.00	31.00	21.00	16.00	10.00		
15G	-0.96	1.09	-0.36	-0.10	-0.08	0.16	0.15		
20A	-0.16	0.58	-0.20	0.95	0.54	0.14	-0.16		
20B	0.92	0.84	-0.B6	0.10	0.58	0.49	0.13		
21A	0.13	-0.22	-0.90	0.61	0.48	0.48	0.00		
21B	0.41	-0.08	-0.06	0.95	0.81	0.71	0.19		
22A	0.99	0.92	-0.47	0.29	0.15	0.05	-0.17		
22B	0.17	0.11	-0.35	0.22	0.46	0.54	0.13		

#### AIR FORCE M PERCENTILE COMPOSITE

Test				Cut Score				
	89.00	61.00	57.00	51.00	45.00	44.00		
REF	9.83	43.98	49.55	56.17	62.58	63.10		
15G	9.71	44.29	49.11	<b>55.6</b> 3	62.25	63.49		
20A	9.03	45.3B	50.81	57.23	64.05	65.09		
20B	8.84	44.55	49.51	56.17	62.75	63.73		
21A	8.41	43.54	49.52	56.14	62.71	63.60		
21B	7.73	43.85	50.29	57.26	64.20	65.26		
22A	9.47	44.70	49.49	56.01	62.44	63.96		
22B	9.63	44.08	48.70	55.31	62.06	63.64		

#### AIR FORCE M PERCENTILE COMPOSITE

## Differences in Percentages At or Above Cut Scores (Test-REF)

Test		Out Score									
	89.00	61.00	57.00	51.00	45.00	44.00					
15G	-0.12	0.31	-0.44	-0.54	-0.33	0.40					
20A	-0.80	1.40	1.27	1.07	1.47	1.99					
20B	-0.99	0.57	-0.03	0.01	0.17	0.64					
21A	-1.42	-0.44	-0.03	-0.03	0.13	0.50					
21B	-2.10	-0.13	0.74	1.10	1.63	2.16					
22A	-0.36	0.72	-0.06	-0.15	-0.14	0.86					
22B	-0.20	0.10	-0.85	-0.86	-0.52	0.54					

#### AIR FORCE A PERCENTILE COMPOSITE

#### Percentages At or Above Cut Scores (Ordered High to Low)

Test	Cut Score									
	67.00	61.00	51.00	45.00	40.00	32.00	27.00			
REF	40.62	47.77	61.32	69.43	74.62	83.40	88.60			
15G	40.58	47.59	61.01	68.89	74.34	83.30	88.81			
20A	40.59	47.77	61.62	69.62	74.58	82.79	88.16			
20B	40.93	47.99	61.55	69.27	74.64	83.11	88.35			
21A	40.72	47.57	61.39	69.50	74.89	83.16	88.86			
21B	40.02	47.35	60.54	68.63	74.30	83.47	88.60			
22A	40.95	47.97	61.03	68.87	74.46	82.92	88.14			
22B	40.30	47.41	60.98	69.41	74.60	83.32	88.36			

#### AIR FORCE A PERCENTILE COMPOSITE

#### Differences in Percentages At or Above Cut Scores (Test-REF)

Test				Cut Score					
	67.00	61.00	51.00	45.00	40.00	32.00	27.00		
15G	-0.04	-0.18	-0.31	-0.54	-0.28	-0.10	0.21		
20A	-0.03	-0.00	0.30	0.19	-0.04	-0.61	-0.44		
20B	0.31	0.22	0.23	-0.16	0.02	-0.2 <del>9</del>	-0.25		
21A	0.10	-0.20	0.08	0.07	0.27	-0.25	0.26		
21B	-0.59	-0.41	-0.78	-0.80	-0.32	0.06	-0.00		
22A	0.33	0.20	-0.29	-0.56	-0.16	-0.48	-0.46		
22B	-0.32	-0.36	-0.34	-0.02	-0.02	-0.08	-0.24		

#### AIR FORCE G PERCENTILE COMPOSITE

Test				Out Sec	re								
				58.00									
REF	31.03	31.03	38.88	44.57	47.00	52.46	57.62	60.26	65.24	67.60	72.09	76.03	82.57
15G	31.67	31.67	39.66	44.32	47.03	52.11	57.26	59.85	64.48	66.92	71.15	75.67	62.38
20A	31.62	31.62	39.25	44.07	46.69	51.80	57.43	59.47	64.81	66.94	72.14	76.16	83.35
20B	31.47	31.47	39.26	44.01	46.94	51.72	56.76	59.44	64.02	66.42	70.91	75.45	82.92
21A				44.13									
21B				44.17									
22A				44.80									

#### AIR FORCE G PERCENTILE COMPOSITE, Con't.

228 31.31 33.31 38.70 43.88 46.60 51.88 57.27 59.96 64.82 67.39 71.34 75.76 82.98 Differences in Percentages At or Above Cut Scores (Test-REF)

Test				Out Sec	TO								
	70.00	69.00	64.00	58.00	56.00	53.00	50.00	48.00	43.00	42.00	39.00	35.00	30.00
15G 20A 208 21A 21B 22A 22B	0.64 0.59 0.44 -0.23 -0.13 0.90 0.29	0.64 0.59 0.44 -0.23 -0.13 0.90 0.29	0.76 0.36 0.38 -0.45 -0.14 0.64	-0.25 -0.50 -0.56 -0.44 -0.40 0.23 -0.68	-0.06 -0.42 -0.10 0.44	-0.34 -0.66 -0.73 -0.66 0.12 0.05 -0.58	-0.20 -0.86 -0.90 -0.06 -0.47	-0.25	-0.43 -1.21	-0.06 -0.74	-1.18 -0.63 -0.09 -0.93	0.14 -0.50 -0.22 0.12 -0.45	-0.19 0.78 0.35 0.67 0.94 0.16 0.41

#### AIR FORCE E PERCENTILE COMPOSITE

Percentages At or Above Out Scores (Ordered High to Low)

Test				Out See	EG						
	81.00	77.00	72.00	67.00	58.00	50.00	46.00	45.00	43.00	39.00	33.00
REF	16.96	21.59		34.94			62.98		67.96	72.62	80.10
15G	16. <b>62</b>	21.24	27.46	34.13	46.26				67.52	72.14	79.73
20A	17.48	22.26	28.55	35.44	47.31	57.94	63.04	64.30	67.82	72.73	80.18
208	17.94	22.65		35.11					67.55	72.26	79.64
21A	16.75	21.63	27.93	34.01	46.12	58.04	62.95	64.17	67.63	72.34	79.97
213	16.30	21.31	27.31	34.34	47.30	58.62	63.65	64.03	68.90	73.62	<b>81.21</b>
22A	16.46	21.43	27.93	35.06	47.07	50.45	63.36	64.40	67.58	72.13	79.82
229	17.09	21.93	28.06	34.70	46.99	58.25	63.06	64.25	67.07	72.80	80.20

#### AIR FORCE E PERCENTILE COMPOSITE

Differences in Percentages At or Above Cut Scores (Test-REP)

Test				Out Score							
	81.00	77.00	72.00	67.00	58.00	50.00	46.00	45.00	43.00	39.00	33.00
15G	-0.34	-0.36	-0.48	-0.80	-0.56	-0.33	-0.30	-0.22	-0.44	-0.49	-0.38
20A	0.53	0.67	0.61	0.50	0.49	0.19	0.06	0.13	-0.14	0.10	0.08
200	0.98	1.06	0.55	0.17	-0.02	0.35	-0.03	-0.05	-0.41	-0.37	-0.46
21A	-0.21	0.04	-0.01	-0.93	-0.70	0.29	-0.03	0.01	-0.33	-0.28	-0.13
21B	-0.57	-0.28	-0.64	-0.60	0.48	0.87	0.67	0.67	0.94	1.00	1.11
22A	-0.50	-0.16	-0.01	0.14	0.25	0.70	0.36	0.23	-0.38	-0.49	-0.28
228	0.14	0.34	0.12	-0.24	0.17	0.49	0.10	0.09	-0.09	0.18	0.10

#### ARMY GT STANDARD SCORE COMPOSITE

Percentages At or Above Cut Scores (Ordered High to Low)

	_
Test	Cut Score 110.00
REF	38.88
15G	39.66
20A	39.25
20B	39.26
21A	38.43
21B	38.75
22A	39.52
22B	38.70

#### ARMY GT STANDARD SCORE COMPOSITE

Differences in Percentages At or Above Cut Scores (Test-REF)

Test	Cut 8	Score 00
15G 20A	0.° 0.°	. •

#### ARMY GT STANDARD SCORE COMPOSITE, Con't.

```
20B 0.38
21A -0.45
21B -0.14
22A 0.64
22B -0.18
```

#### ARMY GM STANDARD SCORE COMPOSITE

Percentages At or Above Cut Scores (Ordered High to Low)

```
Test ----- Cut Score -----
       105.00 100.00 95.00 90.00 85.00
REF
       46.48 58.49 68.11
                             78.28 85.96
       45.55 57.21 67.25
15G
                             78.46 86.64
       47.18 59.40 69.24
20A
                             78.90 86.49
20B
       46.86 58.52 68.00
                             78.46 85.80
       45.85 58.09 68.82
21A
                             79.36
                                    86.86
       46.59 58.98 69.71
46.72 58.08 68.41
46.41 58.07 68.59
21B
                             80.07
                                    87.70
                             78.14 86.00
78.68 86.26
22A
22B
```

#### ARMY CM STANDARD SCORE COMPOSITE

Differences in Percentages At or Above Cut Scores (Test-REF)

Test		a				
	105.00	100.00	95.00	90.00	85.00	
15G	-0.92	-1.28	-0.86	0.18	0.67	
20A	0.70	0.92	1.14	0.61	0.53	
20B	0.38	0.04	-0.11	0.17	-0.16	
21A	-0.63	-0.40	0.72	1.08	0.89	
21B	0.11	0.49	1.60	1.78	1.74	
22A	0.24	-0.41	0.30	-0.15	0.04	
22B	-0.06	-0.41	0.48	0.40	0.29	

#### ARMY EL STANDARD SCORE COMPOSITE

Test			(	Out Scor	æ			
	120.00	115.00	110.00	105.00	100.00	95.00	90.00	85.00
REF	17.95	26.88	36.22	46.82	57.75	67. <del>9</del> 6	77.95	86.39
15G	17.45	26.37	35.17	46.26	57.42	67.52	77.48	86.37
20A	18.57	27.43	36.44	47.31	<b>57.94</b>	67.82	78.22	86.38
20B	18.73	27.50	36.12	46.80	58.11	67.55	77.69	85.89
21A	17.71	26.91	35.17	46.12	58.04	67.63	77.69	86.63
21B	17.43	26.14	35.60	47.30	58.62	68.90	79.04	87.74
22A	17.28	26.77	36.41	47.07	58.45	67.58	77.76	86.19
22B	17.92	27.05	35.75	46.99	58.25	67.87	78.11	86.90

#### ARMY EL STANDARD SCORE COMPOSITE

Differences in Percentages At or Above Cut Scores (Test-REF)

Test				Cut Score				
	120.00	115.00	110.00	105.00	100.00	95.00	90.00	85.00
15G	-0.50	-0.51	-1.05	-0.56	-0.33	-0.44	-0.47	-0.02
20A	0.62	0.54	0.21	0.49	0.19	-0.14	0.27	-0.01
20B	0.78	0.62	-0.11	-0.02	0.35	-0.41	-0.26	-0.50
21A	-0.24	0.03	-1.06	-0.70	0.29	-0.33	-0.26	0.24
21B	-0.52	-0.75	-0.63	0.48	0.87	0.94	1.09	1.36
22A	-0.67	-0.11	0.18	0.25	0.70	-0.38	-0.19	-0.20
22B	-0.03	0.17	-0.47	0.17	0.49	-0.09	0.16	0.51

#### ARMY CL STANDARD SCORE COMPOSITE

Percentages At or Above Cut Scores (Ordered High to Low)

Test	Out Score								
	110.00	105.00	100.00	95.00	90.00	85.00			
REF	39.32	51.13	61.35	72.32	80.06	86.77			
15G	39.80	51.14	61.34	72.26	80.60	87.14			
20A	39.60	50.92	60.96	71.79	80.42	87.43			
20B	39.10	50.64	60.57	71.56	80.05	87.14			
21A	39.00	50.62	60.87	71.86	80.26	87.43			
21B	38.72	50.97	61.85	72.77	81.18	88.01			
22A	39.65	51.38	61.11	72.12	80.14	87.13			
22B	39.26	51.08	61.24	71.71	80.42	87.19			

#### ARMY CL STANDARD SCORE COMPOSITE

Differences in Percentages At or Above Cut Scores (Test-REF)

Test	Cut Score								
	110.00	105.00	100.00	95.00	90.00	85.00			
15G	0.47	0.02	-0.01	-0.06	0.54	0.37			
20A	0.28	-0.21	-0.39	-0.53	0.36	0.66			
20B	-0.23	-0.48	-0. <b>78</b>	-0.76	-0.00	0.37			
21A	-0.33	-0.50	-0.48	-0.47	0.20	0.66			
21B	-0.60	-0.16	0.50	0.45	1.12	1.24			
22A	0.33	0.26	-0.24	-0.20	0.09	0.36			
22B	-0.07	-0.04	-0.11	-0.61	0.36	0.42			

#### ARMY MM STANDARD SCORE COMPOSITE

Test			Score - 95.00	
REF		60.24		80.79
15G	47.62	58.89		81.42
20A	50.13	61.61	72.64	81.87
20B	49.95	60.95	71.90	81.05

#### ARMY MM STANDARD SCORE COMPOSITE, Con't.

21A	49.37	60.60	71.87	81.69
21B	49.89	61.29	73.28	81.81
22A	49.24	60.40	71.99	80.87
22B	49.71	60.00	72.26	81.08

#### ARMY MM STANDARD SCORE COMPOSITE

#### Differences in Percentages At or Above Cut Scores (Test-REF)

Test		Cut	Score -	
	105.00	100.00	95.00	90.00
15G	-1.81	-1.34	-0.40	0.63
20A	0.69	1.37	0.64	1.08
20B	0.52	0.71	-0.11	0.26
21A	-0.06	0.37	-0.13	0.90
21B	0.46	1.05	1.27	1.02
22A	-0.19	0.16	-0.01	0.08
22B	0.28	-0.23	0.25	0.29

## ARMY SC STANDARD SCORE COMPOSITE

#### Percentages At or Above Cut Scores (Ordered High to Low)

Test		Cut	Score -	
	105.00	100.00	95.00	90.00
REF	49.86	59.96	70.50	79.47
15G	49.75	60.23	70.97	80.27
20A	50.78	60.82	71.05	80.18
20B	49.62	59.84	70.28	79.29
21A	49.55	59.87	70.66	80.39
21B	50.82	61.17	72.11	81.30
22A	50.36	60.64	70.81	79.64
22B	50.05	59.74	70.20	79.51

#### ARMY SC STANDARD SCORE COMPOSITE

#### Differences in Percentages At or Above Cut Scores (Test-REF)

Test		Cut	Score -	
	105.00	100.00	95.00	90.00
15G	-0.10	0.27	0.47	0.81
20A	0.93	0.86	0.56	0.71
20B	-0.24	-0.12	-0.21	-0.18
21A	-0.31	-0.09	0.16	0.92
21B	0.96	1.21	1.61	1.83
22A	0.51	0.69	0.31	0.17
22B	0.20	-0.22	-0.30	0.04

#### ARMY CO STANDARD SCORE COMPOSITE

Percentages At or Above Cut Scores (Ordered High to Low)

Test	Cut Score					
	100.00	95.00	90.00	85.00		
REF	60.61	70.94	80.21	87.67		
15G	61.37	71.78	80.98	88.41		
20A	61.49	72.02	80.86	87.86		
20B	61.17	71.29	80.25	87.67		
21A	61.00	71.76	80.93	88.52		
21B	62.41	72.81	81.85	89.17		
22A	61.41	71.51	80.86	88.26		
22B	61.03	70.85	80.48	88.15		

#### ARMY CO STANDARD SCORE COMPOSITE

Differences in Percentages At or Above Cut Scores (Test-REF)

Test		Cut	Score	
	100.00	95.00	90.00	85.00
15G	0.75	0.85	0.77	0.74
20A	0.87	1.09	0.65	0.19
20B	0.55	0.36	0.04	0.00
21A	0.38	0.82	0.72	0.85
21B	1.80	1.87	1.64	1.51
22A	0.80	0.57	0.65	0.59
22B	0.42	-0.08	0.27	0.48

#### ARMY FA STANDARD SCORE COMPOSITE

Percentages At or Above Cut Scores (Ordered High to Low)

Test	Cut Score						
	100.00	95.00	90.00	85.00			
REF	61.71	72.98	81.90	89.07			
15G	62.09	73.80	82.47	89.53			
20A	61.77	73.20	81.63	88.68			
20B	61.50	73.26	81.97	88.85			
21A	61.93	73.31	82.13	88.91			
21B	62.65	73.75	82.93	89.67			
22A	62.22	73.42	82.19	89.14			
22B	61.82	73.24	82.59	89.48			

## ARMY FA STANDARD SCORE COMPOSITE

Differences in Percentages At or Above Cut Scores (Test-REF)

Test		Cut	Score		
	100.00	95.00		85.00	
15G	0.38	0.82	0.58	0.46	
20A	0.06	0.22	-0.27	-0.39	
20B	-0.22	0.28	0.07	-0.22	
21A	0.22	0.33	0.23	-0.16	
21B	0.94	0.77	1.03	0.60	

## ARMY FA STANDARD SCORE COMPOSITE, Con't.

22A 0.50 0.44 0.29 0.07 22B 0.10 0.26 0.69 0.40

#### ARMY OF STANDARD SCORE COMPOSITE

Percentages At or Above Cut Scores (Ordered High to Low)

Test		Cut	Score	
	105.00	100.00	95.00	90.00
REF	53.10	64.78	75.52	84.67
15G	52.38	65.26	76.55	86.19
20A	54.20	65.97	75.96	84.94
20B	53.18	64.96	74.97	84.56
21A	53.00	65.29	76.18	85.60
21B	53.22	65.66	76.88	86.21
22A	53.69	65.26	75.47	85.18
22B	52.84	64.46	75.41	84.95

#### ARMY OF STANDARD SCORE COMPOSITE

Differences in Percentages At or Above Cut Scores (Test-REF)

Test	105.00	Cut 100.00	Score 95.00	90.00
15G 20A 20B 21A 21B 22A 22B	-0.72 1.09 0.07 -0.10 0.11 0.58 -0.26	0.47 1.19 0.17 0.51 0.88 0.48 -0.32	1.03 0.44 -0.54 0.66 1.37 -0.04	1.51 0.26 -0.11 0.93 1.54 0.51 0.28

#### ARMY ST STANDARD SCORE COMPOSITE

Test			(	out Scor	e		
	115.00	110.00	105.00	110.00	95.00	90.00	85.00
REF	27.46	39.07	50.83	61.09	71.90	81.34	88.11
15G	28.28	39.56	51.16	61.52	72.96	82.35	89.27
20A	28.44	39.50	50.87	61.25	71.83	81.03	88.39
20B	28.20	38.82	50.73	60.88	71.40	80.75	88.29
21A	27.96	38.80	50.15	60.49	71.57	81.18	88.68
21B	28.13	39.40	50.85	61.25	72.31	82.14	89.09
22A	28.25	39.96	51.85	61.83	71.92	81.00	88.16
22B	28.07	39.05	51.09	61.69	72.39	81.18	88.47

#### ARMY ST STANDARD SCORE COMPOSITE

Differences in Percentages At or Above Cut Scores (Test-REF)

Test			(	Out Scor	<b>e</b>		
	115.00	110.00		110.00	95.00	90.00	85.00
15G	0.82	0.49	0.33	0.44	1.05	1.01	1.16
20A	0.98	0.43	0.04	0.16	-0.07	-0.31	0.27
20B	0.74	-0.25	-0.10	-0.21	-0.51	-0.59	0.18
21A	0.50	-0.26	-0.68	-0.59	-0.34	-0.16	0.56
21B	0.67	0.33	0.01	0.17	0.40	0.80	0.97
22A	0.79	0.89	1.02	0.74	0.02	-0.34	0.05
22B	0.61	-0.02	0.26	0.60	0.49	-0.16	0.35

## MARINE CORPS MM STANDARD SCORE COMPOSITE

Percentages At or Above Cut Scores (Ordered High to Low)

		Score	
115.00	105.00	95.00	85.00
27.12	47.26	66.91	83.90
25.98	46.35	65.82	84.74
26.80	47.92	67.56	85.01
26.27	46.97	66.61	84.25
26.38	47.04	66.49	84.73
26.45	48.22	68.37	85.73
27.05	47.49	66.84	83.99
26.59	47.62	66.86	84.62
	27.12 25.98 26.80 26.27 26.38 26.45 27.05	115.00 105.00 27.12 47.26 25.98 46.35 26.80 47.92 26.27 46.97 26.38 47.04 26.45 48.22 27.05 47.49	115.00 105.00 95.00 27.12 47.26 66.91 25.98 46.35 65.82 26.80 47.92 67.56 26.27 46.97 66.61 26.38 47.04 66.49 26.45 48.22 68.37 27.05 47.49 66.84

#### MARINE CORPS MM STANDARD SCORE COMPOSITE

Differences in Percentages At or Above Cut Scores (Test-REF)

Test		Cut	Score	
	115.00	105.00	95.00	85.00
15G	-1.14	-0.91	-1.09	0.84
20A	-0.32	0.66	0.65	1.11
20B	-0.85	-0.29	-0.29	0.35
21A	-0.74	-0.22	-0.42	0.83
21B	-0.67	0.96	1.47	1.83
22A	-0.07	0.23	-0.07	0.09
22B	-0.53	0.37	-0.05	0.72

#### MARINE CORPS CL STANDARD SCORE COMPOSITE

Test	Cut Score				
			101.00		
REF	17.25	42.00	66.82	86.43	95.78
15G	18.44	43.10	67.94	87.16	96.06
20A	17.42	41.84	66.27	86.44	95.61
20B	18.02	42.15	66.80	86.67	95.92

#### MARINE CORPS CL STANDARD SCORE COMPOSITE, Con't.

21A	17.23	41.84	66.62	87.09	95.96
21B	17.19	41.57	66.96	87.26	96.00
22A	17.83	42.23	66.46	86.21	95.62
22B	17.02	41 75	66 90	86 76	95 81

#### MARINE CORPS CL STANDARD SCORE COMPOSITE

#### Differences in Percentages At or Above Cut Scores (Test-REF)

Test	Cut Score				
	120.00	110.00	101.00	90.00	80.00
15G	1.19	1.10	1.11	0.73	0.28
20A	0.16	-0.16	-0.55	0.01	-0.17
20B	0.77	0.15	-0.02	0.24	0.15
21A	-0.03	-0.16	-0.20	0.66	0.18
21B	-0.06	-0.43	0.13	0.83	0.23
22A	0.58	0.23	-0.36	-0.22	-0.16
22B	-0.23	-0.25	0.08	0.33	0.04

#### MARINE CORPS GT STANDARD SCORE COMPOSITE

#### Percentages At or Above Cut Scores (Ordered High to Low)

Test		Cut	Score	
	110.00	100.00	90.00	80.00
REF	39.56	61.40	79.45	92.48
15G	39.87	61.34	79.95	92.98
20A	40.12	61.07	79.66	92.59
20B	39.47	60.83	79.53	92.66
21A	39.45	61.23	79.51	93.06
21B	40.22	62.31	80.59	93.06
22A	40.21	62.07	79.70	92.60
22B	39.59	61.44	80.17	93.00

#### MARINE CORPS GT STANDARD SCORE COMPOSITE

#### Differences in Percentages At or Above Cut Scores (Test-REF)

Test	110.00	Cut 100.00	Score 90.00	80.00
15G 20 <b>A</b>	0.31 0.56	-0.06 -0.33	0.50 0.21	0.50 0.12
20B	-0.08	-0.56	0.07	0.18
21A	-0.11	-0.17	0.06	0.58
21B	0.67	0.92	1.14	0.58
22A	0.66	0.67	0.25	0.13
22B	0.03	0.05	0.71	0.52

#### MARINE CORPS EL STANDARD SCORE COMPOSITE

Percentages At or Above Cut Scores (Ordered High to Low)

Test		Cut S	Score	
	115.00	110.00	100.00	90.00
REF	25.72	36.22	57.75	77.95
15G	25.31	35.17	57.42	77.48
20A	26.46	36.44	57.94	78.22
20B	26.66	36.12	58.11	77.69
21A	25.61	35.17	58.04	77.69
21B	25.18	35.60	58.62	79.04
22A	25.49	36.41	58.45	77.76
22B	25.91	35.75	58.25	78.11

#### MARINE CORPS EL STANDARD SCORE COMPOSITE

Differences in Percentages At or Above Cut Scores (Test-REF)

Test		Cut S	Score	
	115.00	110.00	100.00	90.00
15G	-0.41	-1.05	-0.33	-0.47
20A	0.74	0.21	0.19	0.27
20B	0.93	-0.11	0.35	-0.26
21A	-0.11	-1.06	0.29	-0.26
21B	-0.54	-0.63	0.87	1.09
22A	-0.23	0.18	0.70	-0.19
22B	0.18	-0.47	0.49	0.16

#### NAVY EL SUM OF SUBTEST STANDARD SCORES COMPOSITE

Percentages At or Above Cut Scores (Ordered High to Low)

Test		Cut 9	Score -	
	218.00	204.00	200.00	190.00
REF	34.94	51.68	56.54	69.22
15G	34.13	51.17	56.21	68.66
20A	35.44	52.31	57.00	69.12
20B	35.11	51.50	57.14	68.63
21A	34.01	51.44	56.69	68.82
21B	34.34	52.27	57.62	70.08
22A	35.08	52.24	57.30	68.71
22B	34.70	52.13	57.04	69.28

#### NAVY EL SUM OF SUBTEST STANDARD SCORES COMPOSITE

Differences in Percentages At or Above Cut Scores (Test-REF)

Test	Cut Score				
	218.00	204.00	200.00	190.00	
15G	-0.80	-0.51	-0.33	-0.56	
20A	0.50	0.63	0.46	-0.11	
20B	0.17	-0.18	0.60	-0.59	
21A	-0.93	-0.24	0.15	-0.41	

#### NAVY EL SUM OF SUBTEST STANDARD SCORES COMPOSITE. Con't.

21B -0.60 0.59 1.08 0.86 22A 0.14 0.56 0.76 -0.52 22B -0.24 0.45 0.50 0.06

#### NAVY E SUM OF SUBTEST STANDARD SCORES COMPOSITE

Percentages At or Above Cut Scores (Ordered High to Low)

Test ----- Cut Score -----214.00 210.00 204.00 200.00 196.00 41.85 46.02 53.24 57.81 62.17 REF 15G 42.50 46.62 52.93 57.81 62.67 42.56 47.01 53.68 58.10 62.65 20A 20B 41.99 46.57 53.33 57.68 62.22 21A 42.12 46.53 53.22 57.55 61.79 42.38 46.76 53.61 58.33 62.67 42.74 47.30 53.88 58.38 62.98 21B 22A 42.24 46.65 53.36 58.48 62.87

#### NAVY E SUM OF SUBTEST STANDARD SCORES COMPOSITE

Differences in Percentages At or Above Cut Scores (Test-REF)

Test ----- Cut Score -----214.00 210.00 204.00 200.00 196.00 0.60 -0.31 -0.00 15G 0.65 0.50 20A 0.71 0.99 0.45 0.28 0.48 20B 0.55 0.09 -0.14 0.14 0.06 0.26 0.51 -0.02 -0.27 21A -0.370.50 0.53 0.37 21B 0.74 0.51 0.64 0.57 0.81 22A 0.89 1.28 22B 0.38 0.12 0.63 0.67 0.70

#### NAVY CL SUM OF SUBTEST STANDARD SCORES COMPOSITE

Percentages At or Above Cut Scores (Ordered High to Low)

Test Cut Score 160.00 REF 50.10 15G 49.68 20A 50.17 20B 50.41 21A 50.03 21B 49.61 22A 50.34 22B 49.80

#### NAVY CL SUM OF SUBTEST STANDARD SCORES COMPOSITE

Differences in Percentages At or Above Cut Scores (Test-REF)

Test	Cut Score
15G	-0.42
20A	0.07
20B	0.31
21A	-0.07
21B	-0.49
22A	0.23
22B	-0.30

#### NAVY GT SUM OF SUBTEST STANDARD SCORES COMPOSITE

Percentages At or Above Cut Scores (Ordered High to Low)

Test			(	Out Scor	e		
	115.00	113.00	108.00	103.00	97.00	96.00	89.00
REF	23.67	28.46	41.72	55.11	69.89	72.09	84.21
15G	24.22	29.18	42.04	54.70	68.95	71.15	83.91
20A	24.04	28.95	41.75	54.30	69.58	72.14	84.77
20B	24.06	29.04	41.47	54.34	68.67	70.91	84.49
21A	23.54	28.33	41.18	54.40	69.24	71.46	84.62
21B	23.31	28.30	41.56	55.12	69.56	72.00	85.20
22A	24.55	29.56	41.94	55.04	69.04	71.16	84.37
22B	23.61	28.90	40.93	54.21	69.47	71.34	84.49

#### NAVY GT SUM OF SUBTEST STANDARD SCORES COMPOSITE

Differences in Percentages At or Above Cut Scores (Test-REF)

Test	Out Score						
	115.00	113.00	108.00	103.00	97.00	96.00	89.00
15G	0.55	0.73	0.32	-0.41	-0.94	-0.94	-0.30
20A	0.37	0.49	0.03	-0.81	-0.31	0.05	0.56
20B	0.39	0.58	-0.25	-0.76	-1.21	-1.18	0.28
21A	-0.13	-0.13	-0.54	-0.70	-0.65	-0.63	0.41
21B	-0.36	-0.16	-0.16	0.02	-0.33	-0.09	0.99
22A	0.88	1.10	0.21	-0.07	-0.84	-0.93	0.17
22B	-0.06	0.44	-0.79	-0.90	-0.42	~0.75	0.28

#### NAVY ME SUM OF SUBTEST STANDARD SCORES COMPOSITE

Test	Cut Score			
	167.00	158.00	150.00	
REF	32.46	46.95	60.30	
15G	31.69	47.38	60.72	
20A	32.78	48.23	61.27	
20B	32.10	47.54	60.18	

#### NAVY ME SUM OF SUBTEST STANDARD SCORES COMPOSITE, Con't.

21A 31.63 46.84 60.29 21B 32.05 47.60 61.14 22A 33.00 47.51 60.30 22B 32.43 47.27 59.89

#### NAVY ME SUM OF SUBTEST STANDARD SCORES COMPOSITE

Differences in Percentages At or Above Cut Scores (Test-REF)

Test ---- Cut Score -----167.00 158.00 150.00 -0.78 15G 0.43 0.41 20A 1.28 0.31 0.96 20B -0.36 0.59 -0.12 21A -0.83 -0.11 -0.02 21B 0.65 -0.420.83 22A 0.53 0.56 -0.00 22B 0.32 -0.03 -0.41

#### NAVY EG SUM OF SUBTEST STANDARD SCORES COMPOSITE

Percentages At or Above Cut Scores (Ordered High to Low)

Test Cut Score 96.00 REF 69.87 15G 70.46 20A 70.12 20B 69.47 21A 70.81 21B 70.90 22A 69.70 22B 69.53

#### NAVY EG SUM OF SUBTEST STANDARD SCORES COMPOSITE

Differences in Percentages At or Above Cut Scores (Test-REF)

Test Cut Score 96.00 0.59 15G 20A 0.24 20B -0.40 0.94 21A 21B 1.03 22Ā -0.17 22B -0.34

#### NAVY CT SUM OF SUBTEST STANDARD SCORES COMPOSITE

Percentages At or Above Cut Scores (Ordered High to Low)

Test Cut Score 202.00 REF 65.51 15G 64.BO 20A 65.54 20B 65.21 21A 65.17 21B 64.80 65.13 65.25 22A 22B

#### NAVY CT SUM OF SUBTEST STANDARD SCORES COMPOSITE

Differences in Percentages At or Above Cut Scores (Test-REF)

Test Cut Score 202.00

15G -0.71
20A 0.03
20B -0.30
21A -0.34
21B -0.71
22A -0.38
22B -0.26

#### NAVY HM SUM OF SUBTEST STANDARD SCORES COMPOSITE

Percentages At or Above Cut Scores (Ordered High to Low)

Test - Cut Score -165.00 149.00 34.67 63.77 35.91 64.04 35.75 63.23 35.44 62.96 REF 15G 20A 20B 21A 35.31 62.54 35.17 63.14 21B 22A 35.86 63.64 22B 35.23 63.57

#### NAVY HM SUM OF SUBTEST STANDARD SCORES COMPOSITE

Differences in Percentages At or Above Cut Scores (Test-REF)

Test - Cut Score - 165.00 149.00

15G 1.24 0.27
20A 1.08 -0.54
20B 0.77 -0.81

#### NAVY HM SUM OF SUBTEST STANDARD SCORES COMPOSITE, Con't.

21A	0.64	-1.23
21B	0.51	-0.63
22A	1.19	-0.13
22B	0.56	-0.20

#### NAVY ST SUM OF SUBTEST STANDARD SCORES COMPOSITE

#### Percentages At or Above Cut Scores (Ordered High to Low)

Test	Cut Score 147.00
REF	98.74
15G	98.86
20A	98.54
20B	98.78
21A	98.62
21B	98.61
22A	98.79
22B	98.65

#### NAVY ST SUM OF SUBTEST STANDARD SCORES COMPOSITE

#### Differences in Percentages At or Above Cut Scores (Test-REF)

Test	Cut Score
15G	0.12
20A	-0.20
20B	0.04
21A	-0.12
21B	-0.13
22A	0.05
22B	-0.09

#### NAVY MR SUM OF SUBTEST STANDARD SCORES COMPOSITE

Test	Cut Score			
	164.00	158.00	130.00	
REF	36.79	45.51	83.68	
15G	36.30	45.41	84.43	
20A	37.05	46.17	84.71	
20B	36.41	45.53	83.97	
21A	36.34	45.31	84.85	
21B	36.53	46.33	85.58	
22A	37.22	46.23	84.49	
22B	36.48	46.03	84.08	

#### NAVY MR SUM OF SUBTEST STANDARD SCORES COMPOSITE

Differences in Percentages At or Above Cut Scores (Test-REF)

Test	Cut Score			
	164.00	158.00	130.00	
15G	-0.49	-0.10	0.74	
20A	0.27	0.66	1.02	
20B	-0.38	0.02	0.29	
21A	-0.45	-0.20	1.16	
21B	-0.26	0.82	1.90	
22A	0.43	0.72	0.80	
22B	-0.30	0.52	0.40	

#### NAVY BC SUM OF SUBTEST STANDARD SCORES COMPOSITE

Percentages At or Above Cut Scores (Ordered High to Low)

Test - Cut Score -153.00 147.00 61.24 72.25 61.96 73.14 60.55 71.93 60.55 71.92 REF 15G 20A 20B 60.66 72.53 21A 21B 60.87 72.42 22A 60.70 72.13 72.75 22B 61.07

## NAVY BC SUM OF SUBTEST STANDARD SCORES COMPOSITE

Differences in Percentages At or Above Cut Scores (Test-REF)

Test - Cut Score -53.00 147.00 0.88 0.72 15G -0.69 20A -0.32 -0.33 0.28 20B -0.69 -0.58 -0.37 21A 21B 0.17 22A -0.54 -0.12 22B 0.49 -0.17

## ASVAB 20, 21, AND 22 IOT&E SUPPLEMENT

Tables 1-26 and Figures 1-35

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Defense Manpower Data Center

**JANUARY 1994** 

## **TABLE OF TABLES**

Table 1	ASVAB Subtests, Numbers of Items, Time Limits, and Normative Means and Standard Deviations
Table 2	Number of Subjects, by Test Form
Table 3	Number of Subjects, Percentage of Subjects, and Contribution to Chi-Square, by Gender, Race, and Education
Table 4	Subtest Raw Score Mean, Standard Deviation, Skewness, and Kurtosis, by ASVAB Form
Table 5	Degrees of Polynomials and Tests of Significance of Item-Order Effects S-5
Table 6	Means, Standard Deviations, and Number of Terms in Polynomial Smoothings for Equating
Table 7	Root Mean Square Difference Between Equatings, by Subtest and Form
Table 8	Percentage of Subjects for Which Equatings Differ by More than .5 Standard Score Points, by Subtest and Form S-8
Table 9	Root Mean Square Difference Between Distributions of Reference Form and Equated New Forms, by Subtest and Form
Table 10	Percentage of Subjects at Scores Where Cumulative Distributions of Reference Form and Equated New Forms Differ by More than .01, by Subtest and Form
Table 11	Subtest Means, Standard Deviations, and Correlations after Application of Current Conversion Tables
Table 12	Subtests and Upper Bounds of Categories for Composites
Table 13	Composite-Category-by-Test-Form Chi-Squares (Reference, Operational, & New [20-22] Forms; Reference Form vs. Operational 15g and Each New Form [20-22])
Table 14	Standard Deviations of Composites
Table 15	Composite-Category-by-Test-Form Chi-Square for ASVAB 15/16/17, After Equatings Based on IOT&E of ASVAB 15/16/17
Table 16	Standard Deviations of Composites from ASVAB 15/16/17 IOT&E S-23

Table 17	Standard Deviations of Composites from ASVAB 18/19 IOT&E S-24
Table 18	AFQT Category Distributions for Three Subsets of the Data S-25
Table 19	Air Force M Composite Distributions for Three Subsets of the Data S-26
Table 20	Army GM Composite Distributions for Three Subsets of the Data S-27
Table 21	ASVAB 20a, Conversion of Raw Test Scores to 1980 Standard Score Equivalents
Table 22	ASVAB 20b, Conversion of Raw Test Scores to 1980 Standard Score Equivalents
Table 23	ASVAB 21a, Conversion of Raw Test Scores to 1980 Standard Score Equivalents
Table 24	ASVAB 21b, Conversion of Raw Test Scores to 1980 Standard Score Equivalents
Table 25	ASVAB 22a, Conversion of Raw Test Scores to 1980 Standard Score Equivalents
Table 26	ASVAB 22b, Conversion of Raw Test Scores to 1980 Standard Score Equivalents
	TABLE OF FIGURES
Figure 1	Unsmoothed and Polynomial Log-Linear Smoothed Distributions for Equating GS
Figure 2	Unsmoothed and Polynomial Log-Linear Smoothed Distributions for Equating AR
Figure 3	Unsmoothed and Polynomial Log-Linear Smoothed Distributions for Equating WK
Figure 4	Unsmoothed and Polynomial Log-Linear Smoothed Distributions for Equating PC
Figure 5	Unsmoothed and Polynomial Log-Linear Smoothed Distributions for Equating NO

Figure 6	Unsmoothed and Polynomial Log-Linear Smoothed Distributions for Equating CS S-51
Figure 7	Unsmoothed and Polynomial Log-Linear Smoothed Distributions for Equating AS
Figure 8	Unsmoothed and Polynomial Log-Linear Smoothed Distributions for Equating MK
Figure 9	Unsmoothed and Polynomial Log-Linear Smoothed Distributions for Equating MC
Figure 10	Unsmoothed and Polynomial Log-Linear Smoothed Distributions for Equating El
Figure 11	Unsmoothed and Polynomial Log-Linear Smoothed Distributions for Equating VE
Figure 12	Standard-Score Contrast of Linear-Rescaling, Quartic Log-Linear and Polynomial Log-Linear Equatings With Linear-Identity Equating for GS
Figure 13	Contrast of Cumulative Distributions of Quartic and Polynomial Log-Linear Equated Scores With Cumulative Distributions of Reference Form for GS
Figure 14	Standard-Score Contrast of Linear-Rescaling, Quartic Log-Linear and Polynomial Log-Linear Equatings With Linear-Identity Equating for AR
Figure 15	Contrast of Cumulative Distributions of Quartic and Polynomial  Log-Linear Equated Scores With Cumulative Distributions  of Reference Form for AR
Figure 16	Standard-Score Contrast of Linear-Rescaling, Quartic Log-Linear and Polynomial Log-Linear Equatings With Linear-Identity  Equating for WK
Figure 17	Contrast of Cumulative Distributions of Quartic and Polynomial  Log-Linear Equated Scores With Cumulative Distributions  of Reference Form for WK
Figure 18	Standard-Score Contrast of Linear-Rescaling, Quartic Log-Linear and Polynomial Log-Linear Equatings With Linear-Identity  Equating for PC

Figure 19	Contrast of Cumulative Distributions of Quartic and Polynomial  Log-Linear Equated Scores With Cumulative Distributions  of Reference Form for PC
Figure 20	Standard-Score Contrast of Linear-Rescaling, Quartic Log-Linear and Polynomial Log-Linear Equatings With Linear-Identity  Equating for NO
Figure 21	Contrast of Cumulative Distributions of Quartic and Polynomial Log-Linear Equated Scores With Cumulative Distributions of Reference Form for NO
Figure 22	Standard-Score Contrast of Linear-Rescaling, Quartic Log-Linear and Polynomial Log-Linear Equatings With Linear-Identity  Equating for CS
Figure 23	Contrast of Cumulative Distributions of Quartic and Polynomial Log-Linear Equated Scores With Cumulative Distributions of Reference Form for CS
Figure 24	Standard-Score Contrast of Linear-Rescaling, Quartic Log-Linear and Polynomial Log-Linear Equatings With Linear-Identity  Equating for AS
Figure 25	Contrast of Cumulative Distributions of Quartic and Polynomial Log-Linear Equated Scores With Cumulative Distributions of Reference Form for AS
Figure 26	Standard-Score Contrast of Linear-Rescaling, Quartic Log-Linear and Polynomial Log-Linear Equatings With Linear-Identity  Equating for MK
Figure 27	Contrast of Cumulative Distributions of Quartic and Polynomial  Log-Linear Equated Scores With Cumulative Distributions  of Reference Form for MK
Figure 28	Standard-Score Contrast of Linear-Rescaling, Quartic Log-Linear and Polynomial Log-Linear Equatings With Linear-Identity  Equating for MC
Figure 29	Contrast of Cumulative Distributions of Quartic and Polynomial  Log-Linear Equated Scores With Cumulative Distributions of  Reference Form for MC
Figure 30	Standard-Score Contrast of Linear-Rescaling, Quartic Log-Linear and Polynomial Log-Linear Equatings With Linear-Identity  Equating for El

Figure 31	Contrast of Cumulative Distributions of Quartic and Polynomial  Log-Linear Equated Scores With Cumulative Distributions				
	of Reference Form for EI	87			
Figure 32	Standard-Score Contrast of Linear-Rescaling, Quartic Log-Linear				
-	and Polynomial Log-Linear Equatings With Linear-Identity				
	Equating for VE S-	88			
Figure 33	Contrast of Cumulative Distributions of Quartic and Polynomial				
_	Log-Linear Equated Scores With Cumulative Distributions				
	of Reference Form for VE	90			
Figure 34	First Principal Component of Power Subtest Standard Scores,				
•	by Test Form	92			
Figure 35	Second and Third Principal Components of Power Subtest Standard Scores,				
-	by Test Form	93			

ASVAB 20, 21, AND 22 IOT&E SUPPLEMENT TABLES 1-26

Table 1

ASVAB Subtests, Numbers of Items, Time Limits, and Normative Means and Standard Deviations

		Time		
<u>Subtest</u> General Science (GS)	<u>Items</u> 25	(min.) 11	<u>Mean</u> 15.950	<u>S.D.</u> 5.010
Arithmetic Reasoning (AR)	30	36	18.009	7.373
Word Knowledge (WK)	35	11	26.270	7.710
Paragraph Comprehension (PC)	15	13	11.011	3.355
Numerical Operations (NO)	50	3	37.236	10.800
Coding Speed (CS)	84	7	47.606	16.763
Auto and Shop Information (AS)	25	11	14.317	5.550
Math Knowledge (MK)	25	24	13.578	6.393
Mechanical Comprehension (MC)	25	19	14.165	5.349
Electronics Information (EI)	20	9	11.569	4.236
Verbal (VE = WK + PC)	50	-	37.281	10.595

Table 2

Number of Subjects, by Test Form

ASVAB Form	All Tested from 10/1/92 to 1/15/93	Initial Testing Only	After Editing for Extreme Unbalancing
15g	18852	15959	13312
(Operational)	13.5%	13.5%	13.4%
15h	18027	15342	12931
(Reference)	12.9%	13.0%	13.0%
20a	18613	15647	13097
	13.3%	13.2%	13.2%
20b	17973	15237	12778
	12.8%	12.9%	12.9%
21a	17688	14951	12532
	12.6%	12.6%	12.6%
21b	16926	14369	12060
	12.1%	12.1%	12.2%
22a	16350	13753	11558
	11.7%	11.6%	11.6%
22b	15633	13007	10986
	11.2%	11.0%	11.1%
Total	140062	118265	99254
Cumulative Percent Deleted		15.6%	29.1%

Table 3

Number of Subjects, Percentage of Subjects, and Contribution to Chi-Square, by Gender, Race, and Education

Female	15G	15H	<u>20A</u>	ASVAB 20B	Form 21A	21B	22 <b>A</b>	22B	Total	
Number 20 Chi-Sq 0.00	065 (	0.0052	0.1891	7,7795	0.7149	2280 2.1895	0.3512	0.4877	19355	
Percent 19	. 53	19.47	19.33	20.59	19.17	18.91	19.74	19.21	19.50	
<u>Male</u>										
Number 10	712	10413	10565	10147			9276		79899	
Chi-Sq 0.00 Percent 80									80.50	
Gender x A	Gender x ASVAB Form Pearson Chi-Square = 14.564 (d.f.=7, pr.=.042)									
Non-High Sch	10001	Gradua	tes (ir	cluding	Currer	it Stude	nts)			
Number 4	647	4513	4664	4437	4430	4242	3980	3869	34782	
Chi-Sq 0.00 Percent 34							1.2208 34.44	0.0951 35.22	35.04	
High School	Grad	luates								
Number 8	047	7803	7829	7758	7517	7290	7071	6629	59944	
Chi-Sq 0.0 Percent 60	066 (	0.0056	0.8269	0.2155	0.3524	0.0057	1.1759	0.0053	60.39	
				00.71	37.70	00.45	01.10	00.54	00.55	
Post-Second			_							
Number Chi-Sq 0.1									4528	
Percent 4	.64	4.76	4.61	4.56	4.67	4.38			4.56	
Education :	x Ast	/AB For	m Pears	son Chi-	-Square	= 9.862	2 (d.f.:	=14, pr.	=.785)	
Caucasian										
Number 10									74658	
Chi-Sq 0.0 Percent 75	.34	75.27	75.33	75.29	74.76	75.60	75.12	75.01	75.22	
Non-Caucasian										
Number 3				3157	3163	2943			24596	
Chi-Sq 0.0 Percent 24	.66	24.73	0.0652 24.67	0.0285 24.71	1.0632 25.24	0.6949 24.40	0.0488		24.78	
Race x ASVAB	Race x ASVAB Form Pearson Chi-Square = 2.894 (d.f.=7, pr.=.895)									

Table 4

Subtest Raw Score Mean, Standard Deviation, Skewness, and Kurtosis, by ASVAB Form

		Form	15G	15H	20A	20B	21 <b>A</b>	21B	22 <b>A</b>	22B
<b>,</b> 1)	GS	Mean	16.849	16.406	17.311		17.484	17.528	17.147	17.144
	•	SD	4.362	4.275	4.448	4.407	4.297	4.211	4.410	4.389
		Skew	-0.256	-0.253	-0.320	-0.282	-0.511	-0.549	-0.516	-0.508
		Kurt	2.434	2.565	2.463	2.408	2.927	3.063	2.738	2.759
	ΔR	Mean	19.33	19.016	20.001	18.596	19.611	19.338	19.468	19.354
		SD	6.188	6.282	5.812	6.440	6.359	5.705	6.055	6.227
		Skew	-0.154	-0.113	-0.244	-0.136	-0.184	-0.087	-0.145	-0.091
		Kurt	2.099	2.102	2.319	2.174	2.097	2.384	2.230	2.120
	WK	Mean	27.333	27.610	27.404	27.090	27.271	27.073	27.175	27.240
		SD	5.552	5.361	5.594	6.150	5.787	5.604	5.733	5.691
		Skew	-0.924	-0.961	-1.029	-0.877	-0.938	-0.837	-0.893	-0.889
		Kurt	3.644	3.904	4.025	3.251	3.523	3.321	3.477	3.440
	PC	Mean	12.353	11.599	11.732	11.668	11.999	11.641	12.070	11.423
		SD	2.492	2.551	2.727	2.484	2.320	2.667	2.588	2.849
		Skew	-1.381	-1.074	-1.093	-0.873	-1.143	-1.007	-1.101	-0.926
		<u>Kurt</u>	<u>5.032</u>	<u>4.069</u>	3.924	3.707	4.613	3.788	4.019	<u>3.398</u>
	NO	Mean	36.781	37.161	36.452	36.678	36.271	36.171	36.818	37.026
		SD	8.639	8.613	8.440	8.316	8.619	8.580	8.610	8.649
		Skew	-0.430	-0.477	-0.354	-0.379	-0.353	-0.314	-0.402	-0.426
		Kurt	2.947	2.990	2.814	2.897	2.793	2.694	2.828	2.823
	CS	Mean	51.296	50.966	48.735	48.983	49.843	49.174	50.382	50.358
		SD	12.555	12.530	12.052	12.161	12.252	12.003	12.669	12.378
		Skew	-0.140	-0.252	-0.194	-0.159	-0.170	-0.130	-0.187	-0.233
	**	Kurt	3.388	3.567 14.840	3.451 14.981	3.447 14.813	3.348	3.444	3.318	<u>3.378</u>
	AS	Mean	14.537 5.060	4.930	4.693	4.714	15.249 4.865	15.355	15.157	15.073
		SD Skew	0.040	-0.012	-0.047	-0.022	0.070	4.810 0.018	5.117 -0.022	5.138 0.011
		Kurt	2.138	2.226	2.370	2.369	2.161	2.197	2.097	2.082
	MZ	Mean	15.345	15.066	15.034	14.698	15.019	$\frac{2.137}{15.027}$	15.270	14.705
	M	SD	5.439	5.532	5.719	5.603	5.728	5.429	6.002	5.854
		Skew	-0.064	-0.022	0.049	0.092	0.065	-0.011	-0.068	0.059
		Kurt	2.101	2.019	1.982	2.057	1.924	2.093	1.931	1.964
	MC	Mean	15.860	15.170	15.463	15.427	16.002	16.085	15.588	15.537
		SD	4.647	4.952	4.871	4.864	4.751	4.727	4.769	4.762
		Skew	-0.274	-0.095	-0.167	-0.167	-0.169	-0.187	-0.149	-0.130
		Kurt	2.396	2.176	2.271	2.294	2.305	2.289	2.257	2.267
	ΕI	Mean	11.778	$1\overline{1.771}$	12.120	12.088	11.927	12.043	11.904	12.032
		SD	3.536	3.600	3.640	3.712	3.725	3.686	3.701	3.636
		Skew	0.075	-0.169	-0.077	-0.108	-0.060	-0.027	-0.079	-0.105
		<u>Kurt</u>	<u>2.519</u>	2.513	2.487	2.462	2.443	2.425	2.500	2.569
	VE	Mean	39.686	39.209	39.136	38.758	39.269	38.714	39.245	38.663
		SD	7.556	7.301	7.790	8.029	7.591	7.719	7.750	7.996
		Skew	-1.070	-1.027	-1.084	-0.862	-1.013	-0.894	-0.946	-0.931
		<u>Kurt</u>	<u>4.101</u>	<u>4.080</u>	4.127	<u>3.361</u>	<u>3.837</u>	3.504	<u>3.632</u>	<u>3.525</u>

Table 5

Degrees of Polynomials and Tests of Significance of Item-Order Effects

Subtests	Forms	Degree of Polynomial	Chi-Square	D.F. Prob.
GS	20a&b	9 (6&9)	13.688	9 0.139
	21a&b	7 (7&6)	14.154	7 0.049
	22a&b	6 (6&6)	1.393	6 0.966
CS	20a&b	8 (8&8)	13.147	8 0.107
	21a&b	8 (8&8)	34.263	8 *0.000
	22a&b	9 (9&8)	22.293	9 0.008
AS	20a&b	7 (7&7)	10.767	7 0.149
	21a&b	7 (7&7)	16.088	7 0.024
	22a&b	9 (7&9)	7.284	9 0.608
MC	20a&b	7 (7&7)	7.614	7 0.368
	21a&b	9 (9&7)	15.729	9 0.083
	22a&b	9 (7&9)	3.548	9 0.939
EI	20a&b	9 (9&5)	12.983	9 0.163
	21a&b	7 (7&4)	13.586	7 0.059
	22a&b	9 (9&9)	20.675	9 0.014

<sup>\*</sup> Chi-square significant at alpha = .05/15 = .0033

Table 6

Means, Standard Deviations, and Number of Terms in Polynomial Smoothings for Equating

	Form	15G	15H	20A 20B	21A 21B	22A 22B
GS	SD	16.849 4.362 6	16.406 4.275 4	17.304* 4.428 6	17.506* 4.255 7	17.146* 4.400 6
AR	Mean : SD Terms	6.188		20.001 18.596 5.812 6.440 6 5	6.359 5.705	
WK	Mean 3 SD Terms	5.552		27.404 27.090 5.594 6.150 7 9		
PC	Mean : SD Terms	2.492		11.732 11.668 2.727 2.484 7 7		
NO	Mean S SD Terms	36.781 8.639 9	37.161 8.613 9	36.564* 8.380 9	36.222* 8.600 10	36.919* 8.630 7
CS	Mean ! SD : Terms	51.296 12.555 8	50.966 12.530 8	48.857* 12.106 8	49.843 49.174 12.252 12.003 8 8	50.370* 12.528 10
AS	SD	5.060	14.840 4.930 9	14.893* 4.704 9	15.301* 4.838 7	15.116* 5.128 9
MK	Mean : SD Terms	5.439	15.066 5.532 7	15.034 14.698 5.719 5.603 9 7	15.019 15.027 5.728 5.429 4 9	1.5.270 14.705 6.002 5.854 6 7
MC	Mean : SD Terms	4.647	15.170 4.952 8	15.445* 4.868 7	16.043* 4.739 9	15.563* 4.766 9
EI	Mean : SD Terms	11.778 3.536 9	11.771 3.600 7	12.104* 3.676 9	11.984* 3.706 9	11.966* 3.670 9
VE	Mean : SD Terms	39.686 7.556 9	39.209 7.301 9	39.136 38.758 7.790 8.029 9 9	39.269 38.714 7.591 7.719 9 10	39.245 38.663 7.750 7.996 9 7

<sup>\*</sup> Data pooled for subtests with same items in different order.

Table 7

Root Mean Square Difference Between Equatings, by Subtest and Form

<del></del>		<del></del>			
AFQT Subtest andForm	Raw vs. <u>Linear</u>	Raw vs. Polymomial	NON-AFQT Subtest and Form	Raw vs. <u>Linear</u>	Raw vs. Polymomial
AR 15g	0.140	0.044	GS 15g	0.278	0.058
AR 20ā	0.415	0.037	GS 20a/b	0.337	0.052
AR 20b	0.153	0.055	GS 21a/b	0.613	0.074
AR 21a	0.226	0.041	GS 22a/b	0.619	0.065
AR 21b	0.527	0.044			
AR 22a	0.246	0.028	NO 15g	0.138	0.063
AR 22b	0.152	0.047	NO 20a/b	0.294	0.058
W 15-	0.014	0.000	NO 21a/b	0.307	0.055
WK 15g WK 20a	0.214 0.147	0.038 0.033	NO 22a/b	0.130	0.052
WK 20a WK 20b	0.433	0.033	CS 15g	0.248	0 061
WK 20D WK 21a	0.298	0.054	CS 20a/b	0.224	0.061 0.083
WK 21b	0.311	0.046	CS 21a	0.244	0.003
WK 22a	0.244	0.039	CS 21b	0.238	0.064
WK 22b	0.268	0.040	CS 22a/b	0.188	0.065
	• • • • • • • • • • • • • • • • • • • •		•		
PC 15g	0.443	0.018	AS 15g	0.207	0.042
PC 20a	0.232	0.050	AS 20a/b	0.291	0.037
PC 20b	0.506	0.026	AS 21a/b	0.221	0.041
PC 21a	0.324	0.041	AS 22a/b	0.253	0.037
PC 21b	0.167	0.069	WO 15-	0.540	0.050
PC 22a	0.183	0.046	MC 15g	0.549	0.050
PC 22b	0.362	0.036	MC 20a/b MC 21a/b	0.244 0.292	0.038
MK 15g	0.189	0.039	MC 22a/b	0.203	0.041 0.048
MK 20a	0.237	0.033	rk zza,D	0.20.3	0.030
MK 20b	0.351	0.033	El 15g	0.614	0.041
MK 21a	0.318	0.051	EI 20a/b	0.238	0.041
MK 21b	0.199	0.038	EI 21a/b	0.327	0.036
MK 22a	0.246	0.040	EI 22a/b	0.249	0.046
MK 22b	0.245	0.045	,		
	0.450	0.041			
VE 15g	0.150	0.041			
VE 20a	0.166	0 :			
VE 20b VE 21a	0.370 0.163	0 4			
VE 21a VE 21b	0.163	0. 0.039			
VE 210 VE 22a	0.219	0.039			
VE 22b	0.284	0.053			
	J				

Table 8

Percentage of Subjects for Which Equatings Differ by More Than .5 Standard Score Points, by Subtest and Form

AFQT Subtest and Form	Raw vs. Linear	Raw vs. Polymomial	NON-AFOT Subtest and Form	Raw vs. Linear	Raw vs. Polymomial
AR 15g AR 20a	0.06 5.98	0.00 0.00	GS 15g GS 20a/b	5.06 7.49	0.00 0.00
AR 20b	1.24	0.00	GS 21a/b	18.27	0.00
AR 21a	3.75	0.00	GS 22a/b	32.72	0.00
AR 21b	48.59	0.00			
AR 22a	3.61	0.00	NO 15g	0.00	0.00
AR 22b	0.00	0.00	NO 20a/b NO 21a/b	10.14 12.26	0.00 0.00
WK 15g	1.95	0.00	NO 22a/b	0.80	0.00
WK 20a	0.74	0.00	140 224/5	0.00	0.00
WK 20b	19.23	0.00	CS 15g	5.73	0.00
WK 21a	3.99	0.00	CS 20a/b	3.28	0.00
WK 21b	8.54	0.00	CS 21a	5.87	0.00
WK 22a	1.88	0.00	CS 21b	4.31	0.00
WK 22b	1.65	0.00	CS 22a/b	3.43	0.00
PC 15g	3.56	0.00	AS 15g	2.21	0.00
PC 20a	0.40	0.00	AS 20a/b	1.55	0.00
PC 20b	39.36	0.00	AS 21a/b	0.06	0.00
PC 21a	4.76	0.00	<b>AS 22a/b</b>	3.15	0.00
PC 21b	0.85	0.55			
PC 22a	0.07	0.00	MC 15g	36.56	0.00
PC 22b	15.85	0.00	MC 20a/b MC 21a/b	3.16 3.66	0.00 0.00
MK 15g	2.49	0.00	MC 22a/b	2.42	0.00
MK 20a	1.53	0.00	110 224/2	2.12	0.00
MK 20b	12.72	0.00	EI 15g	51.55	0.00
MK 21a	2.98	0.00	EI 20a/b	0.00	0.00
MK 21b	0.00	0.00	EI 21a/b	13.17	0.00
MK 22a	5.10	0.00	EI 22a/b	5.79	0.00
MK 22b	2.02	0.00			
VE 15q	0.04	0.00			
VE 20a	1.70	0.00			
VE 20b	4.66	0.00			
VE 21a	0.73	0.00			
VE 21b	2.62	0.00			
VE 22a	1.64	0.00			
VE 22b	2.09	0.00			

Table 9

Root Mean Square Difference Between Distributions of Reference Form and Equated New Forms, by Subtest and Form

AFQT Subtest	Reference vs. Polynomial	NON-AFQT Subtest	Reference vs. Polynomial
and Form	Equated Scores	and Form	Equated Scores
AR 15g	0.0013	GS 15g	0.0017
AR 20a	0.0010	GS 20a/b	0.0014
AR 20b	0.0014	GS 21a/b	0.0017
AR 21a	0.0009	GS 22a/b	0.0017
AR 21b	0.0010	-	
AR 22a	0.0006	NO 15q	0.0019
AR 22b	0.0012	NO 20a/b	0.0014
		NO 21a/b	0.0020
WK 15g	0.0007	NO 22a/b	0.0015
WK 20a	0.0009		
WK 20b	0.0009	CS 15g	0.0023
WK 21a	0.0011	CS 20a/b	0.0028
WK 21b	0.0008	CS 21a	0.0020
WK 22a	0.0008	CS 21b	0.0019
WK 22b	0.0013	CS 22a/b	0.0021
			******
PC 15g	0.0003	AS 15g	0.0009
PC 20a	0.0006	AS 20a/b	0.0010
PC 20b	0.0003	AS 21a/b	0.0009
PC 21a	0.0007	AS 22a/b	0.0009
PC 21b	0.0007	·	
PC 22a	0.0013	MC 15g	0.0014
PC 22b	0.0002	MC 20a/b	0.0009
	•	MC 21a/b	0.0009
MK 15g	0.0010	MC 22a/b	0.0012
MK 20a	0.0008		0,000
MK 20b	0.0006	EI 15g	0.0009
MK 21a	0.0013	EI 20a/b	0.0010
MK 21b	0.0010	EI 21a/b	0.0009
MK 22a	0.0010	EI 22a/b	0.0014
MK 22b	0.0010		0.0011
	313323		
VE 15g	0.0014		
<b>VE 20a</b>	0.0013		
VE 20b	0.0015		
VE 21a	0.0013		
VE 21b	0.0013		
VE 22a	0.0013		
VE 22b	0.0020		

Table 10

Percentage of Subjects at Scores Where Cumulative Distributions of Reference Form and Equated New Forms
Differ by More than .01, by Subtest and Form

AFQT Subtest and Form	Reference vs. Polynomial Equated Scores	NON-AFOT Subtest and Form	Reference vs. Polynomial Equated Scores
AR 15g AR 20a AR 20b AR 21a AR 21b	0.00 0.00 0.00 0.00 0.00	GS 15g GS 20a/b GS 21a/b GS 22a/b	0.00 0.00 0.00 0.00
AR 22a AR 22b WK 15g	0.00 0.00 0.00	NO 15g NO 20a/b NO 21a/b NO 22a/b	0.00 0.00 0.00 0.00
WK 20a WK 20b WK 21a WK 21b WK 22a WK 22b	0.00 0.00 0.00 0.00 0.00 0.00	CS 15g CS 20a/b CS 21a CS 21b CS 22a/b	0.00 0.00 0.00 0.00 0.00
PC 15g PC 20a PC 20b PC 21a PC 21b	0.00 0.00 0.00 0.00 0.00	AS 15g AS 20a/b AS 21a/b AS 22a/b	0.00 0.00 0.00 0.00
PC 22a PC 22b MK 15g	0.00 0.00 0.00	MC 15g MC 20a/b MC 21a/b MC 22a/b	0.00 0.00 0.00 0.00
MK 20ā MK 20b MK 21a MK 21b MK 22a MK 22b	0.00 0.00 0.00 0.00 0.00 0.00	EI 15g EI 20a/b EI 21a/b EI 22a/b	0.00 0.00 0.00 0.00
VE 15g VE 20a VE 20b VE 21a VE 21b VE 22a VE 22b	0.00 0.00 0.00 0.00 0.00 0.00 0.00		-

Subtest Means, Standard Deviations, and Correlations of Subtests, after Application of Current Conversion Tables

			FORM	15h St	andard	Score S	tatisti	.CS			
Subtest											
MEAN	50.81	51.34	51.73	51.80	53.12	52.58	50.91	52.33	51.89	50.46	51.80
S.D. N	8.55 12931	8.53 12931	6.94 12931	7.65 12931	7.78 12931	7.65 12931	8.88 12931	8.64 12931	9.31 12931	8.48 12931	6.82 12931
.,	44771	12/31	12371	****	12/54	14731	14771	14//1	12331	12771	14731
			FORM	15h Sta	ndard S	core Co	rrelati	.ons			
Subtest											
STD-GS STD-AR	1.00 0.60	0.60 1.00	0.72 0.59	0.56 0.58	0.23	0.22 0.37	0.58 0.44	0.53 0.73	0.65 0.61	0.69 0.53	0.72 0.63
STD-WK	0.72	0.59	1.00	0.66	0.28	0.28	0.48	0.50	0.55	0.60	0.96
STD-PC	0.56	0.58	0.66	1.00	0.38	0.37	0.36	0.51	0.46	0.48	0.83
SID-NO	0.23	0.44	0.28	0.38	1.00	0.63	0.09	0.47	0.20	0.16	0.34
STD-CS STD-AS	0.22 0.58	0.37	0.28 0.48	0.37 0.36	0.63 0.09	1.00 0.10	0.10 1.00	0.40	0.20 0.67	0.17 0.68	0.34 0.48
STD-MK	0.53	0.44 0.73	0.50	0.51	0.47	0.10	0.24	1.00	0.48	0.40	0.54
STD-MC	0.65	0.61	0.55	0.46	0.20	0.20	0.67	0.48	1.00	0.67	0.56
STD-EI	0.69	0.53	0.60	0.48	0.16	0.17	0.68	0.40	0.67	1.00	0.60
STD-VE	0.72	0.63	0.96	0.83	0.34	0.34	0.48	0.54	0.56	0.60	1.00
		FORM	1 15g (C	peratio	nal) St	andard	Score S	tatisti	.C8		
Subtest	STD-GS	STD-AR	STD-WK	STD-PC	STD-NO	STD-CS	STD-AS	STD-MK	STD-MC	STD-EI	STD-VE
MEAN	51.00	51.07	52.00	52.06	52.84	52.83	50.89	52.44	52.07	50.32	52.03
S.D.	8.36	8.56	6.88	7.46	7.72	7.59	8.95	8.63	9.07	8.99	6.87
N	13312	13312	13312	13312	13312	13312	13312	13312	13312	13312	13312
		FORM	15g (Op	eration	al) Sta	ndard S	core Co	rrelati	ons.		
Subtest	STD-GS	STD-AR		STD-PC	STD-NO	STD-CS	STD-AS	STD-MK	STD-MC	STD-EI	
STD-GS	1.00		0.70	0.58	0.22	0.23	0.53	0.54 0.71	0.65	0.62	0.70
STD-AR	0.62 0.70	1.00	0.59	0.55 0.72	0.42	0.39	0.39	0.71	0.62 0.51	0.47	0.62 0.97
STD-WK STD-PC	0.58	0.59 0.55	1.00 0.72	1.00	0.29 0.32	0.33 0.34	0.40	0.50 0.48	0.42	0.47 0.39	0.86
STD-NO	0.22	0.42	0.29	0.32	1.00	0.65	0.03	0.44	0.18	0.13	0.32
STD-CS	0.23	0.39	0.33	0.34	0.65	1.00	0.05	0.40	0.19	0.15	0.35
STD-AS	0.53	0.39	0.40 0.50	0.30 0.48	0.03 0.44	0.05	1.00	0.19 1.00	0.60	0.65	0.39 0.52
STD-MK STD-MC	0.54 0.65	0.71 0.62	0.50	0.42	0.18	0.40 0.19	0.19 0.60	0.50	0.50 1.00	0.36 0.60	0.52
STD-EI	0.62	0.47	0.47	0.39	0.13	0.15	0.65	0.36	0.60	1.00	0.48
STD-VE	0.70	0.62	0.97	0.86	0.32	0.35	0.39	0.52	0.52	0.48	1.00
FOR	M 15g S	tandard	Score :	Statist:	ic Diffe	erences	from t	he Refe	rence P	ORM (15)	H)
Subtest	STD-GS					STD-CS		STD-MK	STD-MC	STD-EI	
MEAN	0.19	-0.27	0.28	0.27	-0.27	0.24	-0.02	0.11	0.18	-0.13	0.23
S.D N	-0.19	0.02	-0.06 381.00	-0.19	-0.06	-0.06	0.07	-0.01	-0.24	0.51	0.05
N	301.00	361.00	361.00	361.00	301.00	301.00	361.00	361.00	361.00	381.00	361.00
FORM	15g St	andard :	Score C	orrelat:	ion Dif	ference	s from	the Ref	erence i	FORM (1	5h)
Subtest	STD-GS	STD-AR	STD-WK					STD-MK	STD-MC	STD-EI	STD-VE
STD-GS	0.00		-0.02	0.02	-0.02	0.00	-0.05	0.02	-0.00	-0.07	-0.02
STID-AR STID-WK	0.02 -0.02	0.00 0.01	0.01 0.00	-0.03 0.07	-0.03 0.01	0.02 0.04	-0.05 -0.09	-0.02 -0.00	0.01 -0.04	-0.06 -0.13	-0.01 0.01
STD-PC	0.02		0.07	0.00	-0.06	-0.03	-0.06	-0.04	-0.03	-0.08	0.03
STD-NO	-0.02	-0.03	0.01	-0.06	0.00	0.02	-0.06	-0.03	-0.01	-0.03	-0.02
SID-CS	0.00	0.02	0.04	-0.03	0.02	0.00	-0.05	0.00	-0.01	-0.02	0.01
STD-AS STD-MK	-0.05 0.02	-0.05 -0.02	-0.09 -0.00	-0.06 -0.04	-0.06 -0.03	-0.05 0.00	0.00 -0.06	-0.06 0.00	-0.07 0.02	-0.03 -0.04	-0.09 -0.02
STD-MC	-0.00		-0.04	-0.03	-0.01	-0.01	-0.07		0.00	-0.07	-0.04
STD-EI	-0.07	-0.06	-0.13	-0.08	-0.03	-0.02	-0.03	-0.04	-0.07	0.00	-0.13
STD-VE	-0.02	-0.01	0.01	0.03	-0.02	0.01	-0.09	-0.02	-0.04	-0.13	0.00
							co	ntinue	d		

# Subtest Means, Standard Deviations, and Correlations of Subtests, after Application of Current Conversion Tables

FORM 20a	Standa	rd Score	Stati	stics							
Subtest	STD-GS	STD-AR	STD-MK	STD-PC	STD-NO	STD-CS	STD-AS	STD-MK	STD-MC	STD-EI	STD-VE
MEAN	51.07	51.37	51.77	51.70	53.16	52.49	51.08	52.27	51.97	50.51	51.82
S.D. N	8.54 13097	8.48 13097	6.96 13097	7.53 13097	7.78	7.62	8.88	8.62	9.29	8.40	6.90
N	13097	13097	13097	13097	13097	13097	13097	13097	13097	13097	13097
FORM 20a											
Subtest											
STD-GS STD-AR	1.00 0.62	0.62 1.00	0.73 0.58	0.63 0.59	0.27 0.43	0.26 0.38	0.48 0.39	0.60 0.74	0.62 0.64	0.64 0.52	0.74 0.63
STD-WK	0.73	0.58	1.00	0.72	0.29	0.32	0.43	0.51	0.55	0.56	0.97
STD-PC	0.63	0.59	0.72	1.00	0.37	0.40	0.39	0.52	0.53	0.51	0.86
STD-NO	0.27	0.43	0.29	0.37	1.00	0.62	0.07	0.44	0.24	0.19	0.33
STD-CS	0.26	0.38 0.39	0.32	0.40 0.39	0.62 0.07	1.00 0.10	0.10 1.00	0.38	0.25	0.19	0.37
STD-AS STD-MK	0.48 0.60	0.74	0.43 0.51	0.52	0.44	0.38	0.22	0.22	0.60 0.52	0.59 0. <b>4</b> 6	0.45 0.55
STD-MC	0.62	0.64	0.55	0.53	0.24	0.25	0.60	0.52	1.00	0.64	0.58
STD-EI	0.64	0.52	0.56	0.51	0.19	0.19	0.59	0.46	0.64	1.00	0.58
STD-VE	0.74	0.63	0.97	0.86	0.33	0.37	0.45	0.55	0.58	0.58	1.00
FORM 20a	Standar	rd Score	e Statis	stic Di	fference	s from	the Rei	ierence	FORM (	15h)	
Subtest						STD-CS				STD-EI	STD-VE
MEAN	0.26	0.03	0.05	-0.10	0.05	-0.10	0.17	-0.06	0.08	0.06	0.02
S.D. N	-0.01	-0.05	0.02	-0.12	0.00	-0.03	-0.00	-0.02	-0.02	-0.08	0.08
14	100.00	166.00	166.00	100.00	100.00	100.00	166.00	166.00	166.00	166.00	166.00
FORM 20a	Standar	rd Score	e Corre	lation I	Differen	nces fro	om the i	Referenc	ce FORM	(15h)	
Subtest											
STD-GS	0.00	0.02	0.01	0.07	0.04	0.04	-0.10	0.07	-0.03	-0.05	0.02
STD-AR STD-WK	0.02 0.01	0.00	-0.00 0.00	0.01 0.06	-0.01 0.00	0.01	-0.05 -0.06	0.01 0.01	0.03	-0.01 -0.04	-0.00 0.01
STD-PC	0.07	0.01	0.06	0.00	-0.01	0.02	0.03	0.01	0.07	0.03	0.03
STD-NO	0.04	-0.01	0.00	-0.01	0.00	-0.01	-0.02	-0.03	0.05	0.03	-0.01
STD-CS	0.04	0.01	0.03	0.02	-0.01	0.00	0.00	-0.02	0.04	0.02	0.03
STD-AS STD-MK	-0.10 0.07	-0.05 0.01	-0.06 0.01	0.03	-0.02 -0.03	0.00	0.00	-0.03	-0.06	-0.08	-0.04
STD-MC	-0.03	0.01	0.00	0.07	0.05	0.04	-0.03 -0.06	0.00	0.04 0.00	0.06 -0.03	0.01 0.02
STD-EI	-0.05	-0.01	-0.04	0.03	0.03	0.02	-0.08	0.06	-0.03	0.00	-0.02
STD-VE	0.02	-0.00	0.01	0.03	-0.01	0.03	-0.04	0.01	0.02	-0.02	0.00
FORM 20a	Standar	rd Score	e Statis	stic Di	ference	s from	the Ope	erations	al FORM	(15g)	
Subtest	STD-GS	STD-AR	STD-WK	STD-PC	STD-NO	STD-CS	SID-AS	STD-MK	STD-MC	SID-RI	STD-VE
MEAN	0.07	0.30	-0.23	-0.36	0.32	-0.34	0.19	-0.17	-0.10	0.19	-0.21
S.D.	0.18	-0.08	0.08	0.07	0.07	0.03	-0.07	-0.01	0.22	-0.59	0.03
N	-215.0	-215.0	-215.0	-215.0	-215.0	-215.0	-215.0	-215.0	-215.0	-215.0	-215.0
FORM 20a	Standar	rd Score	e Corre	lation I	Differen	nces fro	om the (	peratio	mal FO	M (15g)	ı
Subtest											
STD-GS	0.00	-0.00	0.03	0.05	0.05	0.04	-0.05	0.05	-0.03	0.02	0.04
STD-AR STD-WK	-0.00 0.03	0.00 -0.01	-0.01 0.00	0.04 -0.01	0.01 -0.01	-0.01 -0.01	-0.01	0.03	0.01	0.05	0.01
SID-WA	0.03	0.01	-0.00	0.00	0.01	0.05	0.03	0.01	0.04 0.11	0.09 0.12	-0.00 0.00
STD-NO	0.05	0.01	-0.01	0.05	0.00	-0.03	0.04	0.00	0.06	0.06	0.01
STD-CS	0.04	-0.01	-0.01	0.05	-0.03	0.00	0.05	-0.02	0.06	0.04	0.01
SID-AS	-0.05	-0.01	0.03	0.09	0.04	0.05	0.00	0.03	0.01	-0.06	0.05
STD-MK	0.05	0.03	0.01	0.04	0.00	-0.02	0.03	0.00	0.02	0.10	0.03
STD-MC STD-EI	-0.03 0.02	0.01 0.05	0.04 0.09	0.11 0.12	0.06 0.06	0.06 0.04	0.01 -0.06	0.02 0.10	0.00	0.04	0.07
STD-EI	0.02	0.03	-0.00	0.00	0.01	0.01	0.05	0.10	0.04	0.00 0.10	0.10 0.00
10	2.34		2.30	2.30	5.52	5.52	J. JJ	0.03	J.J.	0.20	0.00

## Subtest Means, Standard Deviations, and Intercorrelations, after Application of Current Conversion Tables

FORM 20b Standard Score Statistics												
Subtest MEAN	51.04	51.36	51.72	51.57	53,18	52.65	50.76	52.37	51.90	50.43	51.88	
S.D. N	8.46 12778	8.53 12778	7.03 12778	7.51 12778	7.83 12778	7.68 12778	8.91 12778	8.67 12778	9.27 12778	8.57 12778	6.95 12778	
N	12//6	12//6				core Co			12//6	12776	14//0	
Subtest	STD-GS	STD-AR	STD-WK	STD-PC	STD-NO	STD-CS	STD-AS	STD-MK	STD-MC	STD-EI	STD-VE	
STD-GS	1.00	0.61	0.73	0.57	0.26	0.25	0.49	0.60	0.62	0.65	0.74	
STD-AR STD-WK	0.61 0.73	1.00 0.58	0.58	0.54	0.43	0.39	0.39	0.74 0.51	0.62 0.57	0.51 9.58	0.61 0.97	
STD-PC	0.57	0.54	0.67	1.00	0.35	0.38	0.31	0.50	0.47	0.46	0.82	
STD-NO	0.26	0.43	0.27	0.35	1.00	0.61	0.07	0.44	0.23	0.19	0.32	
STD-CS STD-AS	0.25	0.39 0.39	0.31 0.47	0.38	0.61	1.00 0.10	0.10	0.38 0.24	0.24	0.20	0.36 0.45	
STD-MK	0.60	0.74	0.51	0.50	0.44	0.38	0.24	1.00	0.53	0.47	0.55	
STD-MC STD-EI	0.62 0.65	0.62 0.51	0.57 0.58	0.47 0.46	0.23 0.19	0.24	0.61	0.53 0.47	1.00	0.65	0.58 0.58	
STD-VE	0.74	0.61	0.97	0.82	0.32	0.36	0.45	0.55	0.65 0.58	0.58	1.00	
FOR	4 20b S	tandard	Score S	Statist	ic Diffe	erences	from th	he Refe	rence F	ORM (15)	1)	
Subtest	STD-GS	STD-AR	STD-WK	STD-PC	STD-NO	STD-CS	STD-AS	STD-MK	STD-MC	STD-EI	STD-VE	
MEAN	0.23	0.03	-0.00	-0.23	0.06	0.06	-0.15	0.05	0.01	-0.03	0.08	
S.D. N	-0.09 -153.0	-0.01 -153.0	0.09	-0.13 -153 0	0.05	0.03 -153.0	0.03	0.03	-0.04 -153 0	0.08	0.13 -153.0	
FORM 20b Standard Score Correlation Differences from the Reference FORM (15h)												
Subtest												
STD-GS STD-AR	0.00 0.01	0.01	0.02 -0.00	0.02 -0.04	0.02 -0.01	0.03	-0.09 -0.05	0.07 0.01	-0.03 0.01	-0.04 -0.02	0.02 -0.02	
STD-WK	0.02	-0.00	0.00	0.01	-0.01	0.02	-0.02	0.02	0.02	-0.02	0.01	
STD-PC	0.02	-0.04	0.01	0.00	-0.03	0.01	-0.06	-0.01	0.01	-0.02	-0.01	
STD-NO STD-CS	0.02	-0.01 0.02	-0.01 0.02	-0.03 0.01	0.00 -0.02	-0.02 0.00	-0.02 -0.00	-0.03 -0.02	0.03 0.04	0.03	-0.02 0.01	
STD-AS	-0.09	-0.05	-0.02	-0.06	-0.02	-0.00	0.00	-0.00	-0.06	-0.06	-0.03	
STD-MK	0.07	0.01	0.02	-0.01	-0.03	-0.02	-0.00	0.00		0.07	0.00	
STD-MC STD-EI	-0.03 -0.04	0.01 -0.02	0.02 -0.02	0.01 -0.02	0.03	0.04	-0.06 -0.06	0.04	0.00	-0.02 0.00	0.02 -0.02	
· STD-VE	0.02	-0.02	0.01	-0.01	-0.02	0.01	-0.03	0.00	0.02	-0.02	0.00	
FORM	20b St	andard :	Score S	tatisti	c Diffe:	rences :	from the	e Opera	tional 1	FORM (1	5g)	
Subtest	STD-GS	STD-AR	STD-WK	STD-PC	STD-NO	STD-CS	STD-AS	STD-MK	STD-MC	STD-EI	STD-VE	
MEAN	0.04	0.29	-0.28	-0.49	0.34	-0.18	-0.13	-0.06	-0.17	0.11	-0.15	
S.D. N	0.09	-0.03 -534.0	0.15 -534.0	0.06	0.11	0.09 -534.0	-0.04	0.04	0.20 -534.0	-0.42 -534.0	0.08	
N	-334.0	-334.0	-334.0	-334.0	-334.0	-334.0	-334.0	-334.0	-334.0	-334.0	-334.0	
FORM :	20b Sta	ndard S	core Co	rrelati	on Diff	erences	from t	he Oper	ational	FORM (	15g)	
Subtest									STD-MC		STD-VE	
STTD-GS	0.00	-0.00	0.04	-0.01	0.04	0.02	-0.04	0.05	-0.03	0.03	0.04	
STD-AR STD-WK	-0.00 0.04	0.00 -0.01	-0.01 0.00	-0.01 -0.06	0.02 -0.02	-0.02	-0.00 0.07	0.03	-0.00 0.06	0.04 0.11	-0.00 -0.00	
STD-PC	-0.01	-0.01	-0.06	0.00	0.03	0.04	0.00	0.02	0.04	0.06	-0.04	
STD-NO	0.04	0.02	-0.02	0.03	0.00	-0.04	0.04	-0.00	0.04	0.06	-0.00	
STD-CS STD-AS	0.02 -0.04	0.00 -0.00	-0.02 0.07	0.04	-0.04 0.04	0.00 0.04	0.04	-0.03 0.05	0.05 0.01	0.05 -0.04	0.00	
STD-MK	0.05	0.03	0.02	0.02	~0.00	-0.03	0.05	0.00	0.03	0.10	0.03	
STD-MC	-0.03	-0.00	0.06	0.04	0.04	0.05	0.01	0.03	0.00	0.05	0.06	
STD-EI STD-VE	0.03	0.04 -0.00	0.11 -0.00	0.06 -0.04	0.06 -0.00	0.05	-0.04 0.06	0.10	0.05	0.00 0.11	0.11	
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## Subtest Means, Standard Deviations, and Intercorrelations, after Application of Current Conversion Tables

FORM 21a Standard Score Statistics												
Subtest MEAN S.D.	STD-GS 50.85 8.60	STD-AR 51.33 8.49	STD-NK 51.74 6.93	STD-PC 51.71 7.43	STD-NO 53.09 7.78	STD-CS 52.58 7.62	STD-AS 50.88 8.99	STD-MK 52.35 8.66	STD-MC 52.00 9.25	STD-BI 50.32 8.51	STD-VE 51.81 6.92	
N.	12532	12532	12532	12532	12532	12532	12532	12532	12532	12532	12532	
			FORM	21a Sta	ndard S	core Co	rrelati	ons				
Subtest												
STD-GS STD-AR	1.00	0.60 1.00	0.72 0.58	0.61 0.56	0.29 0.44	0.28 0.40	0.36 0.37	0.61 0.72	0.58 0.62	0. <b>54</b> 0. <b>49</b>	0.74 0.61	
STD-WK	0.72	0.58	1.00	0.70	0.29	0.31	0.37	0.49	0.54	0.54	0.97	
STD-PC	0.61	0.56	0.70	1.00	0.33	0.34	0.36	0.45	0.50	0.48	0.84	
STD-NO STD-CS	0.29 0.28	0.44	0.29 0.31	0.33 0.34	1.00 0.63	0.63 1.00	0.03	0.43	0.19 0.23	0.10 0.14	0.32 0.34	
STD-AS	0.26	0.37	0.37	0.34	0.03	0.06	1.00	0.36 0.17	0.60	0.67	0.39	
STD-MK	0.61	0.72	0.49	0.45	0.43	0.36	0.17	1.00	0.50	0.34	0.51	
STD-MC	0.58	0.62	0.54	0.50	0.19	0.23	0.60	0.50	1.00	0.68	0.57	
STD-EI STD-VE	0.54 0.74	0.49 0.61	0.54 0.97	0.48 0.84	0.10 0.32	0.14 0.34	0.67 0.39	0.34 0.51	0.68 0.57	1.00 0.56	0.56 1.00	
		tandard										
											-•	
Subtest MEAN	0.04	-0.01	0.01	-0.09	-0.02	-0.01	-0.03	511D-MK 0.02	0.12	-0.14	SID-VE 0.01	
S.D.	0.05	-0.04	-0.01	-0.22	0.00	-0.04	0.10	0.02	-0.07	0.03	0.10	
N	-399.0											
N -399.0												
Subtest	STD-GS	STD-AR	STD-WK	STD-PC	STD-NO		STD-AS	S'ID-MK	STD-MC	STD-EI	STD-VE	
SID-GS	0.00	0.00	0.00	0.05	0.06	0.05	-0.23	0.08	-0.08	-0.15	0.02	
STD-AR STD-WK	0.00	0.00 -0.01	-0.01 0.00	-0.02 0.04	-0.00 0.01	0.03 0.02	-0.07 -0.11	-0.01 -0.01	0.01 -0.00	-0.04 -0.06	-0.02 0.01	
STD-PC	0.05	-0.02	0.04	0.00	-0.05	-0.03	-0.00	-0.06	0.05	0.01	0.00	
STD-NO	0.06	-0.00	0.01	-0.05	0.00	-0.00	-0.07	-0.04	-0.00	-0.06	-0.02	
STD-CS STD-AS	0.05 -0.23	0.03 -0.07	0.02 -0.11	-0.03 -0.00	-0.00 -0.07	0.00 -0.04	-0.04 0.00	-0.04 -0.08	0.02 -0.07	-0.04	-0.00 -0.09	
STD-MK	0.08	-0.01	-0.01	~0.06	-C.04	-0.04	-0.08	0.00	0.02	-0.01 -0.06	-0.03	
STD-MC	-0.08	0.01	-0.00	0.05	-0.00	0.02	-0.07	0.02	0.00	0.01	0.01	
STD-EI	-0.15	-0.04	-0.06	0.01	-0.06	-0.04	-0.01	-0.06	0.01	0.00	-0.05	
STD-VE	0.02	-0.02	0.01	0.00	-0.02	-0.00	-0.09	-0.03	0.01	-0.05	0.00	
		andard S						_			_	
Subtest MEAN	-0.15	STD-AR 0.26	-0.26	-0.35	STD-NO 0.25	STD-CS -0.25	STD-AS -0.01	-0.09	STD-MC -0.07	STD-EI -0.00	STD-VE -0.22	
S.D.	0.24	-0.07	0.05	-0.03	0.06	0.03	0.03	0.03	0.18	-0.48	0.05	
N		-780.0			-780.0							
EYYDM	21a Sta	ndard S	cone Co	melati	on Diff	evences	from t	he Oner	ational	ECOM /	15~\	
Subtest	STD-GS	STD-AR	STD-WK	STD-PC	STD-NO	STD-CS	STD-AS	STD-MK	STD-MC	STD-EI	SID-VE	
STD-GS	0.00	-0.01	0.02	0.02	0.07	0.05	-0.18	0.06	-0.08	-0.08	0.03	
STD-AR	-0.01	0.00	-0.01	0.01	0.02	0.01	-0.02	0.01	-0.00	0.01	-0.00	
STD-WK STD-PC	0.02	-0.01 0.01	0.00 -0.03	-0.03 0.00	0.00	-0.02 -0.00	-0.03 0.06	-0.01 -0.02	0.03	0.07 0.09	0.00 -0.02	
STD-NO	0.07	0.02	0.00	0.01	0.00	-0.02	-0.00	-0.01	0.01	-0.03	0.00	
STD-CS	0.05	0.01	-0.02	-0.00	-0.02	0.00	0.00	-0.04	0.04	-0.02	-0.02	
STD-AS	-0.18 0.06	-0.02 0.01	-0.03 -0.01	0.06 -0.02	-0.00 -0.01	0.00 -0.04	0.00	-0.02	-0.00	0.02	-0.00	
STD-MK STD-MC	-0.08	-0.00	0.03	0.02	0.01	0.04	-0.02 -0.00	0.00	0.00	-0.02 0.08	-0.01 0.05	
STD-EI	-0.08	0.01	0.07	0.09	-0.03	-0.02	0.02	-0.02	0.08	0.00	0.08	
STD-VE	0.03	-0.00	0.00	-0.02	0.00	-0.02	-0.00	-0.01	0.05	0.08	0.00	

# Subtest Means, Standard Deviations, and Intercorrelations, after Application of Current Conversion Tables

FORM 21b Standard Score Statistics												
Subtest MEAN S.D. N	STD-GS 50.92 8.44 12060	STD-AR 51.46 8.53 12060	STD-WK 51.68 6.87 12060	STD-PC 51.68 7.62 12060	STD-NO 53.02 7.76 12060	STD-CS 52.58 7.62 12060	STD-AS 50.96 8.84 12060	STD-MK 52.36 8.62 12060	STD-MC 52.16 9.19 12060	STD-EI 50.60 8.39 12060	STD-VE 51.82 6.85 12060	
			FORM	21b Sta	ndard S	core Co	rrelati	ons.				
Subtest SID-GS SID-AR SID-WK SID-PC SID-NO SID-CS SID-AS SID-MK SID-MC	STD-GS 1.00 0.58 0.72 0.62 0.30 0.35 0.59	STD-AR 0.58 1.00 0.55 0.55 0.43 0.39 0.31 0.69 0.58	STD-WK 0.72 0.55 1.00 0.70 0.28 0.32 0.40 0.46 0.56	STD-PC 0.62 0.55 0.70 1.00 0.34 0.36 0.29 0.46 0.49	STD-NO 0.30 0.43 0.28 0.34 1.00 0.63 0.02 0.42 0.19	STD-CS 0.30 0.39 0.32 0.36 0.63 1.00 0.06 0.38 0.23	STD-AS 0.35 0.31 0.40 0.29 0.02 0.06 1.00 0.15	STD-MK 0.59 0.69 0.46 0.42 0.38 0.15 1.00 0.49	STD-MC 0.57 0.58 0.56 0.49 0.19 0.23 0.59 0.49 1.00	STD-EI 0.55 0.44 0.56 0.45 0.11 0.15 0.67 0.34 0.68	SID-VE 0.74 0.59 0.97 0.86 0.32 0.36 0.39 0.50	
SID-EI SID-VE	0.55 0.74	0.44 0.59	0.56 0.97	0.45 0.86	0.11 0.32	0.15 0.36	0.67 0.39	0.34 0.50	0.68 0.58	1.00 0.56	0.56 1.00	
FORM	1 21b Si	andard	Score s	Statist	ic Diffe	erences	from t	he Refe	rence R	ORM (15)	a)	
Subtest MEAN S.D. N	0.11 -0.12	0.13 -0.00	-0.05 -0.07	-0.12 -0.03	-0.10 -0.02	-0.01 -0.03	0.05	0.04	0.28 -0.12	STD-EI 0.14 -0.09 -871.0	0.02	
FORM 21b Standard Score Correlation Differences from the Reference FORM (15h)												
Subtest SID-GS SID-AK SID-PC SID-NO SID-SS SID-AS SID-MK SID-MC SID-EI SID-VE	STD-GS 0.00 -0.02 0.00 0.07 0.08 -0.23 0.06 -0.08 -0.14	SID-AR -0.02 0.00 -0.04 -0.03 -0.02 -0.13 -0.04 -0.03 -0.09	SID-WK 0.00 -0.04 0.00 0.05 -0.01 0.03 -0.08 -0.04 0.01 -0.04	STD-PC 0.07 -0.03 0.05 0.00 -0.04 -0.02 -0.07 -0.05 0.03 -0.03	STD-NO 0.07 -0.02 -0.01 -0.04 0.00 -0.01 -0.07 -0.05 -0.01 -0.05	SID-CS 0.08 0.02 0.03 -0.02 -0.01 0.00 -0.05 -0.02 0.03 -0.02	SID-AS -0.23 -0.13 -0.08 -0.07 -0.05 0.00 -0.09 -0.07 -0.01	STD-MK 0.06 -0.04 -0.05 -0.05 -0.02 -0.09 0.00 0.01 -0.06	SID-MC -0.08 -0.03 0.01 0.03 -0.01 0.03 -0.07 0.01 0.00 0.01	SID-BI -0.14 -0.09 -0.04 -0.05 -0.05 -0.02 -0.01 -0.06 0.01 0.00	STD-VE 0.02 -0.04 0.00 0.02 -0.02 -0.09 -0.05 0.02 -0.09	
FORM	21b Sta	andard S	Score St	tatistic	Differ	rences i	Erom th	e Operat	cional 1	FORM (19	śg)	
Subtest MEAN S.D. N	STD-GS -0.08 0.07 -1252	STD-AR 0.39 -0.03 -1252	STD-WK -0.32 -0.01 -1252	STD-PC -0.39 0.17 -1252	STD-NO 0.18 0.04 -1252	STD-CS -0.25 0.04 -1252	STD-AS 0.07 -0.11 -1252	STD-MK -0.07 -0.01 -1252	STD-MC 0.09 0.12 -1252	STD-EI 0.27 -0.60 -1252	STD-VE -0.21 -0.02 -1252	
FORM 2	lb Star	ndard So	core Cor	rrelatio	on Diffe	erences	from t	he Opera	ational	FORM (	L5g)	
Subtest STD-GS STD-AR STD-WK STD-PC STD-NC STD-CS STD-AS STD-MK STD-MK STD-EI STD-VE	STD-GS 0.00 -0.04 0.02 0.04 0.08 0.07 -0.18 0.05 -0.08 -0.07	STD-AR -0.04 0.00 -0.04 -0.00 0.01 -0.08 -0.02 -0.04 -0.03 -0.03	SID-WK 0.02 -0.04 0.00 -0.02 -0.01 0.00 -0.03 0.05 0.09 -0.01	SID-PC 0.04 -0.00 0.02 0.01 0.02 -0.01 -0.01 0.07 9.06 -0.00	SID-NO 0.08 0.01 -0.02 0.01 0.00 -0.03 -0.01 -0.02 0.01 -0.02	SID-CS 0.07 0.01 -0.01 0.02 -0.03 0.00 0.00 -0.02	SID-AS -0.18 -0.08 0.00 -0.01 -0.01 0.00 0.00 -0.04 -0.01 0.02 0.00	STD-MK 0.05 -0.02 -0.03 -0.01 -0.02 -0.02 -0.04 0.00 -0.01 -0.02 -0.03	SID-MC -0.08 -0.04 0.05 0.07 0.01 -0.01 -0.01 0.00 0.08	SID-EI -0.07 -0.03 0.09 0.06 -0.02 -0.00 0.02 -0.02 0.08 0.09	STD-VE 0.03 -0.03 -0.00 -0.00 -0.00 0.00 -0.03 0.06 0.09 0.00	

# Subtest Means, Standard Deviations, and Intercorrelations, after Application of Current Conversion Tables

FORM 22a Standard Score Statistics														
O	Subtest STD-GS STD-AR STD-WK STD-PC STD-NO STD-CS STD-AS STD-MK STD-MC STD-EI STD-VE													
MEAN	50.89	51.40	51.76	51.68	53.15	52.58	50.99	52.33	52.13	50.30	51.86			
S.D.	8.56	8.56	6.93	7.36	7.80	7.70	8.91	8.57	9.22	8.62	7.05			
N	11558	11558	11558	11558	11558	11558	11558	11558	11558	11558	11558			
			FORM	22a Sta	ndard S	core Co	rrelati	ons						
Subtest														
STD-GS STD-AR	1.00 0.59	0.59 1.00	0.76 0.59	0.63 0.57	0.26 0.41	0.27 0.39	0.49	0.56 0.72	0.60 0.60	0.61 0.49	0.77 0.63			
STD-WK	0.76	0.59	1.00	0.69	0.28	0.32	0.42	0.51	0.54	0.55	0.97			
STD-PC	0.63	0.57	0.69	1.00	0.36	0.37	0.33	0.50	0.48	0.46	0.84			
STD-NO STD-CS	0.26 0.27	0.41 0.39	0.28 0.32	0.36 0.37	1.00 0.63	0.63 1.00	0.04 0.06	0.45 0.40	0.17 0.20	0.15 0.18	0.33 0.36			
STD-AS	0.49	0.39	0.42	0.33	0.04	0.06	1.00	0.21	0.65	0.10	0.42			
STD-MK	0.56	0.72	0.51	0.50	0.45	0.40	0.21	1.00	0.49	0.39	0.55			
STD-MC	0.60	0.60	0.54	0.48	0.17	0.20	0.65	0.49	1.00	0.66	0.56			
STD-EI STD-VE	0.61 0.77	0.49 0.63	0.55 0.97	0.46 0.84	0.15 0.33	0.18 0.36	0.67 0.42	0.39 0.55	0.66 0.56	1.00 0.56	0.56 1.00			
			Score S											
										•	•			
Subtest MEAN	51D-GS 0.07	0.06	0.03	-0.11	0.04	-0.01	SID-AS 0.08			STD-EI				
S.D.	0.01	0.02	-0.01	-0.29	0.02	0.05	0.03	0.00 -0.08	0.25 -0.10	-0.16 0.13	0.06 0.23			
N	-1373	-1373	-1373	-1373	-1373	-1373	-1373	-1373	-1373	-1373	-1373			
FORM	22a Sta	andard s	Score Co	orrelati	ion Difi	ference	s from	the Ref	erence l	PORM (15	ih)			
Subtest	STD-GS	STD-AR	STD-WK	STD-PC	STD-NO	STD-CS	STD-AS	STD-MK	STD-MC	STD-EI	STD-VE			
STD-GS	0.00	-0.01	0.04	0.07	0.02	0.05	-0.09	0.03	-0.05	-0.07	0.05			
STD-AR STD-WK	-0.01 0.04	0.00 0.01	0.01 0.00	-0.01 0.03	-0.04 -0.00	0.02 0.03	-0.05 -0.07	-0.01 0.01	-0.01 -0.01	-0.04 -0.04	-0.90 0.01			
STD-PC	0.07	-0.01	0.03	0.00	-0.02	-0.01	-0.03	-0.01	0.02	-0.02	0.01			
SID-NO	0.02	-0.04	-0.00	-0.02	0.00	-0.01	-0.05	-0.02	-0.02	-0.01	-0.02			
SID-CS	0.05	0.02	0.03	-0.01	-0.01	0.00	-0.04	0.00	-0.00	0.01	0.02			
STD-AS STD-MK	-0.09 0.03	-0.05 -0.01	-0.07 0.01	-0.03 -0.01	-0.05 -0.02	-0.04 0.00	0.00 -0.04	-0.04 0.00	-0.01 0.00	-0.01 -0.01	-0.06 0.00			
STD-MC	-0.05	-0.01	-0.01	0.02	-0.02	-0.00	-0.01	0.00	0.00	-0.01	0.00			
SID-EI	-0.07	-0.04	-0.04	-0.02	-0.01	0.01	-0.01	-0.01	-0.01	0.00	-0.04			
STD-VE	0.05	-0.00	0.01	0.01	-0.02	0.02	-0.06	0.00	0.00	-0.04	0.00			
FORM	22a Sta	andard !	Score St	atistic	Diffe	rences i	from the	e Operat	tional !	PORM (19	ig)			
Subtest														
MEAN S.D.	-0.12 0.20	0.33	-0.24 0.05	-0.38 -0.09	0.31	-0.25 0.11	0.10 -0.05	-0.11 -0.07	0.06 0.14	-0.02 -0.38	-0.17 0.18			
N.D.	-1754	-1754	-17	-1754	-1754	-1754	-1754	-1754	-1754	-1754	-1754			
FORM 2	22a Sta	ndard S	core Cor	relatio	n Diffe	erences	from t	he Opera	ational	FORM (2	L5g)			
Subtest														
STD-GS	0.00	-0.03	0.06	0.05	0.04	0.05	-0.04	0.02	-0.05	-0.01	0.07			
STD-AR STD-WK	-0.03 0.06	0.00 -0.00	-0.00	0.02 -0.04	-0.01 -0.01	0.00 -0.01	-0.00 0.02	0.01 0.02	-0.02 0.03	0.02 0.08	0.01 -0.00			
STD-PC	0.05	0.02	-0 1	0.00	0.03	0.03	0.02	0.02	0.06	0.08	-0.02			
STD-NO	0.04	-0.01	-0.01	0.03	0.00	-0.03	0.01	0.01	-0.01	0.02	0.01			
SID-CS	0.05	0.00	-0.01	0.03	-0.03	0.00	0.01	-0.00	0.01	0.03	0.00			
STD-AS STD-MK	-0.04 0.02	-0.00 0.01	0.02 0.02	0.03	0.01 0.01	0.01 -0.00	0.00	0.02 0.00	0.06 -0.01	0.02	0.03 0.03			
STD-MC	-0.05	-0.02	0.03	0.06	-0.01	0.01	0.06	-0.01	0.00	0.06	0.04			
STD-EI	-0.01	0.02	0.08	0.07	0.02	0.03	0.02	0.03	0.06	0.00	0.09			
STD-VE	0.07	0.01	-0.00	-0.02	0.01	0.00	0.03	0.03	0.04	0.09	0.00			

## Subtest Means, Standard Deviations, and Intercorrelations, after Application of Current Conversion Tables

			FORM	22b St	andard	Score S	Statisti	.C8	<u>-</u>		
Subtest											
MEAN S.D.	50.88 8.52	51.34 8.49	51.71 6.92	51.64 7.54	53.02 7.77	52.57 7.53	50.85 8.94	52.39 8.60	52.03 9.20	50.60 8.46	51.84 6.86
N.	10986	10986	10986	10986	10986	10986	10986	10986	10986	10986	10986
			FORM	22b Sta	ndard S	core Co	rrelati	.ons			
Subtest	STD-GS	STD-AR	STD-WK	STD-PC	STD-NO		STD-AS	STD-MK	STD-MC	STD-BI	STD-VE
STD-GS		0.60	0.75	0.66	0.26	0.28	0.50	0.55	0.61	0.62	0.77
STD-AR		1.00	0.58	0.60	0.42	0.40	0.41	0.72	0.59	0.50	0.63
STD-WK STD-PC		0.58 0.60	1.00 0.72	0.72 1.00	0.27 0.38	0.32 0.40	0.44 0.36	0.48 0.52	0.55 0.49	0.56 0.49	0.97 0.87
STD-NO		0.42	0.27	0.38	1.00	0.62	0.06	0.42	0.18	0.16	0.33
STD-CS	0.28	0.40	0.32	0.40	0.62	1.00	0.08	0.38	0.21	0.18	0.37
STD-AS		0.41	0.44	0.36	0.06	0.08	1.00	0.24	0.67	0.67	0.45
STD-MK		0.72	0.48	0.52	0.42	0.38	0.24	1.00	0.51	0.40	0.53
STD-MC STD-EI		0.59 0.50	0.55 0.56	0.49 0.49	0.18 0.16	0.21 0.18	0.67 0.67	0.51 0.40	1.00 0.66	0.66 1.00	0.57 0.57
STD-VE		0.63	0.97	0.87	0.33	0.37	0.45	0.53	0.57	0.57	1.00
FOR	M 22b S						from t		rence R	ORM (15)	a)
Subtest	STD-GS	STD-AP	SID-MK	SEL-BC	STD-NO	STD-CS	STD-AS	STD-MK	STO-MC	STD-RT	STD-VE
MEAN	0.07	-0.00	-0.02	-0.16	-0.09	-0.02	-0.07	0.06	0.15	0.15	0.04
S.D.	-0.03	-0.05	-0.02	-0.11	-0.01	-0.12	0.06	-0.04	-0.12	-0.02	0.04
N	-1945	-1945	-1945	-1945	-1945	-1945	-1945	-1945	-1945	-1945	-1945
FORM	22b St	andard :	Score C	orrelat	ion Dif	ference	s from	the Ref	erence 1	FORM (15	5h)
Subtest	STD-GS	STD-AR	STD-WK	STD-PC	STD-NO	STD-CS	STD-AS	STD-MK	STD-MC	STD-EI	STD-VE
STD-GS		0.00	0.03	0.10	0.02	0.06	-0.08	0.02	-0.05	-0.07	0.05
STD-AR		0.00	-0.01	0.03	~0.03	0.03	-0.03	-0.01	-0.01	-0.03	-0.00
STD-WK STD-PC		-0.01 0.03	0.00 0.06	0.06	-0.01 -0.00	0.03			0.00	-0.04 0.01	0.00 0.04
STD-NO		-0.03	-0.01	-0.00	0.00	-0.01		-0.05	-0.01	0.00	-0.01
STD-CS		0.03	0.03	0.03	-0.01	0.00			0.00	0.01	0.03
STD-AS		-0.03	-0.04	-0.00		-0.02				-0.01	-0.04
STD-MK		-0.01	-0.02	0.01	-0.05	-0.02	-0.00		0.02	-0.00	-0.02
STD-MC		-0.01	0.00	0.03	-0.01	0.00		0.02	0.00	-0.00	0.01
STD-EI		-0.03	-0.04	0.01	0.00	0.01	-0.01	-0.00	-0.00	0.00	-0.03
STD-VE	0.05	-0.00	0.00	0.04	-0.01	0.03	-0.04	-0.02	0.01	-0.03	0.00
FORM	22b St	andard :	Score S	tatisti	c Diffe	rences	from th	e Opera	tional 1	FORM (1	5g)
Subtest											
MEAN	-0.13	0.26		-0.42	0.18	-0.26	-0.04	-0.05	-0.04	0.28	-0.19
S.D. N	0.16 -2326	-0.07 -2326	0.04 -2326	0.08 -2326	0.06 -2326	-0.06 -2326	-0.01 -2326	-0.03 -2326	0.13 -2326	-0.53 -2326	-0.01 -2326
-	-2320 22b Sta										
	STD-GS							_			
STD-GS		-0.02	0.05	0.08	0.04	0.06	-0.03	0.01	-0.04	-0.00	0.07
STD-AR		0.00	-0.01	0.06	0.00	0.01	0.01	0.01	-0.03	0.02	0.01
SID-WK		-0.01	0.00	-0.00	-0.02		0.05		0.04	0.09	-0.01
SID-PC	0.08	0.06	-0.00	0.00	າ.05	0.06	0.06	0.05	0.07	0.10	0.01
SID-NO		0.00	-0.02	0.05	0.00			-0.02	-0.00	0.04	0.01
STD-CS		0.01	-0.01	0.06	-0.03	0.00			0.02	0.03	0.02
STD-AS STD-MK		0.01		0.06						0.02	0.05
STD-MC		0.01 -0.03	-0.02 0.04	0.05 0.07	-0.02 -0.00			0.00		0.03 0.06	0.01 0.05
SID-EI		0.02	0.09	0.10	0.04	0.02			0.06	0.00	0.10
STD-VE		0.01	-0.01	0.01	0.01	0.02			0.05	0.10	0.00

Table 12 Subtests and Upper Bounds of Categories for Composites

	· · · · · · · · · · · · · · · · · · ·	
<u>Comp</u> AFQT	osite ** 2VE + AR + MK	<u>Category Upper Bounds</u> 09/15/20/30/49/64/92/99
~~	ARMY**	100) 160
GT	VE + AR	109\160
GM EL	MK + EI + AS + GS AR + MK + EI + GS	84/89/94/99/104/160 84/89/94/99/104/109/114/119/160
CL	AR + MK + EI + GS AR + MK + VE	84/89/94/99/104/109/114/119/160
MM	NO + AS + MC + EI	
SC		
CO	AR + AS + MC + VE CS + AR + MC + AS AR + CS + MC + MK	84/89/94/99/160
FA	AR + CS + MC + MK	84/89/94/99/160
OF	NO + AS + MC + VE	
ST	VE + MK + MC + GS	84/89/94/99/104/109/114/160
	NAVY***	100 /100 /000 /010 /000
EL	AR + MK + EI + GS AR + GS + 2MK	189/199/203/217/320 195/199/203/209/213/320
E CL	NO + CS + VE	159/240
GT	VE + AR	88/95/96/102/107/112/114/160
ME	VE + MC + AS	149/157/166/240
EG	MK + AS	95/160
CT	VE + AR + NO + CS	201/320
HM	VE + MK + GS	148/164/240
ST	VE + AR + MC	146/240
MR	AR + MC + AS	129/157/163/240
BC	VE + MK + CS	146/152/240
	AIR FORCE*	
М	MC + GS + 2AS	43/44/50/56/60/88/99
Α	NO + CS + VE	26/31/39/44/50/60/66/99
G	VE + AR	29/34/38/41/42/47/49/
		52/55/57/63/68/69/99
E	AR + MK + EI + GS	32/38/42/44/45/49/57/
		66/71/76/80/99
	MARINE CORPS**	
MM	AR + EI + MC + AS	84/94/104/114/160
$C\Gamma$	VE + MK + CS	79/89/99/109/119/160
GT	VE + AR + MC	79/89/99/109/160
$\mathtt{EL}$	AR + MK + EI + GS	89/99/109/114/160

Percentile Scores; AFQT upper bounds are for categories V, IVc, IVb, IVa, IIIb, IIIa, II and I, respectively. Standard Scores (Mean=100, S.D.=20). Sum of Subtest Standard Scores.

Table 13

Composite-Category-by-Test-Form Chi-Squares (Reference, Operational, & New [20-22] Forms)

Compo AFQT	Osite 2VE + AR + MK	D.F. 49	<u>Chi-Square</u> 148.836*	Prob 000
		ARMY		
GT	VE + AR	7	6.824	.447
GM.	MK + EI + AS + GS	35	88.814*	.000
EL	AR + MK + EI + GS	56	108.241	.000
$\alpha$	AR + MK + VE	42	46.701	.285
MM	NO + AS + MC + EI	28	81.825*	.000
SC	AR + AS + MC + VE	28	41.266	.051
$\infty$	CS + AR + MC + AS	28	39.739	.070
FA	AR + CS + MC + MK	28	27.037	.516
OF	NO + AS + MC + VE	28	75.452*	.000
ST	VE + MK + MC + GS	49	67.870	.038
		AIR FORCE		
M	MC + GS + 2AS	42	246.198*	.000
A	NO + CS + VE	49	47.891	.516
G	VE + AR	84	186.039*	.000
E	AR + MK + EI + GS	77	99.539	.043
		NAVY		
EL	AR + MK + EI + GS	28	55.575	.001
E	AR + GS + 2MK	35	41.523	.208
$\mathbf{cr}$	NO + CS + VE	7	3.043	.881
GT	VE + AR	49	81.834	.002
ME	VE + MC + AS	21	33.496	.041
EG	MIK + AS	7	12.859	.076
CT	VE + AR + NO + CS	7	3.029	.882
HM	VE + MK + GS	14	21.252	.095
ST	VE + AR + MC	7	8.277	.309
MR	AR + MC + AS	21	39.759	.008
BC	VE + MK + CS	14	14.767	.394
	M	ARINE CORPS		
MM	AR + EI + MC + AS	28	59.689*	.000
αт	VE + MK + CS	35	37.329	.362
GT	VE + AR + MC	28	27.560	.488
EL	AR + MK + EI + GS	28	59.054*	.001

<sup>\*</sup> Chi-Square > 2 x D.F.

(continued)

Composite-Category-by-Test-Form Chi-Squares
(Reference Form vs. Operational 15G and Each New Form [20-22])

Como.	DE	15G	20A	20B	21A	21B	22A	22B
	1 7 1					· ·		_ :
AFQT ARMY	1 / 1	30.392*	14.31/-	26.029"	12.950	12.192	20.080*	5.961
GM ELL MM SC FA FA FST	15864447	1.674 13.844* 6.414 5.547 19.411* 4.093 3.747 3.083 22.092* 12.709	0.359 4.455 5.586 11.266 11.960* 3.505 4.527 2.953 5.520 9.239	0.389 2.538 12.441 7.564 5.609 0.326 1.299 2.830 4.567 13.169	0.552 13.408* 20.021* 8.003 12.627* 7.379 5.427 1.759 6.357 11.821	0.048 22.825* 18.656* 15.443* 6.387 13.473* 16.025* 5.309 14.736* 9.143	1.046 6.901 13.078 3.604 0.999 1.549 2.801 0.877 5.048 7.200	0.081 5.831 10.193 9.240 2.958 1.878 3.954 2.948 1.593 9.658
AIR FORC	Œ							
M A G E	6 7 12 11	47.080* 3.256 26.608* 4.071	45.779* 5.204 -1.061* 4.638	35.388* 3.065 39.105* 13.596	30.692* 7.111 18.188 18.648	81.012* 5.108 15.273 16.120	72.520* 5.662 24.736* 13.705	78.533* 1.532 20.801 6.903
NAVY								
日年じら無路じまな所名	4 5 1 7 3 1 1 2 1 3 2	2.970 13.914* 0.463 8.537 7.868* 1.098 1.459 5.134* 0.779 5.041 2.591	2.611 6.089 0.012 12.277 6.325* 0.185 0.003 8.722* 1.898 5.794 1.555	16.136* 5.744 0.248 17.604* 6.752* 0.486 0.248 7.872* 0.083 1.874 1.498	7.174 4.815 0.013 7.132 3.670 2.694* 0.325 11.208* 0.703 9.325* 4.662*	10.507* 2.925 0.609 12.790 6.349* 3.193* 1.379 3.928 0.838 24.528* 1.808	9.986* 8.822 0.133 15.217* 1.992 0.084 0.383 6.277* 0.121 3.353 1.268	2.707 7.704 0.221 19.714* 3.190 0.319 0.181 1.772 0.347 5.199 2.885
MARINE (	CORPS							
MM CL GT EL	4 5 4 4	20.082* 8.445 3.947 5.349	9.286* 2.459 4.085 3.404	4.745 3.872 2.480 11.176	10.726* 4.535 4.514 12.050*	23.985* 5.932 5.471 10.601	0.685 2.762 1.484 4.397	7.453 1.195 3.847 5.470

Table 14
Standard Deviations of Composites

Comp.	15H	15G	20A	20B	21A	21B	22A	22B
AFQT P	ERCENTILE							
AFQT	23.932	23.961	23.925	24.179	23.935	23.777	24.334	23.975
army st	'ANDARD SO	ORE						
GT GM	15.003	15.012 16.004	15.004 15.900	15.040 16.077	14.974 15.546	14.838 15.277	15.232 15.914	14.991 15.934
EL.	16.010	15.918	16.068	16.156	15.773	15.483	15.892	15.807
<u>cr</u>	15.375	15.284	15.394	15.466	15.284	15.088	15.462	15.291
MM	15.870	15.551	15.604	15.745	15.574	15.409	15.727	15.744
SC	16.221	15.791	16.048	16.077	15.911	15.611	16.098	16.072
$\infty$	16.183	15.808	16.059	16.090	15.922	15.649	15.998	16.011
FA	16.025	15.928	16.159	16.197	16.032	15.884	15.970	15.911
OF	15.043		14.959	14.977	14.685	14.544	14.857	14.878
ST	15.836	15.597	16.039	16.026	15.906	15.684	15.911	15.822
AIR FOR	CE PERCEN	TILE						
М	25.967		25.327	25.400	24.853	24.500	25.554	25.640
A	23.821	24.014	23.882	24.001	23.764	23.820	24.157	23.799
G	23.878	23.912	23.870	24.129	23.886	23.729	24.281	23.924
E	23.904	23.760	23.981	24.133	23.639	23.202	23.783	23.644
VAVY SS	SS							
缸	28.318		28.423	28.577	27.900	27.393	28.103	27.963
E	30.071	29.951	30.378	30.446	30.463	29.999	30.065	30.011
GT.	17.686	17.653	17.726	17.738	17.658	17.611	17.875	17.618
GT ME	13.882	13.886	13.886	13.920	13.859	13.729	14.097	13.874
ME EG	21.254 13.825	20.478 13.550	21.010	21.097 13.851	20.854 13.474	20.644 13.250	21.137 13.582	21.163 13.821
CT	23.794	23.716	23.773	23.846	23.783	23.650	23.964	23.700
	20.508	20.326	20.876	20.868	20.889	20.544	20.932	20.673
				23.846	23.783	23.650	23.964	23.700
HM		23.7161	23.//41				,	,,,,,
HM ST	23.794	23.716 22.134	23.773				22.340	22.387
HM		22.134	22.262	22.282	22.172	21.667 18.021	22.340 18.435	
HM ST MR BC	23.794 22.632	22.134 18.188	22.262 18.264	22.282	22.172	21.667		
HM ST MR BC	23.794 22.632 18.220 CORPS STAI	22.134 18.188 NDARD SCO	22.262 18.264 )RE	22.282 18.344	22.172 18.031	21.667 18.021	18.435	18.107
HM ST MR BC MARINE	23.794 22.632 18.220 CORPS STAI	22.134   18.188   NDARD SCO   16.623	22.262 18.264 RE 16.459	22.282 18.344	22.172 18.031	21.667 18.021		22.387 18.107 16.653 14.151
HM ST MR BC MARINE MM	23.794 22.632 18.220 CORPS STAI	22.134   18.188   NDARD SCO   16.623   14.219	22.262 18.264 )RE	22.282 18.344	22.172 18.031	21.667 18.021	18.435 16.688	18.107

Table 15

Composite-Category-by-Test-Form Chi-Square for ASVAB 15/16/17,

After Equatings Based on IOT&E of ASVAB 15/16/17

			•	
Comp	osite	D.F.	Chi-Square	Prob.
AFQ1	2VE + AR + MK	42	161.889*	.000
GT GM ELL CL MM SC OF OF ST	ARMY  VE + AR  MK + EI + AS + GS  AR + MK + EI + GS  AR + MK + VE  NO + AS + MC + EI  AR + AS + MC + VE  CS + AR + MC + AS  AR + CS + MC + MK  NO + AS + MC + VE  VE + MK + MC + GS	6 30 48 36 24 24 24 24 24 24	16.118* 61.126* 85.668 77.358* 105.695* 46.598 67.394* 47.832 54.103* 68.413	.013 .001 .001 .000 .000 .004 .000 .003
EEUGEECHNIK ME	NAVY  AR + MK + EI + GS  AR + GS + 2MK  NO + CS + VE  VE + AR  VE + MC + AS  MK + AS  VE + AR + NO + CS  VE + MK + GS  VE + AR + MC  AR + MC + AS  VE + MK + CS	24 30 6 30 18 6 6 12 6 18	48.487* 36.016 3.010 102.940* 51.008* 13.519* 3.815 20.890 18.101* 47.849* 38.865*	.002 .208 .808 .000 .000 .036 .702 .052 .006
M A G E	AIR FORCE  MC + GS + 2AS  NO + CS + VE  VE + AR  AR + MK + EI + GS	30 42 60	75.807* 40.596 138.701* 88.960	.000 .533 .000
MM CL GT EL	MARINE CORPS AR + EI + MC + AS VE + MK + CS VE + AR + MC AR + MK + EI + GS	24 30 24 24	90.074* 94.259* 55.064* 38.179	.000 .000 .000 .033

<sup>\*</sup> Chi-Square > 2 x D.F.

Table 16

Standard Deviations of Composites from ASVAB 15/16/17 IOT&E

NAVY  EL AR + MK + EI + GS	Compos	ite	15C	15A	15B	16A	16B	17 <b>A</b>	17B
GT VE + AR 15.92 15.82 15.96 15.88 16.03 15.91 15.88 GM MK + EI + AS + GS 17.07 16.44 16.67 16.40 16.55 16.78 16.66 EL AR + MK + EI + GS 16.80 16.23 16.53 16.30 16.53 16.49 16.64 CL AR + MK + VE 16.10 15.90 16.04 15.86 16.01 15.97 15.84 MM NO + AS + MC + EI 16.49 15.94 16.02 15.92 16.16 16.02 15.90 CS AR + AS + MC + VE 17.10 16.66 16.70 16.68 16.72 16.59 16.49 CC S + AR + MC + AS 16.63 16.17 16.31 16.28 16.33 16.09 16.01 FA AR + CS + MC + MK 16.28 16.18 16.30 16.15 16.22 15.97 15.86 OF NO + AS + MC + VE 15.78 15.21 15.23 15.29 15.38 15.29 15.08 ST VE + MK + MC + GS 16.63 16.32 16.50 16.53 16.57 16.43 16.26 CL NO + CS + VE 18.36 18.25 18.37 18.36 18.48 18.24 13.26 GT VE + AR 14.73 14.64 14.76 14.69 14.83 14.72 14.70 ME VE + MC + AS 22.51 21.72 21.76 21.96 21.83 21.80 21.54 EG MK + AS 22.51 21.72 21.38 21.66 24.77 24.55 24.52 HM VE + MK + GS 21.72 21.38 21.66 21.83 21.93 21.70 21.60 ST VE + MR + GS 22.19 21.38 22.04 21.98 22.10 21.74 21.60 ST VE + AR MC 22.19 21.88 22.04 21.98 22.10 21.74 21.60 ST VE + AR MC 22.19 21.88 22.04 21.98 22.10 21.74 21.60 ST VE + AR MC 22.19 21.88 22.04 21.98 22.10 21.74 21.60 ST VE + AR MC 22.19 21.88 22.04 21.98 22.10 21.74 21.60 ST VE + AR MC 22.19 21.88 22.04 21.98 22.10 21.74 21.60 MR AR + MC + AS 23.55 22.87 23.00 22.82 22.99 22.64 22.55 BC VE + MK + CS 18.90 18.83 18.99 19.00 19.02 18.84 18.75 AR HMK + EI + GS 25.07 24.31 24.70 24.40 24.76 24.67 24.65 24.55 AR + MK + EI + GS 25.07 24.31 24.70 24.40 24.76 24.67 24.65	afqt	2VE + AR + MK	24.05	23.85	24.15	23.79	24.31	24.06	23.85
NAVY  EL AR + MK + EI + GS		ARMY							
NAVY  EL AR + MK + EI + GS	GT .	VE + AR	15.92	15.82	15.96	15.88	16.03	15.91	15.88
NAVY  EL AR + MK + EI + GS	GM.	MOK + BI + AS + GS	17.07	16.44	16.67	16.40	16.55	16.78	16.66
NAVY  EL AR + MK + EI + GS	豇	AR + MK + EI + GS	16.80	16.23	16.53	16.30	16.53	16.49	16.44
NAVY  EL AR + MK + EI + GS	Gr.	AR + MK + VE	16.10	15.90	16.04	15.86	16.01	15.97	15.84
NAVY  EL AR + MK + EI + GS	MM CC	NO + AS + MC + ME	17.10	15.54	16.02	15.92	16.10	16.02	15.90
NAVY  EL AR + MK + EI + GS	ac m	CC + AD + MC + AC	16.63	16.00	16 31	16 28	16 23	16.09	16.43
NAVY  EL AR + MK + EI + GS	FA	AR + CS + MC + MK	16.28	16.18	16.30	16.15	16.22	15.97	15.86
NAVY  EL AR + MK + EI + GS	OF	NO + AS + MC + VE	15.78	15.21	15.23	15.29	15.38	15.29	15.08
NAVY  EL AR + MK + EI + GS	ST	VE + MK + MC + GS	16.63	16.32	16.50	16.53	16.57	16.43	16.26
THE VE + MK + GS 21.72 21.38 21.66 21.83 21.93 21.70 21.60 ST VE + AR + MC 22.19 21.88 22.04 21.98 22.10 21.74 21.64 MR AR + MC + AS 23.50 22.87 23.00 22.82 22.99 22.64 22.59 BC VE + MK + CS 18.90 18.83 18.99 19.00 19.02 18.84 18.75  AIR FORCE  M MC + GS + 2AS 27.12 26.36 26.49 26.45 26.48 26.62 26.52 A NO + CS + VE 24.16 24.25 24.34 24.57 24.10 24.28 24.32 G VE + AR 24.59 24.47 24.77 24.34 24.98 24.63 24.55 E AR + MK + EI + GS 25.07 24.31 24.70 24.40 24.76 24.67 24.60		A T A T B C							
THE VE + MK + GS 21.72 21.38 21.66 21.83 21.93 21.70 21.60 ST VE + AR + MC 22.19 21.88 22.04 21.98 22.10 21.74 21.64 MR AR + MC + AS 23.50 22.87 23.00 22.82 22.99 22.64 22.59 BC VE + MK + CS 18.90 18.83 18.99 19.00 19.02 18.84 18.75  AIR FORCE  M MC + GS + 2AS 27.12 26.36 26.49 26.45 26.48 26.62 26.52 A NO + CS + VE 24.16 24.25 24.34 24.57 24.10 24.28 24.32 G VE + AR 24.59 24.47 24.77 24.34 24.98 24.63 24.55 E AR + MK + EI + GS 25.07 24.31 24.70 24.40 24.76 24.67 24.60	EL.	AR + MK + EI + GS	29.72	28.71	29.23	28.82	29.24		
THE VE + MK + GS 21.72 21.38 21.66 21.83 21.93 21.70 21.60 ST VE + AR + MC 22.19 21.88 22.04 21.98 22.10 21.74 21.64 MR AR + MC + AS 23.50 22.87 23.00 22.82 22.99 22.64 22.59 BC VE + MK + CS 18.90 18.83 18.99 19.00 19.02 18.84 18.75  AIR FORCE  M MC + GS + 2AS 27.12 26.36 26.49 26.45 26.48 26.62 26.52 A NO + CS + VE 24.16 24.25 24.34 24.57 24.10 24.28 24.32 G VE + AR 24.59 24.47 24.77 24.34 24.98 24.63 24.55 E AR + MK + EI + GS 25.07 24.31 24.70 24.40 24.76 24.67 24.60	E	AR + GS + 2MR	30.99	30.54	30.88	30.70	30.98		
THE VE + MK + GS 21.72 21.38 21.66 21.83 21.93 21.70 21.60 ST VE + AR + MC 22.19 21.88 22.04 21.98 22.10 21.74 21.64 MR AR + MC + AS 23.50 22.87 23.00 22.82 22.99 22.64 22.59 BC VE + MK + CS 18.90 18.83 18.99 19.00 19.02 18.84 18.75  AIR FORCE  M MC + GS + 2AS 27.12 26.36 26.49 26.45 26.48 26.62 26.52 A NO + CS + VE 24.16 24.25 24.34 24.57 24.10 24.28 24.32 G VE + AR 24.59 24.47 24.77 24.34 24.98 24.63 24.55 E AR + MK + EI + GS 25.07 24.31 24.70 24.40 24.76 24.67 24.60	CT.	NO + CS + VB	10.30	10.23	14.76	14 60	14 07		
THE VE + MK + GS 21.72 21.38 21.66 21.83 21.93 21.70 21.60 ST VE + AR + MC 22.19 21.88 22.04 21.98 22.10 21.74 21.64 MR AR + MC + AS 23.50 22.87 23.00 22.82 22.99 22.64 22.59 BC VE + MK + CS 18.90 18.83 18.99 19.00 19.02 18.84 18.75  AIR FORCE  M MC + GS + 2AS 27.12 26.36 26.49 26.45 26.48 26.62 26.52 A NO + CS + VE 24.16 24.25 24.34 24.57 24.10 24.28 24.32 G VE + AR 24.59 24.47 24.77 24.34 24.98 24.63 24.55 E AR + MK + EI + GS 25.07 24.31 24.70 24.40 24.76 24.67 24.60	MOR	VE + MC + AS	22.51	21.72	21 76	21 96	21 83		
THE VE + MK + GS 21.72 21.38 21.66 21.83 21.93 21.70 21.60 ST VE + AR + MC 22.19 21.88 22.04 21.98 22.10 21.74 21.64 MR AR + MC + AS 23.50 22.87 23.00 22.82 22.99 22.64 22.59 BC VE + MK + CS 18.90 18.83 18.99 19.00 19.02 18.84 18.75  AIR FORCE  M MC + GS + 2AS 27.12 26.36 26.49 26.45 26.48 26.62 26.52 A NO + CS + VE 24.16 24.25 24.34 24.57 24.10 24.28 24.32 G VE + AR 24.59 24.47 24.77 24.34 24.98 24.63 24.55 E AR + MK + EI + GS 25.07 24.31 24.70 24.40 24.76 24.67 24.60	BG	MK + AS	14.44	14.08	14.17	13.86	13.91		
AIR FORCE  M MC + GS + 2AS 27.12 26.36 26.49 26.45 26.48 26.62 26.52  A NO + CS + VE 24.16 24.25 24.34 24.57 24.10 24.28 24.32  G VE + AR 24.59 24.47 24.77 24.34 24.98 24.63 24.55  E AR + MK + EI + GS 25.07 24.31 24.70 24.40 24.76 24.67 24.60	ĊĪ	VE + AR + NO + CS	24.59	24.52	24.60	24.56	24.77	24.55	24.52
AIR FORCE  M MC + GS + 2AS 27.12 26.36 26.49 26.45 26.48 26.62 26.52  A NO + CS + VE 24.16 24.25 24.34 24.57 24.10 24.28 24.32  G VE + AR 24.59 24.47 24.77 24.34 24.98 24.63 24.55  E AR + MK + EI + GS 25.07 24.31 24.70 24.40 24.76 24.67 24.60		VE + MEK + GS	21.72	21.38	21.66	21.83	21.93	21.70	21.60
AIR FORCE  M MC + GS + 2AS 27.12 26.36 26.49 26.45 26.48 26.62 26.52  A NO + CS + VE 24.16 24.25 24.34 24.57 24.10 24.28 24.32  G VE + AR 24.59 24.47 24.77 24.34 24.98 24.63 24.55  E AR + MK + EI + GS 25.07 24.31 24.70 24.40 24.76 24.67 24.60		VE + AR + MC	22.19	21.88	22.04	21.98	22.10	21.74	21.64
AIR FORCE  M MC + GS + 2AS 27.12 26.36 26.49 26.45 26.48 26.62 26.52  A NO + CS + VE 24.16 24.25 24.34 24.57 24.10 24.28 24.32  G VE + AR 24.59 24.47 24.77 24.34 24.98 24.63 24.55  E AR + MK + EI + GS 25.07 24.31 24.70 24.40 24.76 24.67 24.60		AR + MC + AS	23.50	22.87	23.00	22.82	22.99	22.64	22.59
MADINE CODDS		VE + MR + CS	18.90	18.83	18.99	19.00	19.02	18.84	18.75
MADINE CODDS	M	AIR FORCE	27 12	26 26	26.40	26 45	26 49	26 62	26 52
MADINE CODDS	r. D	NO + CS + VR	24 16	24 25	24 34	20.42	24 10	24 22	20.32
MADINE CODDS	Ĝ	VE + AR	24.59	24.47	24.77	24.34	24.98	24.63	24.55
MADINE CODDS	Ē	AR + MK + EI + GS	25.07	24.31	24.70	24.40	24.76	24.67	24.60
MM AR + EI + MC + AS 17.63 17.08 17.27 17.11 17.29 17.11 17.09 CL VE + MK + CS 14.78 14.73 14.85 14.86 14.88 14.73 14.67 GT VE + AR + MC 16.78 16.54 16.66 16.62 16.71 16.44 16.36		MADINE CODE							
CL VE + MK + CS 14.78 14.73 14.85 14.86 14.88 14.73 14.67 GT VE + AR + MC 16.78 16.54 16.66 16.62 16.71 16.44 16.36	MM	AR + EI + MC + AS	17.63	17.08	17.27	17.11	17.29	17.11	17.09
GT VE + AR + MC 16.78 16.54 16.66 16.62 16.71 16.44 16.36	<u>αr</u>	VE + MK + CS	14.78	14.73	14.85	14.86	14.88	14.73	14.67
	GT EL	VE + AR + MC	16.78	16.54	16.66	16.62	16.71	16.44	16.36

Table 17

Standard Deviations of Composites from ASVAB 18/19 IOT&E

Compos	<u>ite</u>	<u>15C</u>	<u> 18A</u>	<u> 18B</u>	19A	19B
AFQT	2VE + AR + MK	23.94	24.32	24.03	24.35	23.95
	ARMY					
GT	VE + AR	15.77	15.79	15.72	15.85	15.70
GM .	MK + BI + AS + GS	16.67	16.30	16.13	16.15	16.15
EL	AR + MK + BI + GS	16.53	16.58	16.46	16.32	16.28
Œ	AR + MK + VE	15.97	16.15	16.03	16.13	15.93
MM	NO + AS + MC + BI	16.67	16.13	16.06	16.05	16.16
SC	AR + AS + MC + VE	16.81	16.28	16.26	16.42	16.46
$\infty$	CS + AR + MC + AS	16.87	16.48	16.50	16.66	16.64
FA	AR + CS + MC + MK	16.73	17.07	17.06	17.23	17.01
OF .	NO + AS + MC + VE	16.05	15.61	15.59	15.65	15.69
ST	VE + MK + MC + GS	16.37	16.70	16.57	16.73	16.59
_	NAVY					
<u>et</u> .	AR + MK + EI + GS	29.24	29.34	29.12	28.87	28.79
E	AR + GS + 2MK	30.84	31.54	31.34	31.31	31.02
<u>a</u>	NO + CS + VE	19.30	19.32	19.54	19.41	19.17
GT ME	VE + AR VE + MC + AS	14.59 22.08	14.62 21.31	14.54 21.29	14.67	14.52
EG EG	MK + AS	14.09	13.84	13.74	21.40 13.83	21.48 13.85
ČT .	VE + AR + NO + CS	25.91	26.14	26.25	26.20	25.81
HM	VE + MK + GS	21.34	21.95	21.73	21.77	21.58
ST	VE + AR + MC	21.96	22.04	21.98	22.27	22.12
MR	AR + MC + AS	23.14	22.22	22.30	22.43	22.58
BC	VE + MK + CS	19.40	19.61	19.66	19.58	19.33
	AIR FORCE					
M	MC + GS + 2AS	26.16	24.86	24.83	24.80	24.89
A	NO + CS + VE	24.99	25.09	25.25	25.14	25.07
G	VE + AR	24.82	24.93	24.78	25.00	24.79
E	AR + MK + EI + GS	24.56	24.65	24.42	24.29	24.22
	MARINE CORPS	_				
MM	AR + EI + MC + AS	17.30	16.64	16.59	16.68	16.80
<u>σ</u> τ	VB + MK + CS	15.17	15.33	15.38	15.31	15.11
<u> </u>	VE + AR + MC	16.60	16.67	16.61	16.84	16.72
EL	AR + MK + EI + GS	16.54	16.60	16.47	16.33	16.29

Table 18

#### AFQT Category Distributions for Three Subsets of the Data

All Initial Tests, N = 118,265

<u>Cut Score on Composite</u>
92.00 64.00 49.00 30.00 20.00 15.00 9.00

		Pe	rcentage	e at or	Above 9	Cut Sco	re	
Form 15H	5.14	35.99	57.87	80.97	91.42	94.60	97.83	
	Contras	t with	Referen	ce Form	Percer	itage (F	'orm - 15	H)
15G	-0.95		-0.33	0.01	0.01	0.12	0.11	
20A	-0.23	0.62	-0.21	1.11	0.67	0.24		
20B	0.81	0.69	-0.93	0.16	0.49	0.41	-0.01	
21A 21B	-0.03 0.37	0.19	-0.89 -0.15	1.15	0.82	0.63	0.03	
21B 22A	0.37		-0.13	0.61	0.96 0.42	0.78 0.21	0.21 -0.17	
22B	0.05	0.57	-0.02		0.42	0.21	0.21	
	Editing				ing. N	= 99.25		
						- 55,25	•	
			Out	Score	on Como	ogite		
	92.00	64.00			20.00	15.00	9.00	
		_						
Form		<u>Pe</u>	rcentage	e at or	Above 9	Cut Sco	æ	
15H	5.07	35.95	57.62	80.91	91.39	94.53	97.76	
		t with	Referen	ce Form	Percen		orm - 15	H)
15G	-0.96	1.09	-0.36	-0.10	-0.08	0.16		
20A	-0.16	0.58	-0.20 -0.86	0.95	0.54 0.58	0.14	-0.16	
20B 21A	0.92	-0.22	-0.86	0.10	0.58 0.48			
21B	0.13	-0.22	-0.90 -0.06	0.01	0.81		0.00 0.19	
22A	0.99	0.92	-0.47	0.29	0.15	0.05		
22B	0.17		-0.35		0.46	0.54	0.13	
	gly Bala				976	0.51	0.13	
			Out	Caomo	A	:		
	92.00	64.00			<u>on Comp</u> 20.00		9.00	
	52.55							
Form		<u>Pe</u>	rcentage	e at or	Above 9	Cut Sco	œ	
Form 15H	5.30	37.34	59.55	82.22	92.05	95.14	98.05	
	Contras	t with	Referen	ce Form			orm - 15	H)
15G	-0.79				0.01	-0.14		
20A 20B	-0.46	0.38 0.96	-0.36 -0.73	1.42 0.20	0.93	0.31	0.05	
20B 21A	0.90 -0.01	-0.29	_1 11	A 79	0.52 0.70	0.38 0.54	-0.05 0.04	
21B	0.36	0.29	0.02		0.70	0.54	0.04	
22A	1.03	0.78	-0.82	0.60	0.53	0.11	-0.17	
22B	0.06	0.18	-0.51	0.19	0.94	0.53	0.27	
_							<del>-</del> -	

Table 19

Air Force M Composite Distributions for Three Subsets of the Data

		All I	nitial	Tests,	N = 118	,265	
	89.00	61.00	57.00	51.00	45.00	44.00	
Form		Perc	entage i	at or A	<u>bove Cu</u>	t Score	
15H	9.83	43.91	49.52	56.17	62.51	62.98	
	Contrast	with Re	eference	e Form I	ercenta	ge (For	m - 15H)
15G	-0.16	0.31	-0.52	-0.65	-0.40		
20A	-0.95	1.46	1.23	1.12	1.45	2.04	
20B	-1.00	0.60	-0.01	0.07	0.23	0.76	
21A	-1.58	-0.80	-0.23	-0.13	0.18	0.68	
21B	-2.06	-0.33	0.50	0.95 -0.19	1.48	2.09	
22A	-0.40	0.87	-0.04	-0.19	-0.17	0.91	
22B				-0.47			
AIter	Editing f	or extr	eme und	alancin	g, N =	99,254	
			Cut S	core on	Compos	ite	
	89.00	61.00		51.00			
		Perc	entage i	at or Al	pove Cut	<u>Score</u>	
Form	0.00	43.00	40 55	FC 10	60 50	<i>c</i> 2	
15H	9.83	43.98	49.55	56.17	62.58	63.10	
15G	Contrast	MICU Ke	rerence	rom P	ercenta		n - 15H)
20A	-0.12	0.31	-0.44	-0.54 1.07	-0.33	0.40	
20A 20B	~0.60	1.40	1.4/	1.07	1.47	1.99	
20B 21A	-0.33	0.57	-0.03	0.01	0.17	0.64	
21B	-2 10	-0.44	0.03	1 10	1 63	2 16	
22A	-0.36	0.13	-0.75	1.10 -0.15	-0.14	2.16	
22B	-0.30	0.72	-0.00	-0.86	-0.14	0.54	
	ly Balanc					0.54	
50202	,_,	ca saip	100, 11	- 55,57	· ·		
			Cut S	core on	Compos	<u>ite</u>	
	89.00	61.00	57.00	51.00	45.00	44.00	
		Dome		31			
Form		Perc	entage i	at or Al	pove cui	Score	
15H	10.29	45.57	51.35	58.05	64 52	65 01	
	10.25	13.37	J2.JJ	30.03	04.52	03.01	
	Contra	at with	Refere	nce For	n Derret	ntage (F	form - 15H)
15G	-0.08	0 64	-0 34	-0.63			Oz. (1 1311)
20A	-0.92	0.64 1.49	1.19	1.24			
20B	-0.92	1.02	0.31	0.31	0.38	0.92	
21A	~1.56	-1.05	-0.48	0.31	-0.10	0.42	
21B	-2.28	-0.38	0.27	0.87	1.28	1.76	
22A	-0.86	0.90	-0.01	0.87 0.02	-0.10	0.84	
22B	~0.04		-0.82			0.39	
		- · - <del>-</del>	<del>-</del>		- · - <del>-</del>		

# Army GM Composite Distributions for Three Subsets of the Data

All Initial	Tests,	N =	118	, 265
-------------	--------	-----	-----	-------

Form	<u>Cut Score on Composite</u> 105.00 100.00 95.00 90.00 85.00
FOLIII	Percentage at or Above Cut Score
15H	46.79 58.70 68.32 78.28 85.86
	Contrast with Reference Form Percentage (Form - 15H)
15G	-1.14 -1.45 -1.05 0.26 0.81
20A	0.52 0.75 1.17 0.88 0.81
20B	0.52  0.75  1.17  0.88  0.81  0.29  -0.07  -0.12  0.19  -0.08
21A	-0.86 -0.55 0.59 1.18 1.07
21B	-0.12 0.30 1.42 1.82 1.83
22A	-0.05 -0.68 0.12 -0.00 0.33
22B	0.00 -0.16 0.62 0.79 0.64
After	Editing for Extreme Unbalancing, N = 99,254
	<u>Cut Score on Composite</u> 105.00 100.00 95.00 90.00 85.00
	203.00 200.00 33.00 30.00 03.00
Form	Percentage at or Above Cut Score
15H	46.48 58.49 68.11 78.28 85.96
-	Contrast with Reference Form Percentage (Form - 15H)
15G	-0.92 -1.28 -0.86 0.18 0.67
20A	0.70 0.92 1.14 0.61 0.53 0.38 0.04 -0.11 0.17 -0.16
20B	0.38
21A	-0.63 -0.40 0.72 1.08 0.89
21B	0.11 0.49 1.60 1.78 1.74
22A	0.24 -0.41 0.30 -0.15 0.04
22B	-0.06 -0.41 0.48 0.40 0.29
	Strongly Balanced Samples, N = 59,976
	Cut Score on Composite

105.00 100.00 95.00 90.00 85.00

FOLU							
	Pe	ercenta	ge at o	r <u>Above</u>	Cut Sc	ore	
15H	48.80	60.74	70.47	79.89	86.86		
	Contrast with	Refere	ence For	m Perce	ntage	(Form -	15H)
15G	-1.31	-1.90	-1.63	-0.05	0.88		
20A	0.33	0.67	1.01	1.08	1.36		
20B	0.63	0.29	-0.09	0.24	0.01		
21A	-1.29	-0.79	-0.06	0.74	0.84		
21B	-0.56	0.16	1.19	1.40	1.82		
22A	-0.32	-1.00	-0.24	-0.05	0.43		
22B	-0.55	-0.85	-0.38	0.45	0.71		

Table 21

ASVAB Form 20A

Conversion of Raw Test Scores to 1980 Standard Score Equivalents

_							_	_							
Raw	<u>cs</u>	AR	MK	PC	NO	CS	Raw	Raw	<u>CS</u>	AR	MK	PC	NO	<u>cs</u>	Raw
0 1 2 3 4 5 6 7 8 9	20 20 22 24 25 27 29 31 33	25 27 28 29 31 32 33 34 35	20 20 20 21 22 24 25 26 28 29	20 21 24 27 30 33 36 39 42	20 20 20 20 20 20 21 22 22 23	22 22 23 23 24 24 25 25 26 26	01234567890	45 46 47 48 49 50 51 52 53					61 61 62 62 62	50 51 51 52 53 53 54 55 55	45 46 47 48 49 50 51 52 53
10 11	37 39	37 38	31 32	47 50	24 25	27 27	10 11	55 56						56 57	55 56
12 13	41 43	40 41	33 34	52 55	26 27	28 28	12 13	56 57 58						58 58	57 58
14 15	45 47	42 44	35 37	58 61	28 29	29 30	14 15	59 60						59 60	59 60
16 17	49 50	45 47	38 39		30 32	30 31	16 17	59 60 61 62						60 61	61 62
18 19	52 54	48 50	40 41		33 34	32 32	18 19	1 63						62 62	63 64
20 21	56 58	51 53	43 44		36 37	33 34	20 21	64 65 66 67						63 63	65 66
22	60	54	45		38	35	22	67						64	67
23 24	62 64	56 57	46 47		39 40	35 36	23 24	68 69						65 65	68 69
25 26	67	59 60	49 50		42 43	37 38	25 26	70 71						66 66	70 71
27 28		62 63	51 52		44 45	39 39	27 28	72 73						67 67	72 73
29 30		65 66	54 55		46 47	40 41	29 30	74						68 69	7 <u>4</u> 75
31 32			56 58		48 50	41 42	31 32	76 77						69 70	75 77
33 34			59 60		51 52	43 43	33 34	78 79						70 71	78 79
35 36			61		53 54	44 45	35 36	80 81						71 71	80 81
37 38					55 56	45 46	37 38	82 83						72 72	82 83
39 40					57 58	47 47	39 40	84 85						72	84 85
41 42					59	48	41	86 87							86
43					59 60	48 49	42 43	88							87 88
44					60	50	44	89							89

Table 21 (continued)

## ASVAB Form 20A Conversion of Raw Test Scores to 1980 Standard Score Equivalents

 							_								-
Raw	AS	MK	MC	EI	<u>VE</u>	Raw		Raw	AS	MK	MC	EI	<u>Ve</u>	Raw	
0	24	29	24	22	20	0 1	$\mathbf{H}$	25	69	67	70		39	25	
1	26	30	25	25	20	1	Ш	26					40	26	
2	27	32	27	27	20	2	Ш	27					41	27	
3 4	29	33	29	29	20	3	П	28					42	28	
4	31	35	31	31	20	4	Ш	29					43	29	
5	33	37	33	34	20	5 6	П	30					44	30	
6	35	38	35	36	21	6	11	31					45	31	
7	36	40	36	38	23	7	П	32					46	32	
8	38	41	38	41	24	8	11	33					46	33	
9	40	43	40	43	25	9	ш	34					47	34	
10	42	45	41	46	26	10	Ш	35					48	35	
11	43	46	43	48	27	11	Ш	36					49	36	
12	45	48	45	51	28	12	11	37					50	37	
13	47	50	47	53	29	13	11	38					51	38	
14	49	51	49	55	30	14	П	39					52	39	
15	51	53	51	57	31	15	Ш	40					52	40	
16	53	54	53	59	32	16	Ш	41					53	41	
17	55	55	55	61	33	17	П	42					54	42	
18	57	57	57	64	33	18	ш	43					55	43	
19	59	58	59	66	34	19	Ш	44					56	44	
20	61	60	61	69	35	20	Ш	45					57	45	
21	63	61	63		36	21	ш	46					58	46	
22	64	63	64		37	22	Н	47					59	47	
23	66	64	66		38	23	П	48					60	48	
24	68	65	68		39	24	П	49					61	49	
							П	50					62	50	

Table 22

ASVAB Form 20B

Conversion of Raw Test Scores to 1980 Standar - Score Equivalents

Raw	<u>cs</u>	AR	MK	PC	NO	cs	Raw	Raw	œ	AR	WK	29	MO	œ	Raw
01234567891011214517890122224567890123456789014244444444444444444444444444444444444	20 222 224 225 227 233 335 337 443 555 566 667	268 2291 3333 3333 444 445 555 555 556 666 666	200 220 222 222 233 333 333 344 444 445 555 555 555 555 661	20 22 22 28 33 36 40 47 55 56 61	200220 200220 222222222222222222222222	22233442556677888990122233344412334444444444444444444444444	0 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 22 24 25 26 27 28 29 30 31 31 31 31 31 31 31 31 31 31 31 31 31	45 467 489 551 552 553 5567 559 662 667 667 777 777 777 777 777 881 888 888 888 88					61 61 62 62 62 62	5011255555555555555555666666666666666666	4567890123456789012345677777778818888888888888888888888888888

Table 22 (continued)

#### ASVAB Form 20B Conversion of Raw Test Scores to 1980 Standard Score Equivalents

Raw	AS	MK	MC	EI	ΥE	Raw		Raw	24	MK	MC	RI	<b>YE</b>	Raw
0	24	29	24	22	20	0	-11	25	69	68	70		40	25
1	26	31	25	25	20	1	H	26					41	26
2	27	32	27	27	20	2	- !	27					42	27
1 2 3 4	29	34	29	29	20	3	- 11	28					43	28
	31	35	31	31	20	4	- 11	29					44	29
5 6 7	33	37	33	34	20	5	- 11	30					45 46 46	30
6	35	39	35	36	21	6	- 11	31					46	31
7	36	40	36	38	22	7	- 11	32					46	32
8 9 10	38	42	38	41	23	1 2 3 4 5 6 7 8 9	- 11	33					47	33
. 9	40	43	40	43	24	. 9	- 11	34 35					48 49	34
10	42	45 47	41	46	25	10	Ш	35					49	34 35 36
11	43	47	43	48	26	11	- [ [	36 37					50	36
12 13 14	45	48	45	51	27	12	H	37					51	37
13	47	50	47	53	28	13	Н	38 39 40					51	38 39
14	49	52	49	55	29	14	- 11	39					52	39
15	51	53	51	57	30	15		40					53	40
16 17	53	55	53	59	31	16	- 11	41					54	41
1/	55	56	55	61	32	17	Ш	42					54 55	42 43
18	57	58 59	57	64 66	33	18 19	-11	43 44					56	44
19	59 61	61	59 61	69	34	20	- 11	45					57	45
20 21	63	62	63	69	35 36	21	-11	46					58	46
22	64	63	64		37	22	-11	47					59	47
23	66	65	66		38	23	Ш	48					60	48
24 24	68	66	68		39	24		49					61	49
4.4	66	90	96		39	24	IJ	50					62	50
							11	30					02	50

Table 23

ASVAB Form 21A

Conversion of Raw Test Scores to 1980 Standard Score Equivalents

								~							
Raw	22	AR	WK	<b>PC</b>	MO	<u>cs</u>	Raw	Raw	<u>cs</u>	AR	WK	PC	NO	<u>CS</u>	Raw
0	20	25	20	20	20	21	0	45					61	50	45
1	20	27	20	20	20	22	1	46					61	50	46
2 3	22	28 30	20 20	22	20 20	22 23	2	47					61 62	51 51	47 48
4	25 27	31	22	25 27	20	23	4	49					62	52	49
5	29	32	23	29	20	24	2 3 4 5 6	[ 50					62	53	50
5 6	30	34	24	32	21	24	6	51						53	51
7	32	35	26	35	22	25	7	52						54	52
8 9	34 35	36 37	27 29	38 <b>4</b> 2	23 24	25 26	8 9	53 54						55 55	53 54
10	37	39	30	45	25	26	10	55						56	55
11	38	40	31	49	26	27	11	56						56	55 56
12	40	41	33	52	27	27	12	57						57	57
13 14	42	43	34 36	55	28	28	13 14	58   59						58 58	58
15	43 45	44 45	37	58 61	29 30	28 29	15	60						59	59 60
16	47	46	39	-	31	30	16	61						60	61
17	49	48	40		32	30	17	62						60	61 62
18	52	49	41		34	31	18	63						61	63
19 20	54 56	50 52	42 43		35 36	32 33	19 20	64						61 62	64 65
21	58	53	45		38	33	21	66						63	66
22	60	54	46		39	34	22	67						63	67
23	62	56	47		40	35	23	68						64	68
24 25	65 67	57 58	48 49		41 42	36 37	24	69						64 65	69 70
25 26	6/	60	50		43	37	25 26	1 71						66	70 71
27		61	51		45	38	27	72						66	71 72
28		63	52		46	39	28	73						67	73
29		64	54		47	40	29	74						67	74
30 31		66	55 56		48 49	40 41	30 31	75   76						68 68	75 76 77
32			57		50	42	32	17						69	77
33			59		51	42	33	11 78						69	78
34			60		52	43	34	79						70	79
35 36			61		53 54	44	35 36	80						70 71	80 81
37					55	45	37	82						71	82
38					56	46	38	83						72	83
39					57	46	39	84						72	84
40 41					58 59	47 47	40	85 86							85 86
42					59	48	41 42	87							86 87
43					60	48	43	88							88
44					60	49	44	89							88 89

Table 23 (continued)

#### ASVAB Form 21A Conversion of Raw Test Scores to 1980 Standard Score Equivalents

Raw	AS	MK	MC	<u>ei</u>	ΥE	Raw		Raw	AS	MK	WC	EI	<b>VE</b>	Raw
0	24	29	23	22	20	0	П	25	69	67	70		39	25
ì	25	30	25	25	20	1	Ш	25 26					40	26
2	27	32	27	27	20	2	Ш	27					41	27
3	29	33	28	29	20	3	Ш	28					42	28
4	29 30	33 35	30	29 31	20	4	Ш	29					43	29
Š	32	37	28 30 32	34	20	5	- { {	30					44	28 29 30
	33	38	33	36	20	6 7	-11	31					45 45	31 32
6 7	35	40	35	36 39	21	7	ш	32					45	32
8	33 35 37	41	33 35 37	41	22	8	Ш	33					46	33
9	39	43	38	44	23	9	Ш	34					47	34
10	39 <b>4</b> 1	45	40	46	24	10	Ш	35					48	35
11	43	47	42	46 49	25	11	ш	36					49	35 36
12	43 45 47	48	44	51 53 55 57	26	12	Ш	37					50	37
13	47	50	46	53	27	13	ш	38					51 51	38 39
14	49	51	48	55	28	14	ш	39					51	39
15	51	53	50	57	29	15	-11	40					52	40
16	52	53 54	52	59	30	16	Ш	41					53	41
17	54	55	54	62	29 30 31	16 17	П	42					53 54 55 56 57	42
18	56	57	56	64	32	18	-11	43					55	43
19	56 58	58	58	66	33	19	- 11	44					56	44
20	59	60	60	68	34	20	ш	45					57	44
21	61	61	62		35	21	Ш	46					58	46
22	63	63	64		36	22	Ш	47					59	47
23	65	64	65		37	23	Ш	48					60	48
24	67	66	67		38	24	ш	49					61	49
			-				11	50					62	50

Table 24

ASVAB Form 21B

Conversion of Raw Test Scores to 1980 Standard Score Equivalents

																-
Raw	GS	AR	WK	PC	NO	œ	Raw	Raw	œ	AR	MK	PC	NO	CS	Raw	
0	20	25	20	20	20	22	0	45					61	50	45	
1	20 22	27 28	20 20	21 24	20 20	22 23	1	46					61 61	51 51	46 47	
3	25	29 29	20	27	20	23	2 3	48					62	52	48	
4	27	30	21	30	20	24	4	49					62	53	49	
1 2 3 4 5 6 7 8	29	32	23	33	20	24	5	50					62	53	50	
6	30	33	24	35	21	25	6	51						54	51	
7	32 34	34 35	25 27	38	22 23	25	7 8	52 53						54	52	
9	35	36	28	41 44	24	25 26	9	53   54						55 56	53 <b>54</b>	
10	37	38	29	47	25	26	10	55						56	55	
11	38	39	30	50	26	27	11	56						57	56	
12	40	40	32	53	27	27	12	57						58	57	
13 14	42	42	33	56	28	28	13	58   59						58	58	
15	43 45	43 44	35 36	58 61	29 30	29 29	14 15	60						59 60	59 60	
15 16	47	46	38	0.2	31	30	16	61						60	61	
17	49	48	39		32	31	17	62						61	62	
18	52	49	41		34	31	18	63						61	63	
19 20	54 56	51 53	42 44		35 36	32 33	19 20	64						62 63	64 65	
21	58	54	45		38	33	21	66						63	66	
22	60	56	46		39	34	22	67						64	67	
23	62	58	47		40	35	23	68						64	68	
24	65	59	48		41	36	24	69 70						65	69	
25 26	67	60 62	<b>49</b> 50		42 43	36 37	25 26	71						65 66	70 71	
27		63	52		45	38	27	72						67	72	
28		64	53		46	39	28	73						67	73	
29		65	54		47	40	29	74						68	74	
30 31		66	55 56		48 49	40 41	30 31	75 76						68 69	75 76	
32			58		50	42	32	11 77						69	77	
33			59		51	42	33	11 78						70	78	
34			60		52	43	34	79						70	79	
35			61		53	44	35	80						71	80	
36 37					54 55	44 45	36 37	81 82						71 71	81 82	
38					56	46	38	83						72	83	
39					57	46	39	84						72	84	
40					58	47	40	85							85	
41 42					59 59	48 48	41	86							86 87	
43					60	49	42 43	88							88	
44					60	49	44	89							89	
								• •								

(continued)

ASVAB Form 21B

Conversion of Raw Test Scores to 1980 Standard Score Equivalents

Raw	AS	MK	MC	EI	VΕ	Raw	Raw	AS	MK	MC	EI	VE	Raw
0	24	29	23	22	20	0	1 25	69	68	70		40	25
i	25	30	25	22 25 27 29 31 34 36	20	0 1 2 3	25 26					41	26
2	27	32	27	27	20	2	27					42 43 43	27 28 29
3	29	33	28	29	20	3	28					43	28
4	30	35	30	31	20	4	29					43	29
5	32	37	32	34	20		30					44	30
6	33	38	33	36	21	5 6 7	31					45	31
7	35	40	35	39	22	7	32					46	32
8	37	29 30 32 33 35 37 38 40 41	23 25 27 28 30 32 33 35 37	39 <b>4</b> 1	22	8	32 33					44 45 46 47	30 31 32 33
9	39	43	38		23	9	34					48	34
10	24 25 27 29 30 32 33 35 37 39	43 44	38 40 42	46	24	10	34 35					49	34 35
11	43	46	42	49	25	11	36					50	36
11 12	43 45	46	44	44 46 49 51 53 55 57 59 62 64 66	20 20 20 20 21 22 23 24 25 26 27 29 30 31 34 35 37	11 12	36 37					48 49 50 50	36 37
13	47	49	46	53	27	13	38					51	38 39
14	49	51	48	55	28	14	39					52	39
13 14 15 16 17	51	52	46 48 50 52	57	29	13 14 15 16 17	40					53	40 41
16	52	54	52	59	30	16	41					54	41
	54	56	54	62	31	17	42					55	42
18	47 49 51 52 54 56 58 59 61	49 51 52 54 56 57 59 61 62	56 58 60 62	64	32	18 19	43					56	43
19	58	59	58	66	34	19	44					56	44
20	59	61	60	68	35	20 21	45					57	45
21	61	62	62		36	21	46					58	46
22	63	63	64		37	22	47					59	47
18 19 20 21 22 23 24	63 65 67	63 65 66	65		38	23	48					51 52 53 54 55 56 57 58 59 60 61	48
24	67	66	67		39	24	49 50					61	49
							50					62	50

Table 25

ASVAB Form 22A

Conversion of Raw Test Scores to 1980 Standard Score Equivalents

Raw	GS	AR	WK	PC	NO	<u>CS</u>	Raw	Raw	<u>GS</u>	AR	MK	EC	NO	CS	Raw
01234567891011213415678891011222234567889033123345367839401422444444444444444444444444444444444	201 221 223 227 231 334 435 446 485 554 485 554 666 68	257892333366788914455545557891235666666666666666666666666666666666666	200 200 221 222 233 333 333 333 333 333 333 333	20 20 23 25 28 31 34 34 34 46 49 55 46 50	20000001234566789123333333333333344434567890124555555555555555555555555555555555555	222334455667788990122233445566778899012223344445566677889901223344445566678889	01 12 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 22 23 24 25 27 28 30 31 31 32 33 34 35 36 37 38 38 38 38 38 38 38 38 38 38 38 38 38	466 47 48 49 55 55 55 55 55 56 66 66 66 67 77 77 77 77 77 77 77 77 77					60 61 61 61 62 62	450 551 552 553 555 555 557 558 559 660 661 663 664 666 667 768 777 777 777 777 777 777 777	456 478 490 123 456 478 490 123 456 666 677 777 777 777 777 777 777 777 7

Table 25 (continued)

#### ASVAB Form 22A Conversion of Raw Test Scores to 1980 Standard Score Equivalents

Raw	AS	MK	MC	EI	<u>VE</u>	Raw	Raw	AS	MK	MC	EI	VE	Rat
0	24	29	23	22	20	0	25	69	67	70		39	25
1	26	31	25	25	20	1	26					40	2€
2	28	33	27	27	20	2	27					41	27
3	29	35	28	29	20	3	28					42	28
4	31	36	30	32	20	4	29					43	29
5	33	38	32	34	20	5	30					44	30
6	35	39	34	37	20	6	31					45	31
7	37	41	36	39	21	7	32					46	32
8	39	42	38	41	22	8	33					46	33
9	40	43	39	43	23	9	34					47	34
10	42	45	41	46	24	10	35					48	35
11	44	46	43	48	25	11	36					49	36
12	46	48	45	51	26	12	37					50	37
13	47	49	47	53	27	13	38					51	38
14	49	51	49 51	55	28	14	39					52	39
15	51	52	51	58	29	15	40					52	40
16	52	53	53	60	30	16	41					53	43
17	54	55	55	62	31	17	42					54	42
18	56	56	57	64	32	18	43					55	43
19	57	57	59	66	33	19	44					56	44
20	59	59	61	69	34	20	45					57	45
21	61	60	63		35	21	46					58	46
22	63	62	64		36	22	47					59	47
23	65	63	66		37	23	48					60	48
24	67	65	68		38	24	49 50					61	49
						ı	50					62	50

Table 26

ASVAB Form 22B

Conversion of Raw Test Scores to 1980 Standard Score Equivalents

Raw	<u>cs</u>	AR	MK	<b>PC</b>	NO	CS	Raw	Raw	<u>GS</u>	AR	MK	PC	NO	CS.	Raw
0 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 6 17 18 19 20 22 22 24 22 6 27 28 29 30 31 2 33 34 35 6 37 38 9 40 14 2 43 44	201 213 227 227 231 334 435 548 558 668 668	267 278 331 333 335 337 340 443 445 555 555 556 666 666 666	200 220 220 222 223 233 333 333 344 444 445 555 555 556 61	20 214 28 314 347 448 553 558 61	200 220 221 225 226 227 233 335 337 344 445 447 489 555 557 559 50 60 60 60 60 60 60 60 60 60 60 60 60 60	22233442556277288990312233344444444444444444444444444444444	01234567891011231441561781992212232456789333345356788394014234444344	45 467 489 551 555 555 556 667 667 777 777 777 777 777					60 61 61 62 62	49 551 551 552 553 555 555 555 555 567 577 58 566 667 667 77 77 77 77 77 77 77	45 46 47 48 49 50 51 55 56 57 58 66 66 67 77 77 77 80 81 82 83 84 85 88 88 88 88 88 88

(continued)

ASVAB Form 22B

Conversion of Raw Test Scores to 1980 Standard Score Equivalents

Raw	AS	MK	MC	EI	<u>VE</u>	Raw	Raw	AS	MK	MC	EI	YE	Raw
0	24	29	23	22	20	0	25	69	67	70		40	25
0 1	26	31	23 25	25	20	1	26					41	26
2	28	33	27	25 27	20	2	27					42	27
3	29	34	28	29	20	3	28					43	28
4	31	36	30	32	20 20	4	29					44	29
5	33	38	32	34	20	Š	30					45	30
5 6 7	35	38 39	34	29 32 34 37	20 21	6	31					46	31
7	37	41	36	39	21	7	32					46	32
8	28 29 31 33 35 37 39	42	38	41	21 22	8	33					46 47	33
9	40	44	39	43	23	9	34					48	34
10	42	46	41	46	23 24	10	35					49	35
11	44	47	43	48	25 <b>26</b>	11	36					50	36
12	46	49	45	51	26	12	37					50 50	37
13	47 49	50 52	47	53 55	27 29	13	38					51	38
14	49	52	49	55	29	14	39					52	39
15	51	53	51	58	30	15	40					53	40
16	52	54	53	60	31	16	41					54	41
15 16 17	54	56	55	62	30 31 32 34	17	42					54 55 55	42
18	56	57	57	64	34	18	43					55	43
19	56 57	59	59	66	35 36	19	44					56 57 58	44
20	59	60 62	61	69	36	20	45					57	45
20 21	61	62	63		37	21	46					58	46
22	63	63	64		38	22	47					59	47
22 23	65	64	66		39	23	48					60	48
24	67	66	68		40	24	49					61	49
							50					62	50

#### ASVAB 20, 21, AND 22 IOT&E SUPPLEMENT FIGURES 1-35

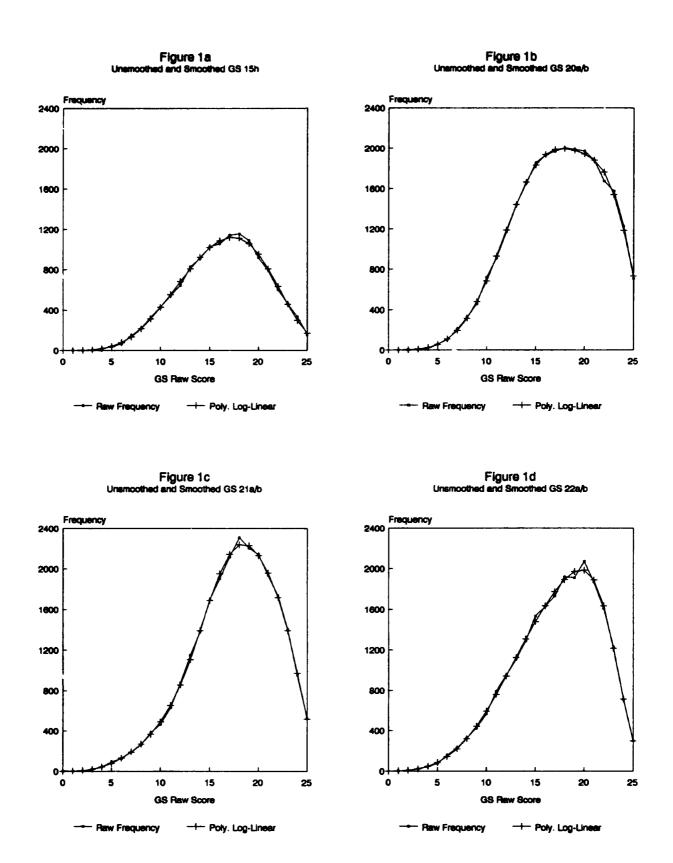


Figure 1. Unsmoothed and Polynomial Log-Linear Smoothed Distributions for Equating GS

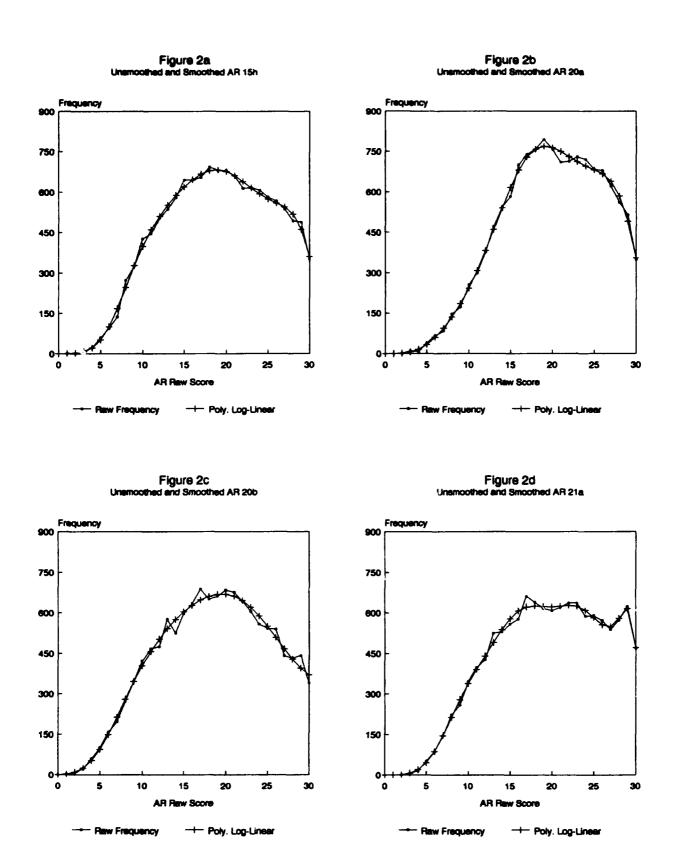


Figure 2. Unsmoothed and Polynomial Log-Linear Smoothed Distributions for Equating AR

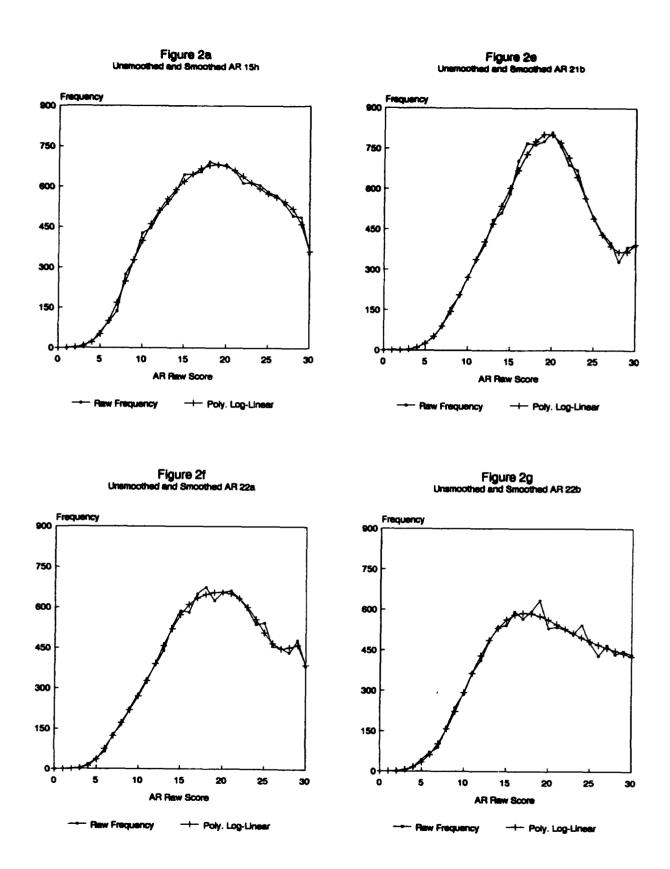


Figure 2, Con't. Unsmoothed and Polynomial Log-Linear Smoothed Distributions for Equating AR

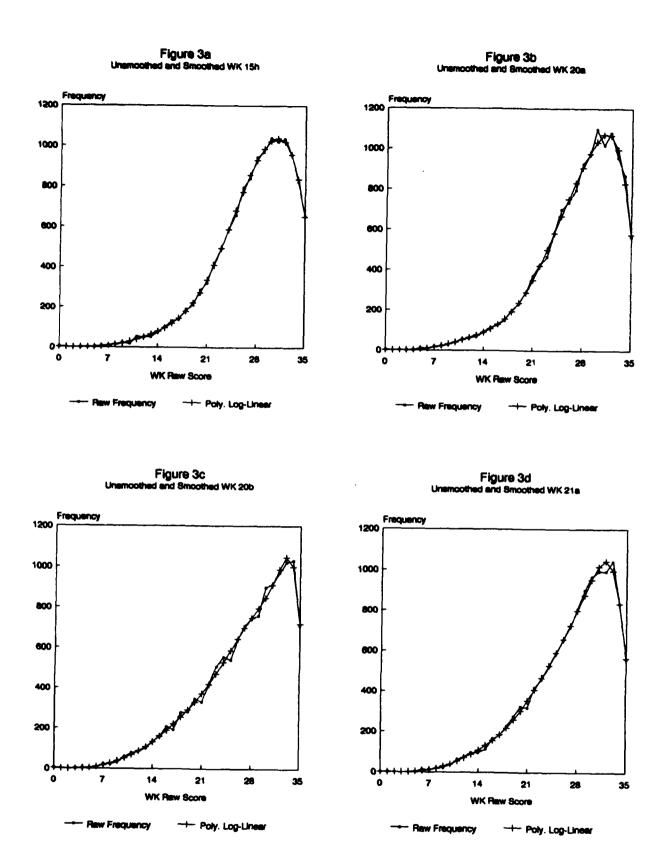


Figure 3. Unsmoothed and Polynomial Log-Linear Smoothed Distributions for Equating WK

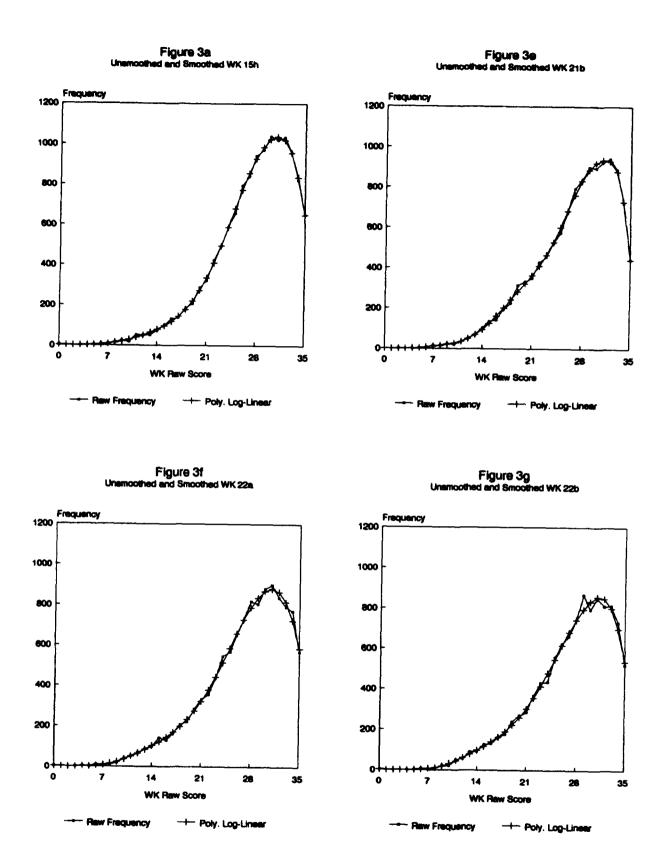


Figure 3, Con't. Unsmoothed and Polynomial Log-Linear Smoothed Distributions for Equating WK

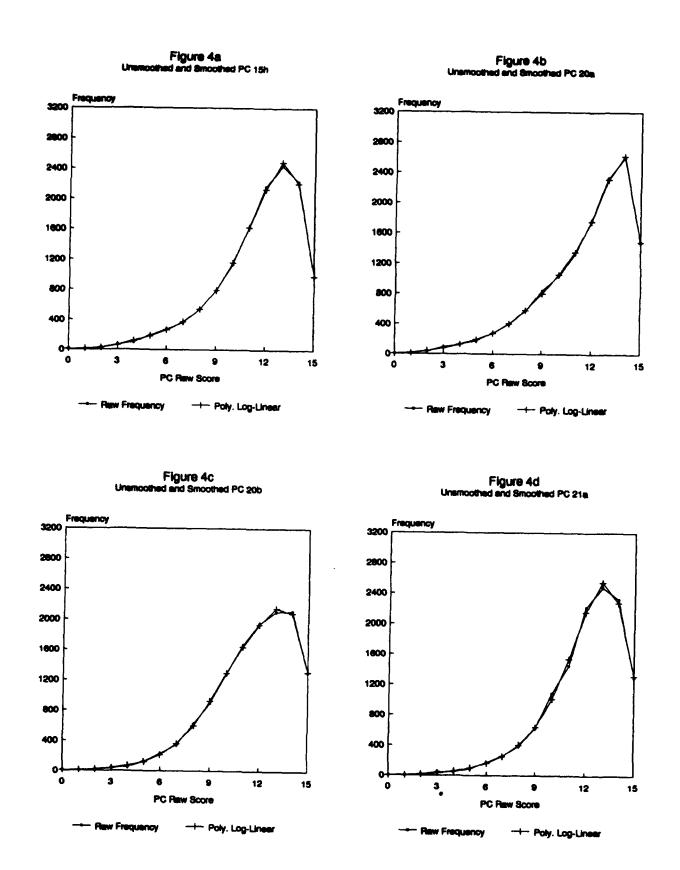


Figure 4. Unsmoothed and Polynomial Log-Linear Smoothed Distributions for Equating PC

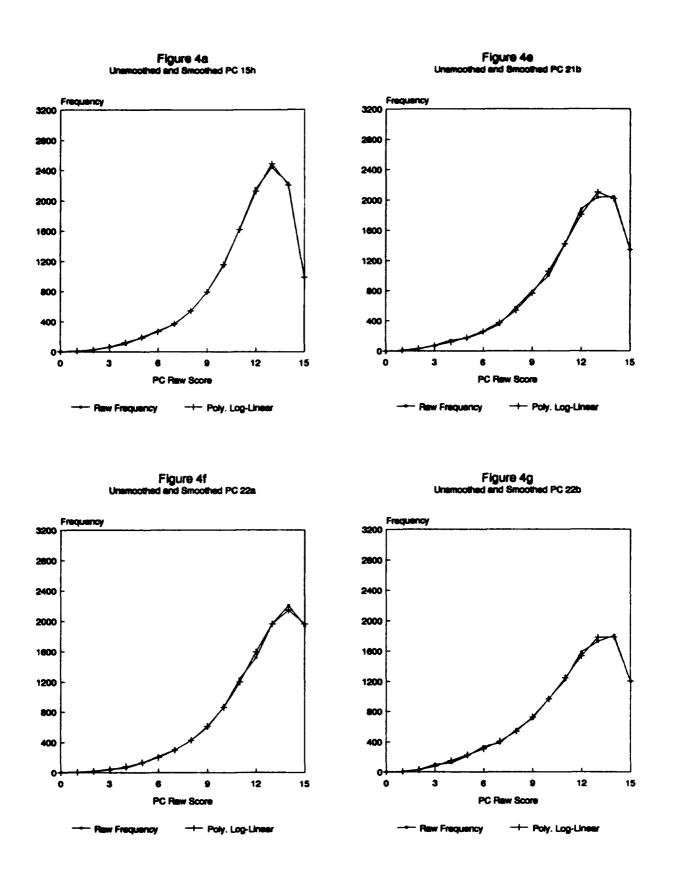


Figure 4, Con't. Unsmoothed and Polynomial Log-Linear Smoothed Distributions for Equating PC

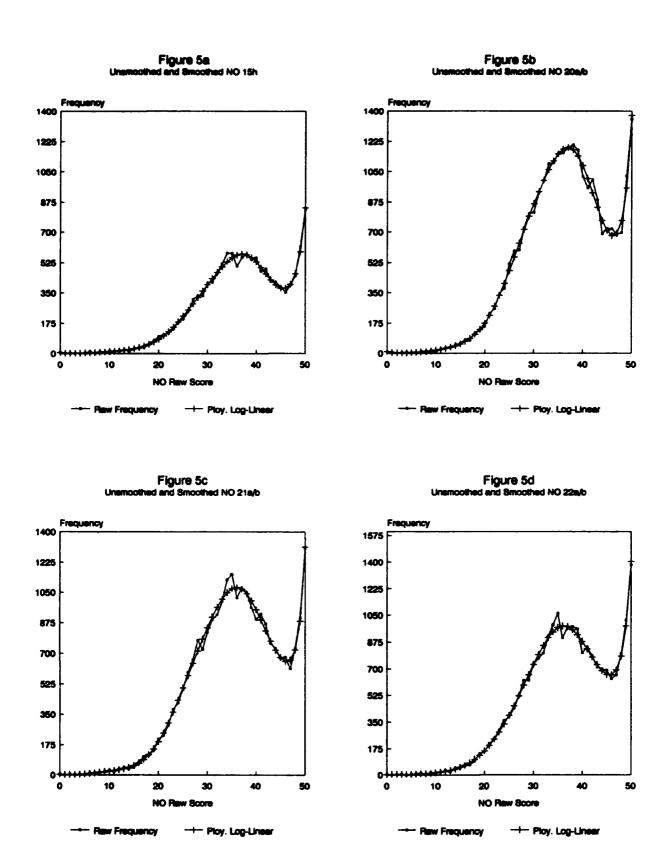


Figure 5. Unsmoothed and Polynomial Log-Linear Smoothed Distributions for Equating NO

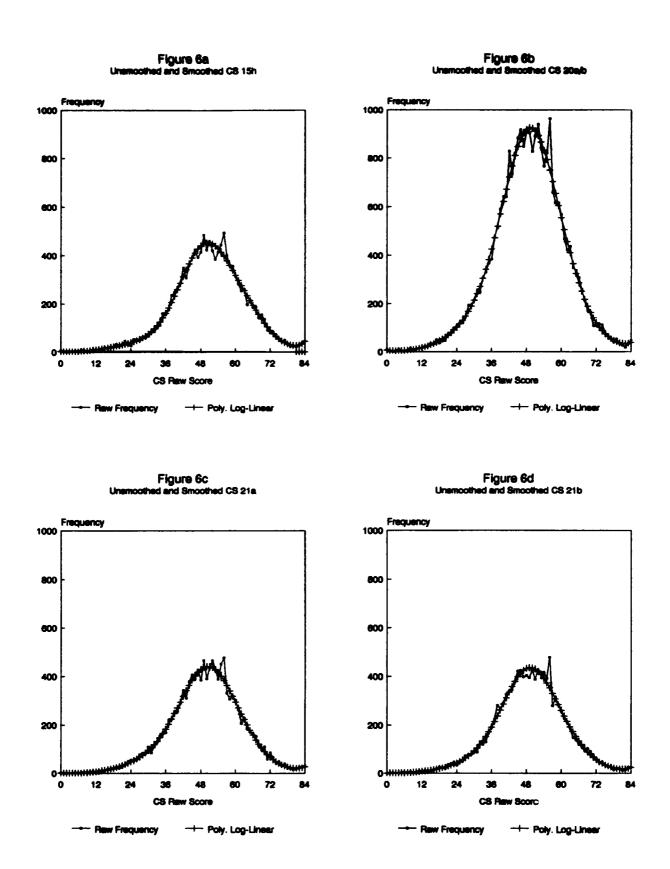


Figure 6. Unsmoothed and Polynomial Log-Linear Smoothed Distributions for Equating CS



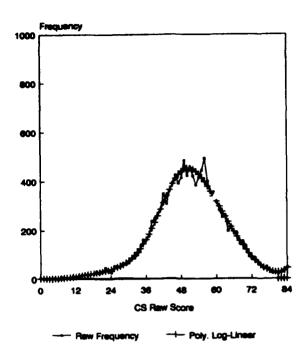


Figure 6e Insmoothed and Smoothed CS 22s/b

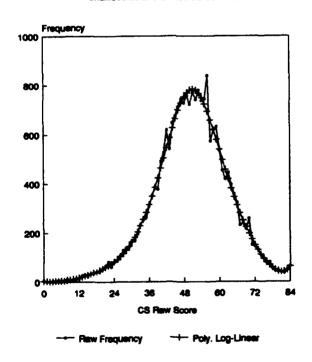


Figure 6, Con't. Unsmoothed and Polynomial Log-Linear Smoothed Distributions for Equating CS

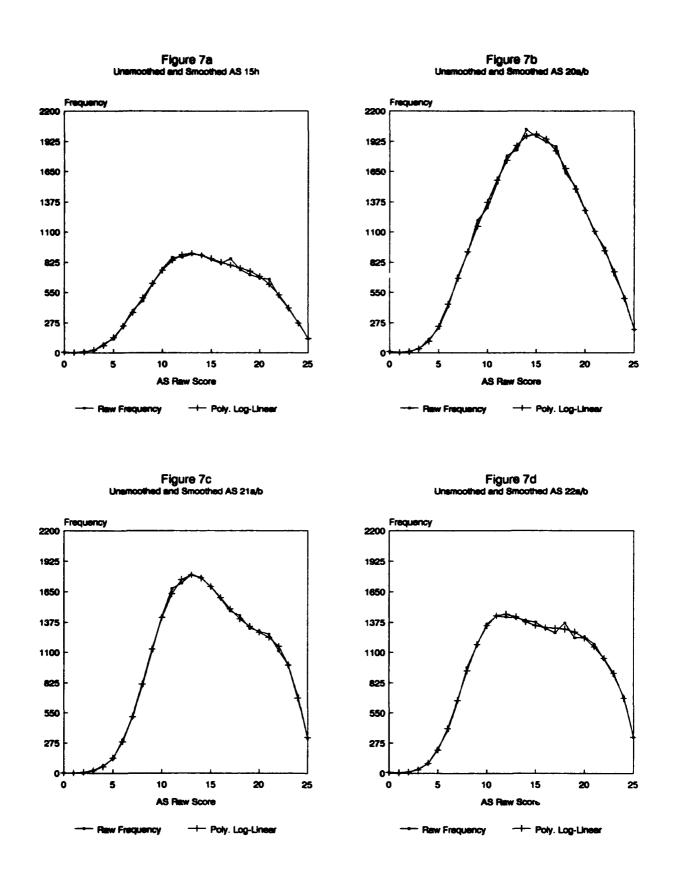


Figure 7. Unsmoothed and Polynomial Log-Linear Smoothed Distributions for Equating AS

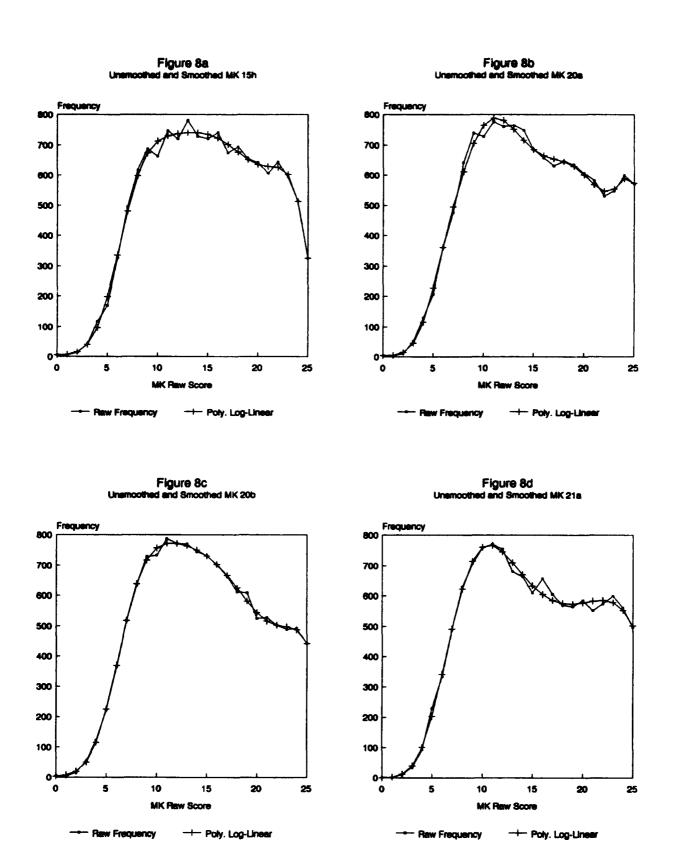


Figure 8. Unsmoothed and Polynomial Log-Linear Smoothed Distributions for Equating MK

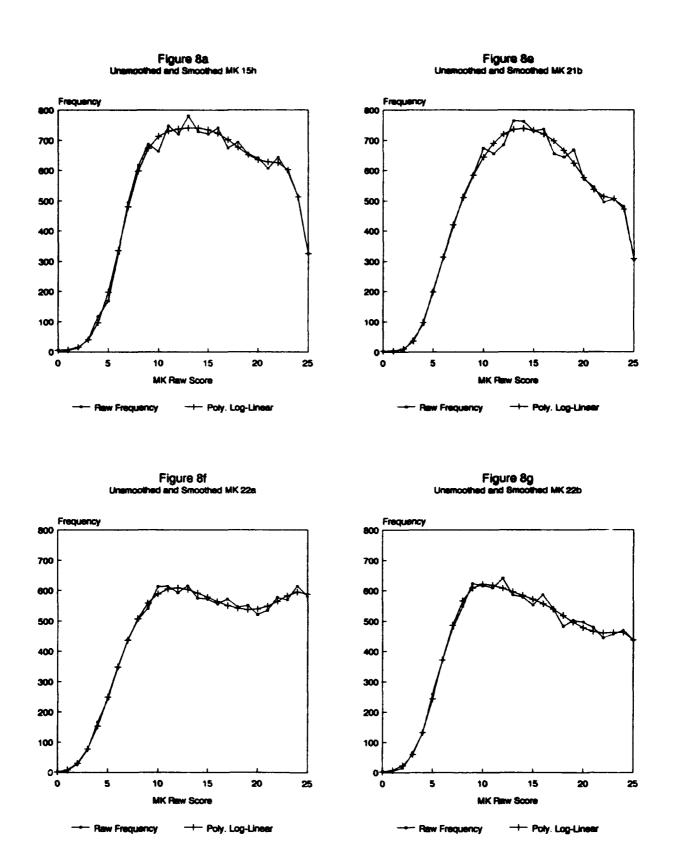


Figure 8, Con't. Unsmoothed and Polynomial Log-Linear Smoothed Distributions for Equating MK

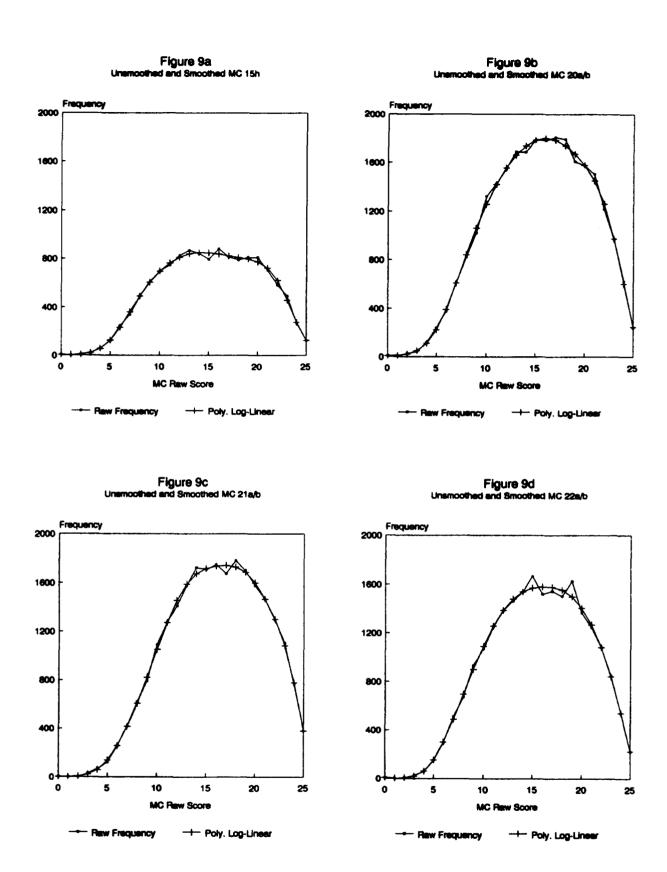


Figure 9. Unsmoothed and Polynomial Log-Linear Smoothed Distributions for Equating MC

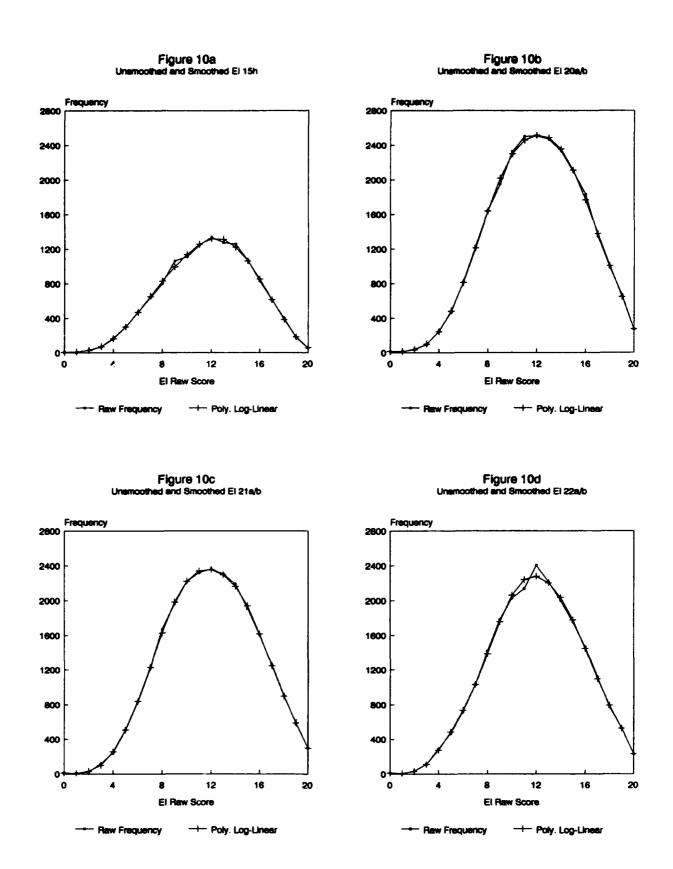


Figure 10. Unsmoothed and Polynomial Log-Linear Smoothed Distributions for Equating EI

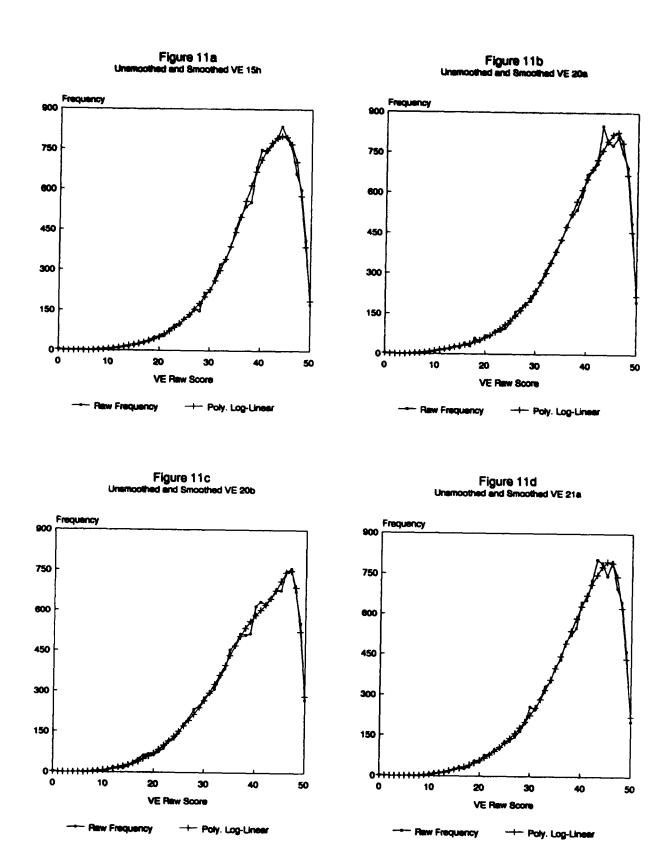


Figure 11. Unsmoothed and Polynomial Log-Linear Smoothed Distributions for Equating VE

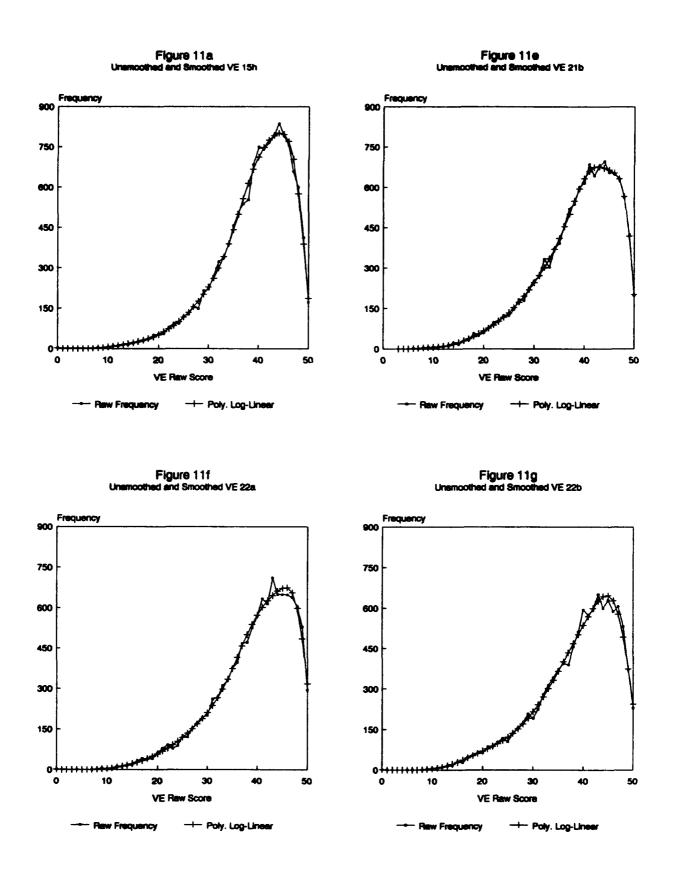
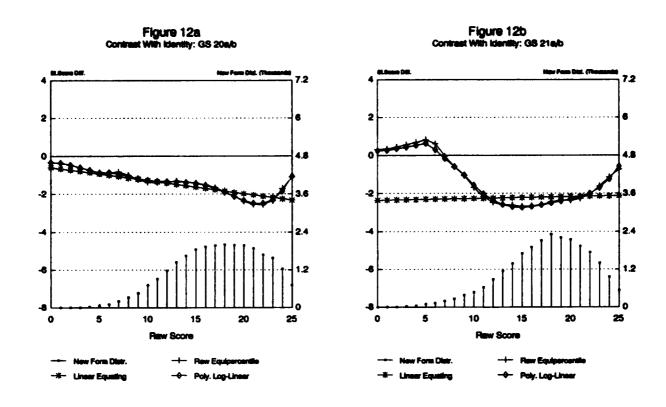


Figure 11, Con't. Unsmoothed and Polynomial Log-Linear Smoothed Distributions for Equating VE



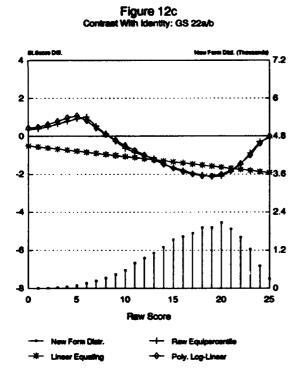
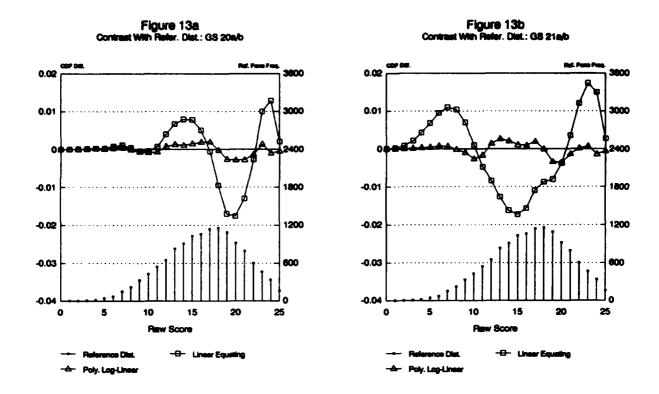


Figure 12 Standard-Score Contrast of Linear-Rescaling, Quartic Log-Linear and Polynomial Log-Linear Equatings With Linear-Identity Equating for GS



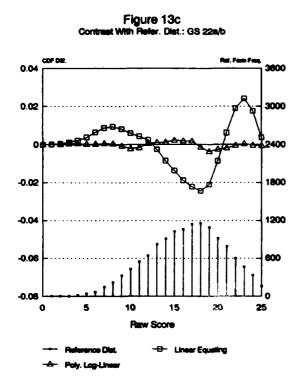


Figure 13. Contrast of Cumulative Distributions of Quartic and Polynomial Log-Linear Equated Scores With Cumulative Distributions of Reference Form for GS

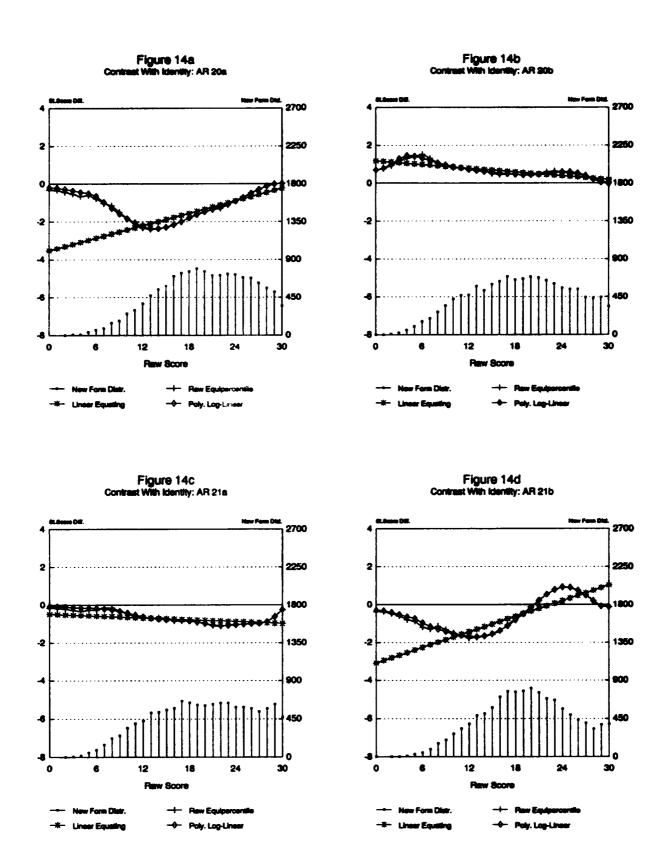


Figure 14. Standard-Score Contrast of Linear-Rescaling, Quartic Log-Linear and Polynomial Log-Linear Equatings With Linear-Identity Equating for AR

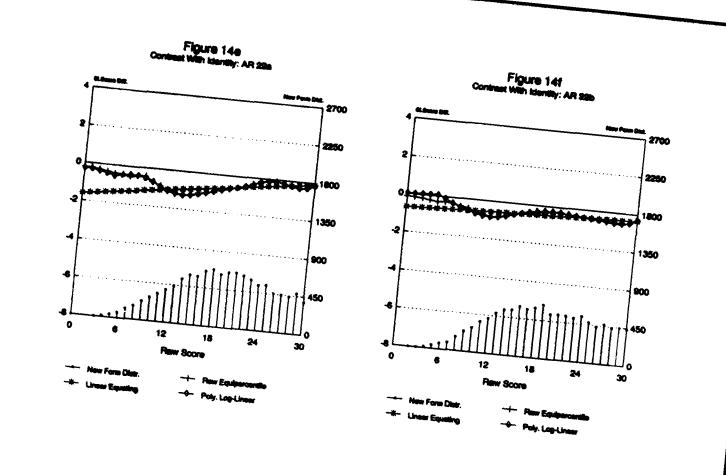


Figure 14, Con't. Standard-Score Contrast of Linear-Rescaling, Quartic Log-Linear and Polynomial Log-Linear Equatings With Linear-Identity Equating for AR

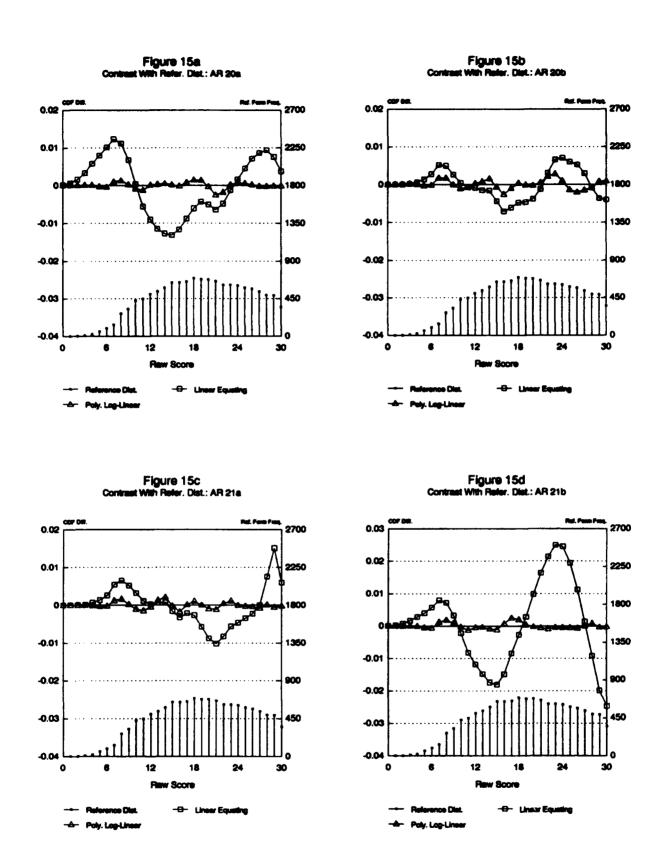


Figure 15. Contrast of Cumulative Distributions of Quartic and Polynomial Log-Linear Equated Scores With Cumulative Distributions of Reference Form for AR

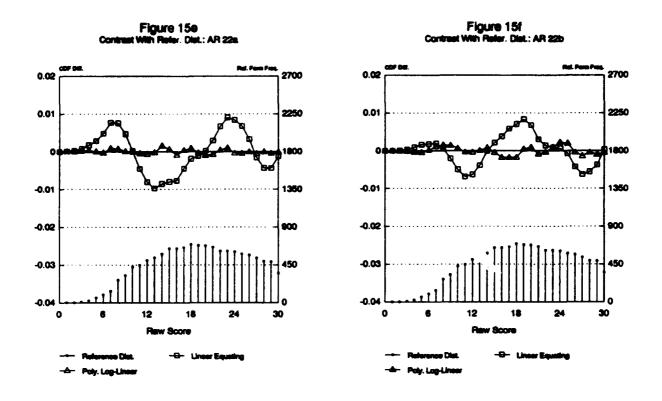


Figure 15, Con't. Contrast of Cumulative Distributions of Quartic and Polynomial Log-Linear Equated Scores With Cumulative Distributions of Reference Form for AR

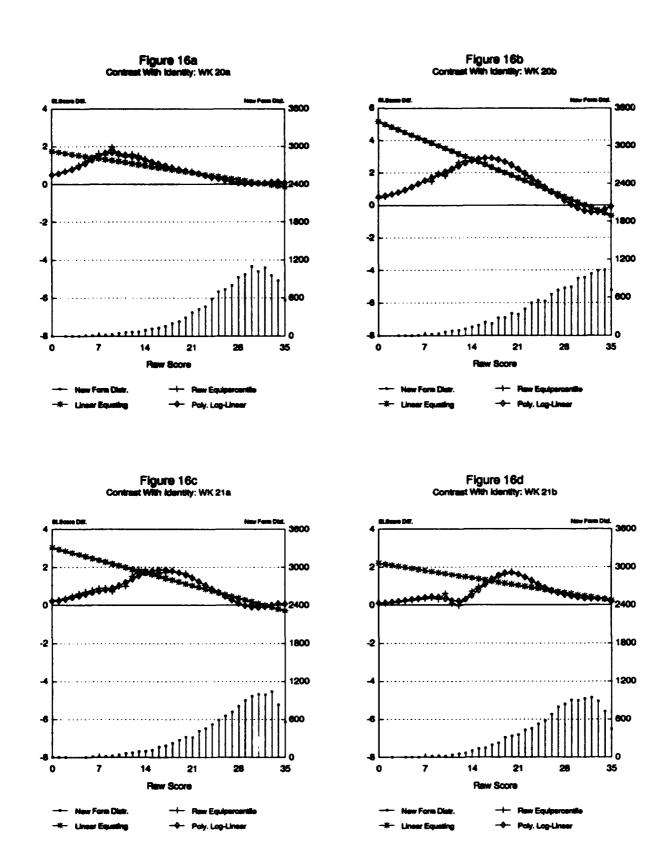


Figure 16. Standard-Score Contrast of Linear-Rescaling, Quartic Log-Linear and Polynomial Log-Linear Equatings With Linear-Identity Equating for WK

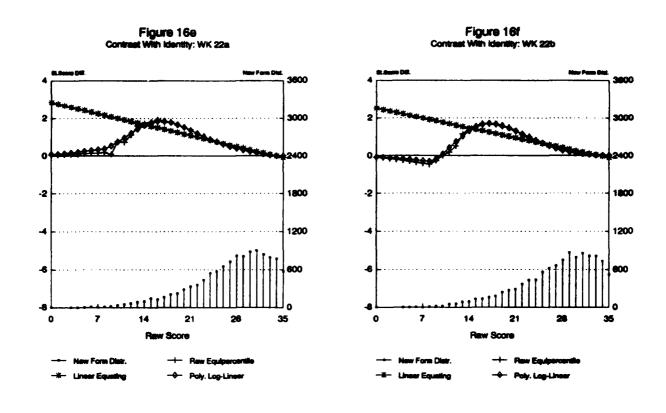


Figure 16, Con't. Standard-Score Contrast of Linear-Rescaling, Quartic Log-Linear and Polynomial Log-Linear Equatings With Linear-Identity Equating for WK

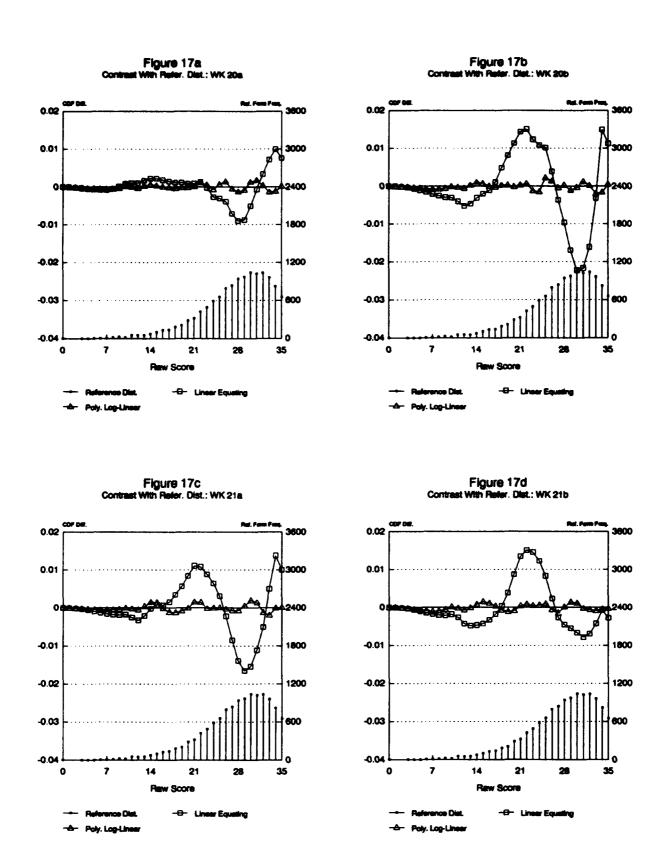


Figure 17. Contrast of Cumulative Distributions of Quartic and Polynomial Log-Linear Equated Scores With Cumulative Distributions of Reference Form for WK

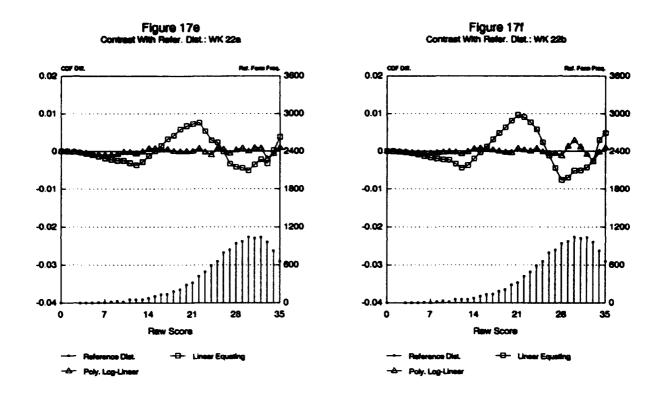


Figure 17, Con't. Contrast of Cumulative Distributions of Quartic and Polynomial Log-Linear Equated Scores With Cumulative Distributions of Reference Form for WK

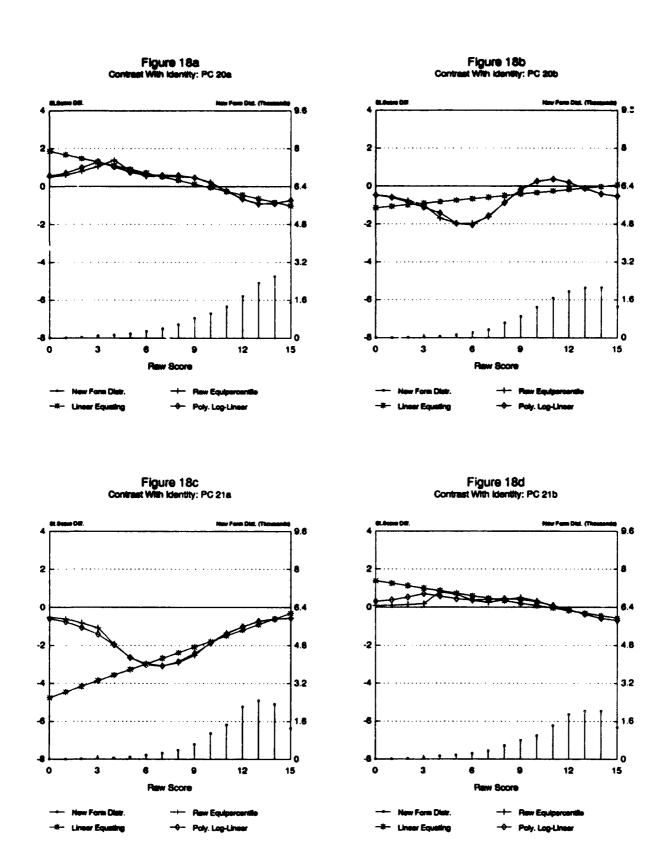


Figure 18. Standard-Score Contrast of Linear-Rescaling, Quartic Log-Linear and Polynomial Log-Linear Equatings With Linear-Identity Equating for PC

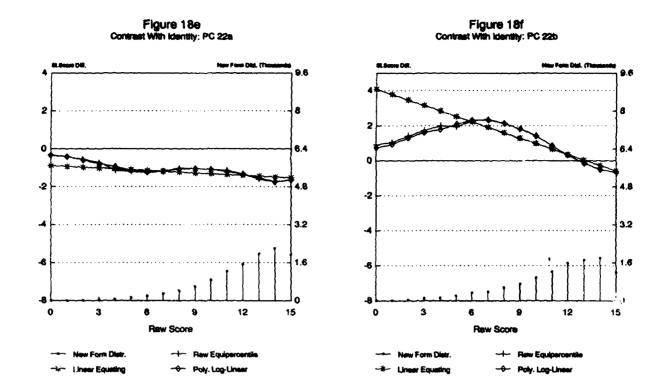


Figure 18, Con't. Standard-Score Contrast of Linear-Rescaling, Quartic Log-Linear and Polynomial Log-Linear Equatings With Linear-Identity Equating for PC

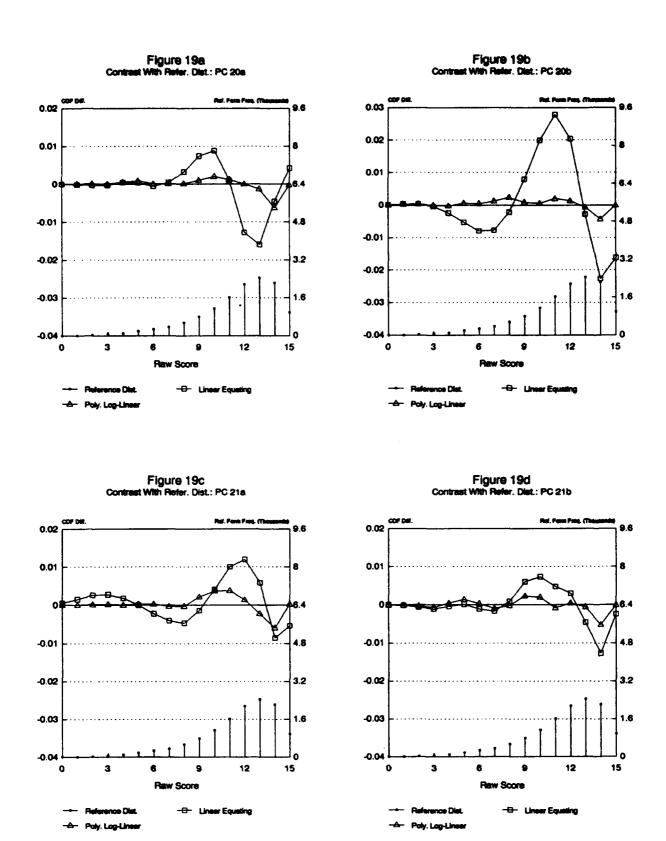


Figure 19. Contrast of Cumulative Distributions of Quartic and Polynomial Log-Linear Equated Scores With Cumulative Distributions of Reference Form for PC

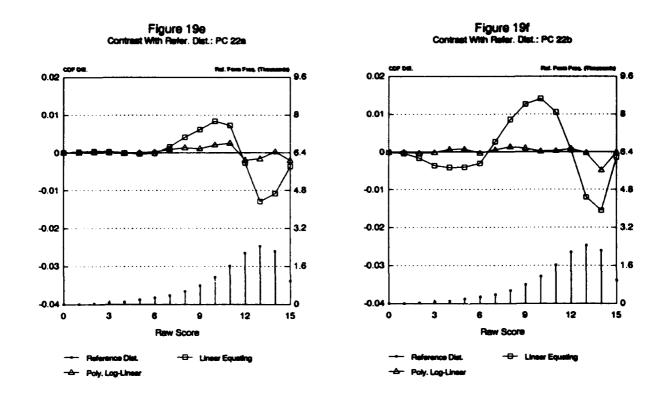
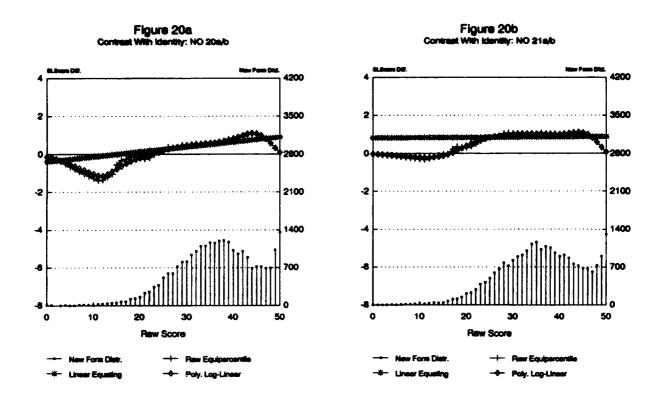


Figure 19, Con't. Contrast of Cumulative Distributions of Quartic and Polynomial Log-Linear Equated Scores With Cumulative Distributions of Reference Form for PC



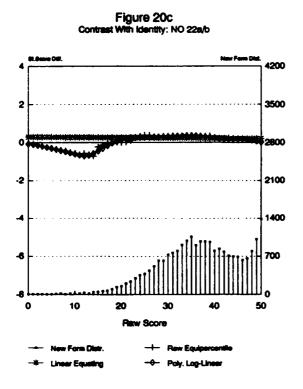
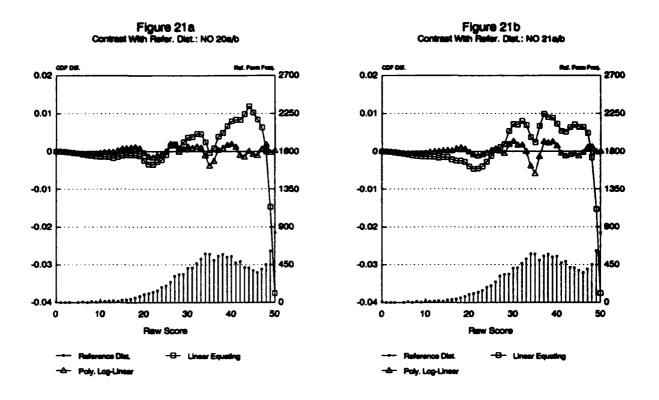


Figure 20. Standard-Score Contrast of Linear-Rescaling, Quartic Log-Linear and Polynomial Log-Linear Equatings With Linear-Identity Equating for NO



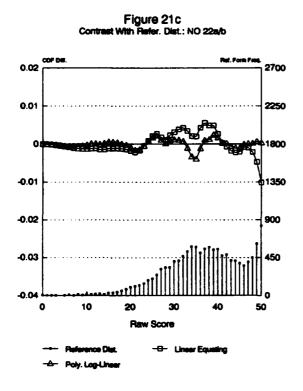


Figure 21. Contrast of Cumulative Distributions of Quartic and Polynomial Log-Linear Equated Scores With Cumulative Distributions of Reference Form for NO

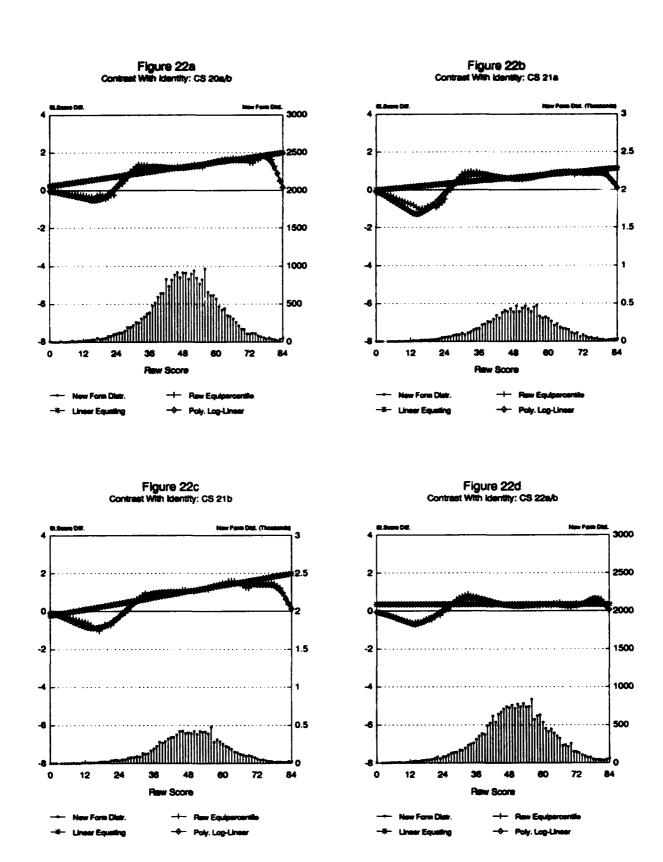


Figure 22. Standard-Score Contrast of Linear-Rescaling, Quartic Log-Linear and Polynomial Log-Linear Equatings With Linear-Identity Equating for CS

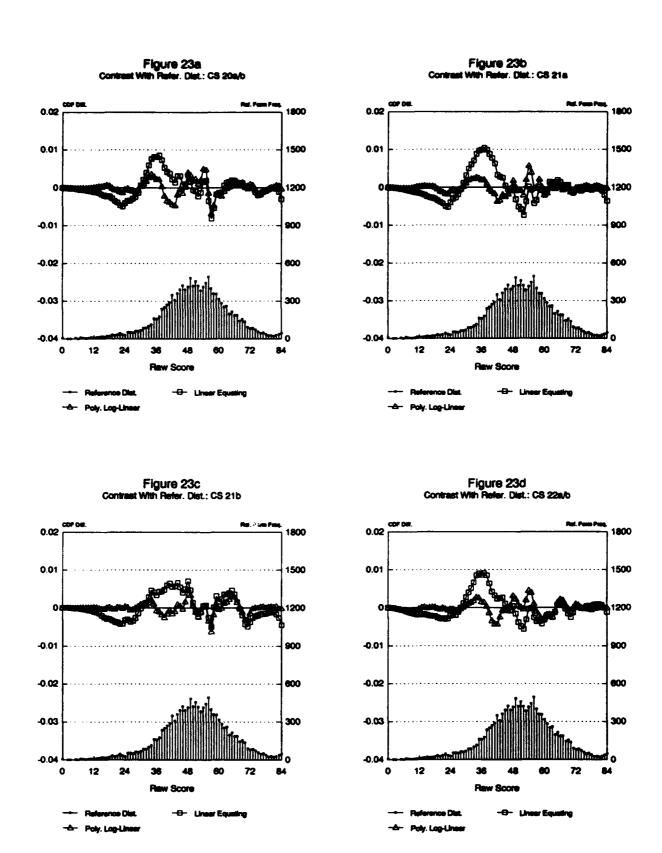
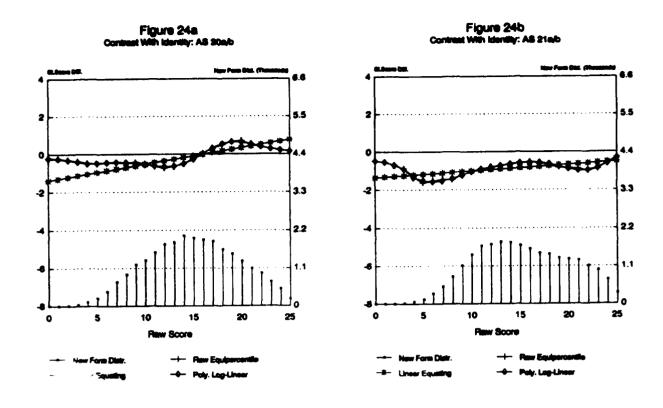


Figure 23. Contrast of Cumulative Distributions of Quartic and Polynomial Log-Linear Equated Scores With Cumulative Distributions of Reference Form for CS



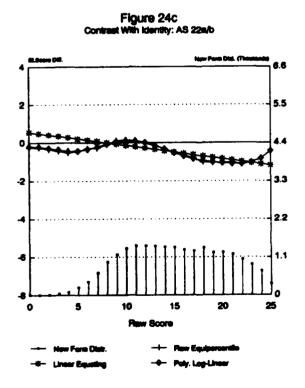
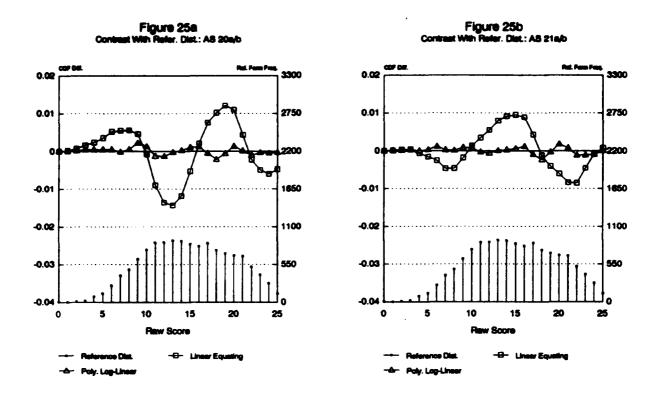


Figure 24. Standard-Score Contrast of Linear-Rescaling, Quartic Log-Linear and Polynomial Log-Linear Equatings With Linear-Identity Equating for AS



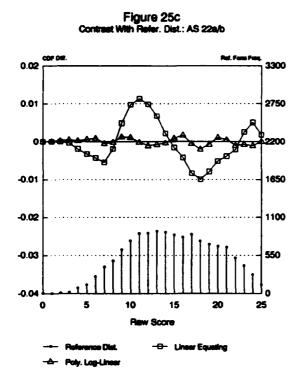
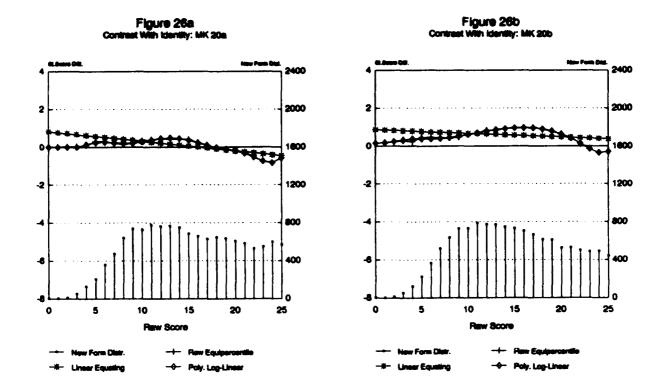


Figure 25. Contrast of Cumulative Distributions of Quartic and Polynomial Log-Linear Equated Scores With Cumulative Distributions of Reference Form for AS



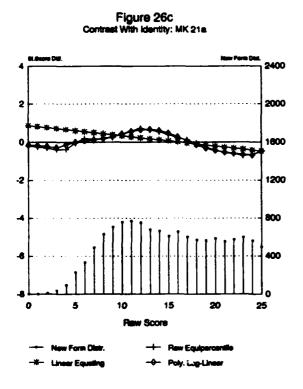
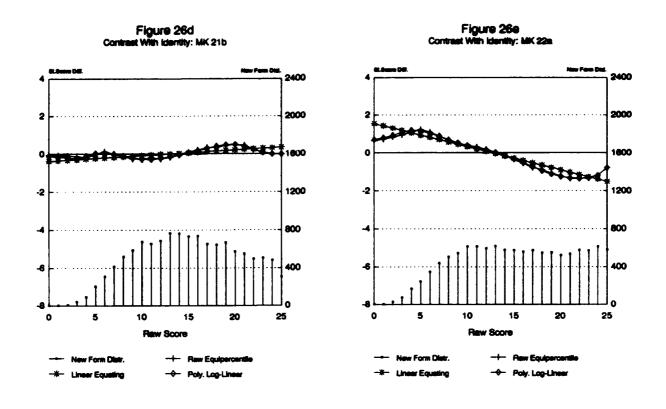


Figure 26. Standard-Score Contrast of Linear-Rescaling, Quartic Log-Linear and Polynomial Log-Linear Equatings With Linear-Identity Equating for MK



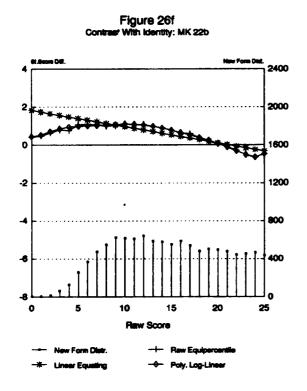


Figure 26, Con't. Standard-Score Contrast of Linear-Rescaling, Quartic Log-Linear and Polynomial Log-Linear Equatings With Linear-Identity Equating for MK

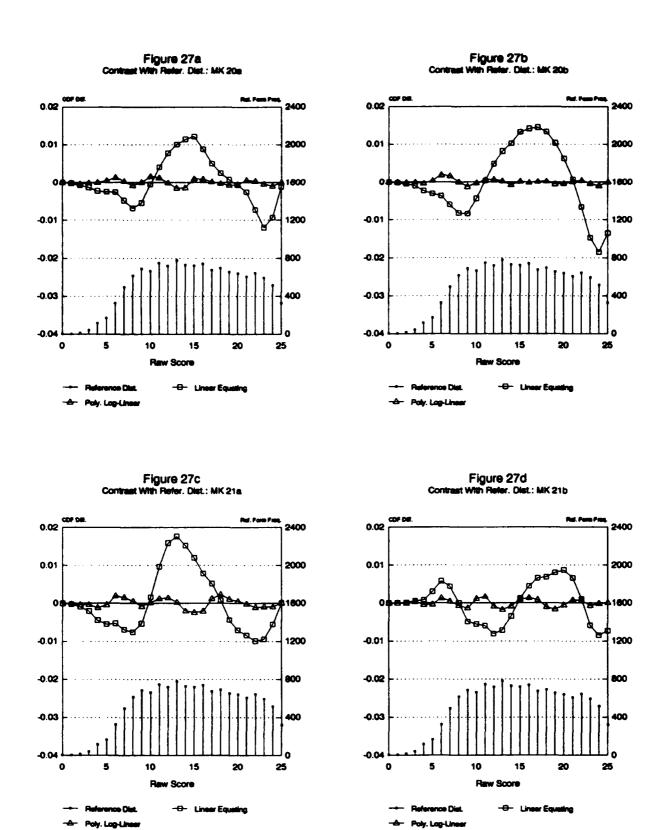


Figure 27. Contrast of Cumulative Distributions of Quartic and Polynomial Log-Linear Equated Scores With Cumulative Distributions of Reference Form for MK

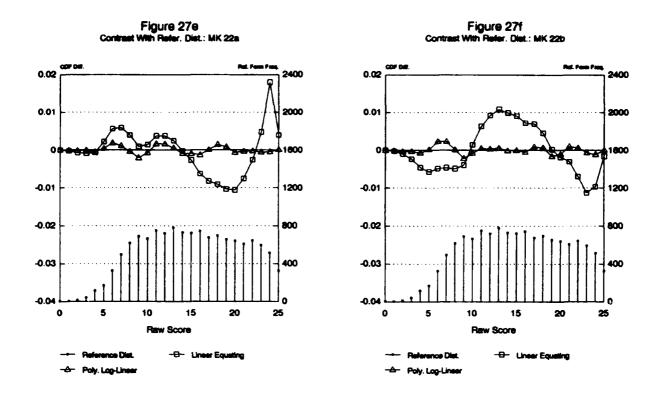
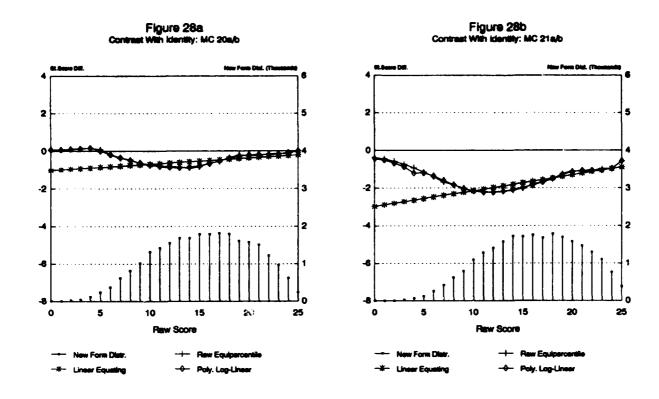


Figure 27, Con't. Contrast of Cumulative Distributions of Quartic and Polynomial Log-Linear Equated Scores With Cumulative Distributions of Reference Form for MK



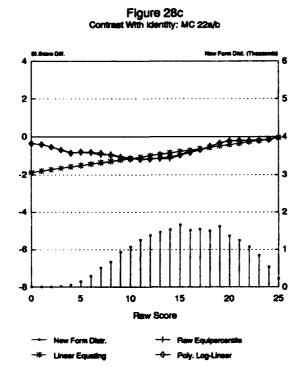
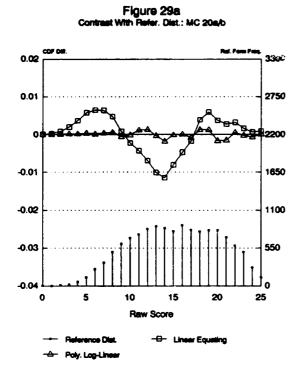


Figure 28. Standard-Score Contrast of Linear-Rescaling, Quartic Log-Linear and Polynomial Log-Linear Equatings With Linear-Identity Equating for MC



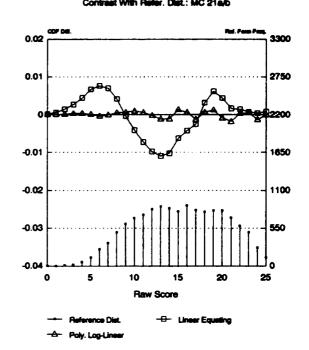


Figure 29b

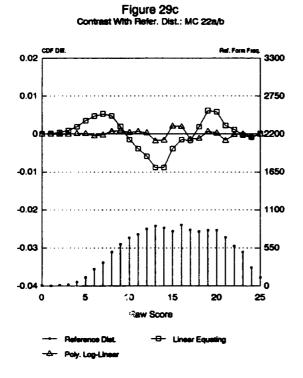
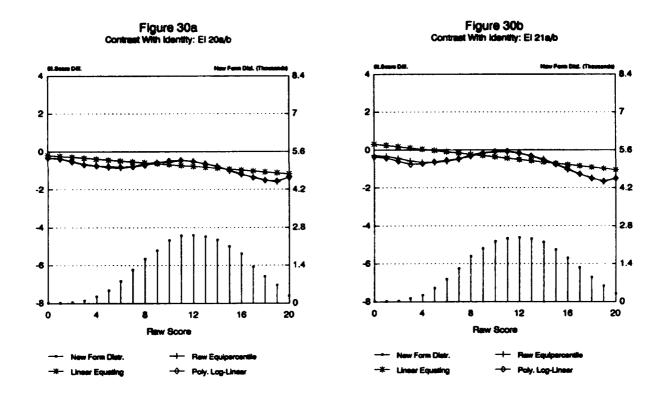


Figure 29. Contrast of Cumulative Distributions of Quartic and Polynomial Log-Linear Equated Scores With Cumulative Distributions of Reference Form for MC



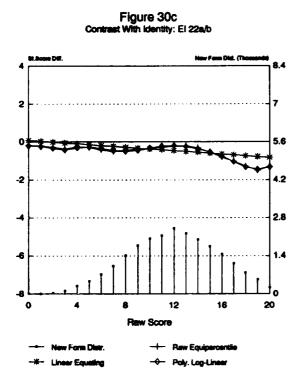
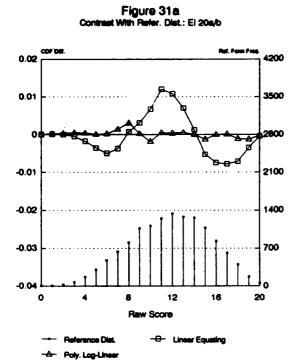
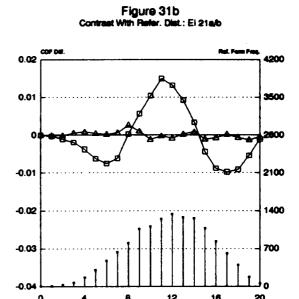


Figure 30. Standard-Score Contrast of Linear-Rescaling, Quartic Log-Linear and Polynomial Log-Linear Equatings With Linear-Identity Equating for EI





Raw Score

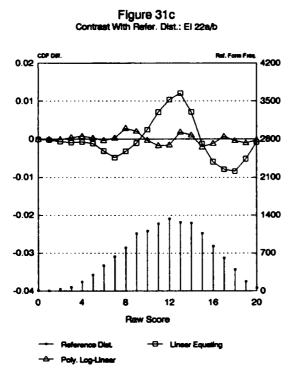


Figure 31. Contrast of Cumulative Distributions of Quartic and Polynomial Log-Linear Equated Scores With Cumulative Distributions of Reference Form for EI

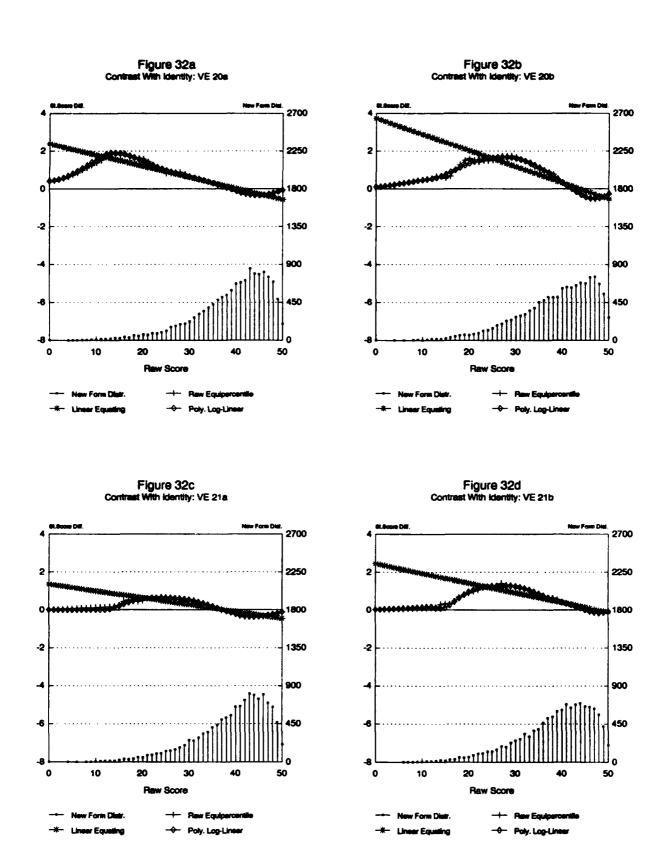


Figure 32. Standard-Score Contrast of Linear-Rescaling, Quartic Log-Linear and Polynomial Log-Linear Equatings With Linear-Identity Equating for VE

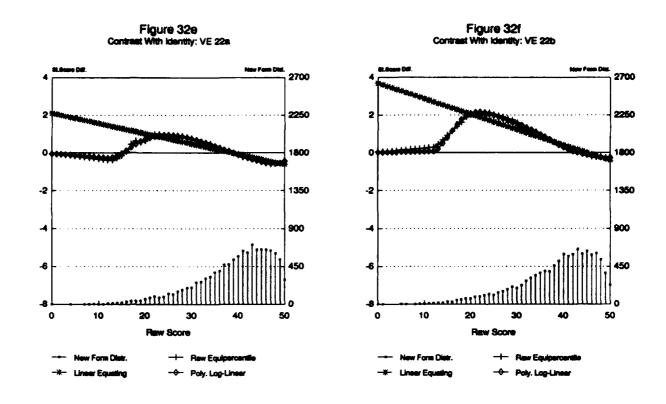


Figure 32, Con't. Standard-Score Contrast of Linear-Rescaling, Quartic Log-Linear and Polynomial Log-Linear Equatings With Linear-Identity Equating for VE

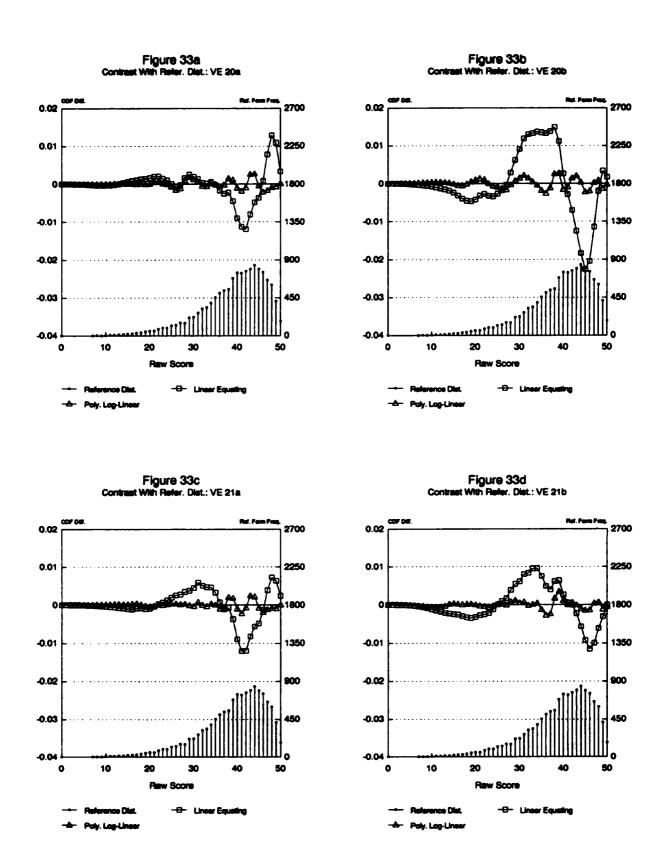


Figure 33. Contrast of Cumulative Distributions of Quartic and Polynomial Log-Linear Equated Scores With Cumulative Distributions of Reference Form for VE

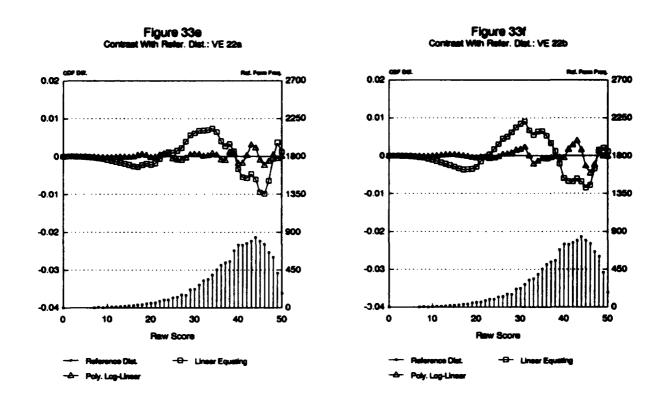


Figure 33, Con't. Contrast of Cumulative Distributions of Quartic and Polynomial Log-Linear Equated Scores With Cumulative Distributions of Reference Form for VE

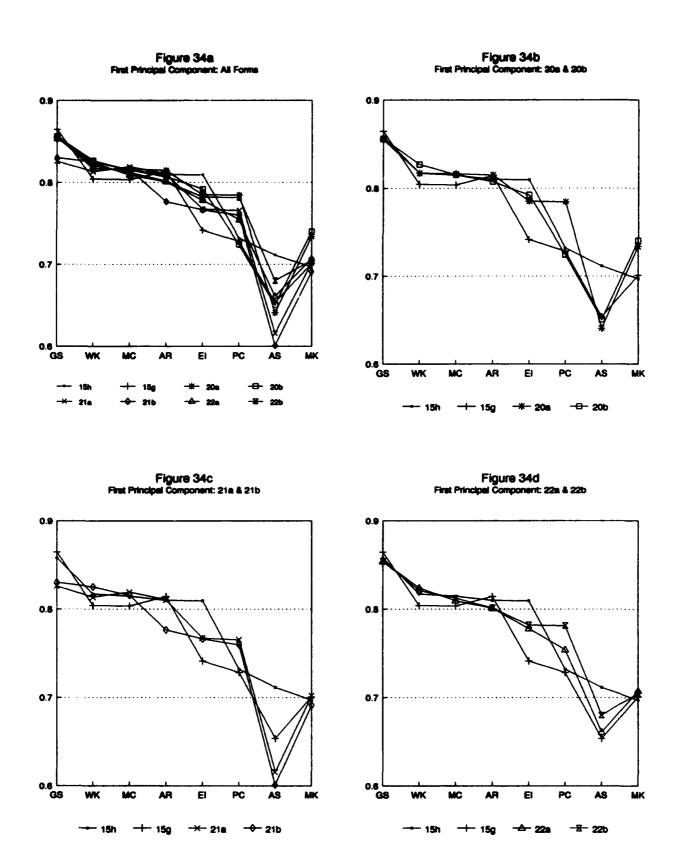


Figure 34. First Principal Component of Power Subtest Standard Scores, by Test Form

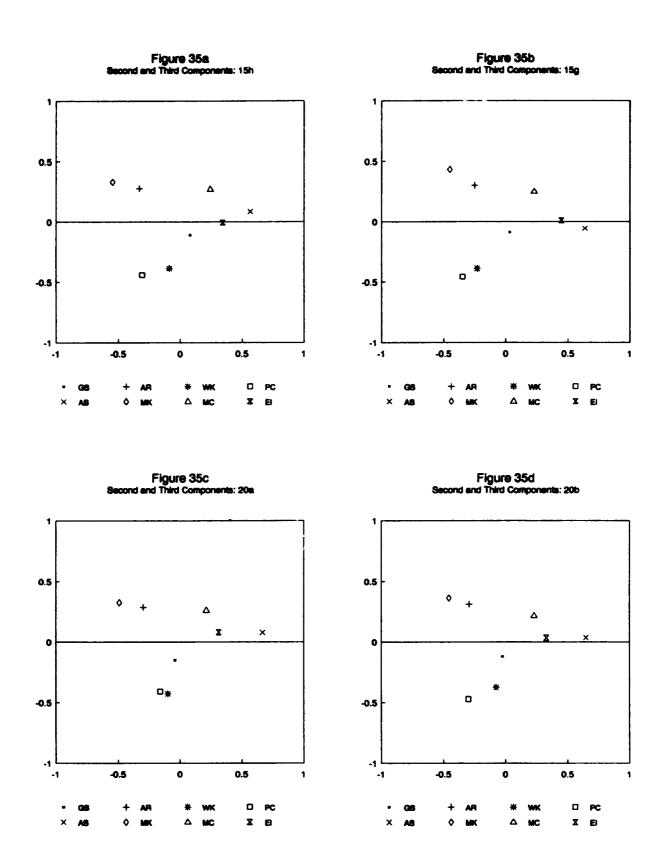


Figure 35. Second and Third Principal Components of Power Subtest Standard Scores, by Test Form

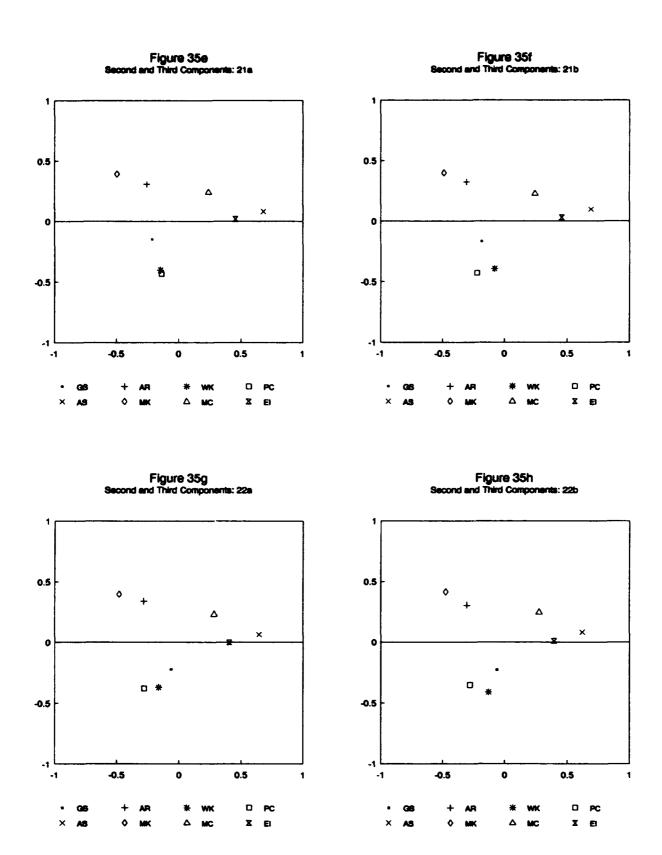


Figure 35, Con't. Second and Third Principal Components of Power Subtest Standard Scores, by Test Form